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# STANDARD DETAILS

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# HANDBOOK OF STANDARD DETAILS

FOR ENGINEERS, DRAFTSMEN
AND STUDENTS

 $\mathbf{B}\mathbf{Y}$ 

# CHARLES H. HUGHES

AUTHOR OF "HANDBOOK OF SHIP CALCULATIONS, CONSTRUCTION AND OPERATION"



ILLUSTRATED

D. APPLETON AND COMPANY NEW YORK LONDON 1921

# COPYRIGHT, 1921, BY D. APPLETON AND COMPANY

PRINTED IN THE UNITED STATES OF AMERICA

261755 JAN 15 1928 TBD H87

# PREFACE

This book was compiled especially for engineers and draftsmen, so they might have, in convenient form, drawings, tables, and formulæ of standard details for use in designing.

The data have been obtained from a variety of sources. Many of the tables have been furnished by the leading machine-tool manufacturers in the United States and represent their current practice.

Besides being of use to engineers and draftsmen, students, purchasing agents, and others interested in mechanical engineering will find the book of value.

CHAS. H. HUGHES

NEW YORK.

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# CONTENTS

# SECTION I

						3	DR	VΑ	/IN	GS	3							
																		PAGE
Notes on			_	•	•	•	•	•		•		•		•	•			1
Limit sta			-						•				•		•	•	•	3
U.S. Pat	tent	Off	ice	dra	awi	ng	з.											9
Shrinkag																		12
Geometri	ical c	on	str	uct	ion	s.					•							12
•						S	EĊ	TI	ON	I	Ι							
						F	AS	TE	NI	ΝG	S							
Bolts .																		25
Nuts .																		36
Screws										:								42
Threads:	for b	olt	s, r	ut	s, s	cre	ws	an	d p	ipe								58
Tap drill										-								77
Nails .						•.												77
Spikes								·							٠,			81
Keys .																		83
Gibs and	key	в.																88
T slots						٠.												89
Cotters																		90
			•			SI	EC	TI	ON	I	II							
				PC	w	ER	1	RA	N	M	IS	SIC	N					
Shafting																		91
Quill driv																		92
Coupling	<b>8</b> .																	94
Clutches																		99
Collars																		105
Bearings																		106
•								v	ii									

viii	CONTENTS	
	PAGE	
Pulleys		
Mule stands		
Belting		
Belt drives		•
Rope sheaves and p		
	ting power	
Sprockets		
Gearing	141	
Spur	142	
Miter and bevel		
Worm		
Helical		
Herringbone .		
	•	
4	SECTION IV	
7521	PE, TUBES AND FITTINGS	
	•	
Trade customs .		
Standard wrought is	on pipe	
	nt iron pipe	
Double extra strong	wrought iron pipe 165	
	166	
Nipples		
Boiler tubes	167	
Flanges		
Brass and copper tu	bes	
•		
Expansion joints .		
•		
	SECTION V	
	•	
RO	PE AND CHAIN FITTINGS	
Turnbuckles		
Thimbles		
Sockets		
Clevis nuts		
Sister hooks	010	

	CONTENTS
	PAGE
	Eye bolts
_	Hooks
	Shackles
	Slings—rope and chain
	Chain—hoisting and anchor
I	Orum scores for chain and rope
	SECTION VI
	MISCELLANEOUS DETAILS
Ŧ	Handles
	Hand wheels
_	Knobs
_	Knurled set
_	Vrenches
•	Spanners
	Stuffing boxes
	Orill shanks
_	Washers
. (	Clinch rings
-	Springs
	Angle couplings
	Knuckle joints
	Yoke ends
F	Rod ends
7	Cool straps and bolts
	Caper pins
I	Finished ends of shafts, studs, screws and bushings 265
	Standard squares for chuck screws and wrenches
	•
	SECTION VII
_	STRUCTURAL DETAILS
_	Rivets
	Riveted joints
	Structural shapes
	Wire and sheet metal gauges
	Plates
	Gauges for punching
	Rivet spacing
1	Beam connections

# CONTENTS

X

# SECTION VIII

# USEFUL TABLES

					PAGE
Weights and measures					294
Metric units					296
Metric and U.S. equivalent measures .					297
Decimal equivalents of an inch	. /				300
Inches and fractions in decimals of a foot					301
Strength of materials					302
Specific gravities and weights of materials					303
Equivalent values of mechanical, electrical	and	heat	uni	ts.	304

# HANDBOOK OF STANDARD DETAILS

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# HANDBOOK OF STANDARD DETAILS

# SECTION I

### **DRAWINGS**

NOTES ON SHOP DRAWINGS—LIMIT STANDARDS—U. S. PATENT OFFICE DRAWINGS—SHRINKAGE OF CASTINGS—GEOMETRICAL CONSTRUCTIONS

# NOTES ON SHOP DRAWINGS

# COMMON ABBREVIATIONS

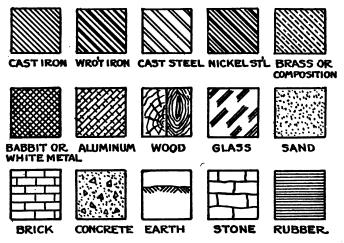
	" or ins.	_	inches	or sq.	ins	. = square inches
	' or ft.	=	feet	or sq.	ft.	= square feet
	f.	=	surface to be finished	F.A.O.	= 1	finished all over
	C.L.	=	center line	dia.	=	diameter
	Cb.	=	counterbore	thds.	-	threads ·
	Csk.	=	countersunk	U.S.G.	=	United States Gauge
	B.W.G.	=	Birmingham or Stubs	Wire Ga	uge	J
	B. & S.	=	Brown & Sharpe or A	merican S	Star	ndard Wire Gauge
_	A.W.G.	=	American Wire Gauge	c.i.	=	cast iron
	w.i.	=	wrought iron	m.i.	=	malleable iron
	c.s.	=	cast steel	Br.	=	brass
	Bz.	=	bronze	O.d. = ou	tsic	le dia. I.d. = inside dia.
	Zn.	=	zinc	# or lb.	=	pound
	Ft.B.M.	_	feet board measure	••		•
	π		3.14159	_		center to center
	• •	asio	ons not to scale should			red or marked "Not to
	Scole "					2,000

Where several pieces are shown on a drawing always have a bill of material and a table for noting alterations and date.

The title is preferably printed in the lower right hand corner.

I beam

# HATCHINGS FOR SECTIONS



RIVET MARKINGS, see page 275.

## LIMIT STANDARDS

### EXPLANATION

# Symbols used on drawing—Using I " as an example

- r" Rough gauge.—Shaft to be ground and to use gauge for shaft work preparatory to grinding.
- I' Finish gauge.—Shaft to be turned or ground to gauge furnished and within the "Go" and "No Go" limits.
- 1" Drive gauge.—Shaft to be turned or ground for a drive fit, and to be furnished to limits of "Go" and "No Go" gauge.
- t" Free hole (Free holes taking in running and sliding fits).—Hole to be bored or reamed to plug furnished and to come within "Go" and "No Go" limits.
- 1" Standard plug.—Hole to be bored or reamed to standard plug furnished and to come within limits of "Go" and "No Go" gauges.

USE WITH S	YMBOL—FINISH GAUG STANDARD SHAFT TANDARD HOLE (WRIN H FREE HOLE (RUNNIN	GING FIT)	DIA. IN INCHES
Maximum	· Minimum	Tolerance	
.3750 .4375	.3743 .4368	.0007 .0007	. %
.5000	.4990	.0010	128
.5625	.5615	.0010	. 62
.6250	.6240	.0010	5%
.6875	.6865	.0010	11/16
.7500	.7490	.0010	
.8125	8115	.0010	179
.8750 .9375	.8740 .9365	.0010 .0010	162
1.0000	.9990	.0010	1 786
1.0000 1.0625	1.0615	.0010	Ī1⁄4
1.1250	1.1240	.0010	11/6 11/6 13/6
1.1875	1.1865 1.2490	.0010	11/4
1.2500	1.2490	.0010	11/
1.3125 1.3750	1.3115 1.3740	.0010 .0010	1 2/16
1.4375	1.3740	.0010	172
1.5000	1.4990	.0010	112
1.5625	1.5615	.0010	1%
1.6250	1.6240	.0010	15/8
1.6875	1.6865	.0010 .0010	111/6
1.7500 1.8125	1.7490 1.8115	.0010	1137
1.8750	1.8740	.0010	176
1.9375	1.9365	.0010	115%
2.0000	1.9990	.0010	2
2.1250	2.1240	.0010 .0010	21/4 21/4 28/2:
2.2500 2.3750	2.2490	.0010	21/4
2.3750 2.5000	2.3740 2.4990	.0010 .0010	212
2.6250	2.6240	.0010	25%
2.7500 •	2.7490	.0010	234
2.8750	2.8740	.0010	27/8
3.0000	2.9985	.0015	3 31⁄4
3.1250 3.2500	3.1235	.0015 .0015	378
3.3750	3.2485 3.3735	.0015	382
3.5000	3.4985	.0015	312
3.6250	3.6235	.0015	35%
3.7500	3.7485	.0015	31/4
3.8750	3.8735	.0015	31/8
4.0000 4.1250	3.9985	.0015 .0015	414
4 2500	4.1235	.0015	412
4.2500 4.3750	4.2485 4.3735	.0015	43%
4.5000	4.4985	.0015	41%
4.6250	4.6235	.0015	456
4.7500	4.7485	.0015	4 34
4.8750	4.8735	.0015	4 1/8 5
5.0000 5.1250	4.9985 5.1235	.0015 .0015	5½
5.2500	5.2485	.0015	514
5.2500 5.3750	5.3735	.0015	53%
5.5000	5.4985	.0015	514
5.6250	5.6235	.0015	5 %
5.7500 5.8750	5.7485 5.8735	.0015	5% 572
6.0000	5.8735 5.9980	.0015	5/8 6
6.1250	6.1230	.002	61/6
6.2500	6.2480	i .002 ⋅ i	614
6.3750	6.3730	l ,002 l	6%

ROU PREPARA (Special C	SYMBOL—ROUGH GAUGE ROUGH TURNING PREPARATORY to GRINDING (Special Cases on Long Shafts) BCREW MACHINE WORK								
Maximum	Minimum	Tolerance							
	Minimum  .383 .445 .508 .570 .633 .695 .759 .821 .946 1.010 1.072 1.135 1.197 1.262 1.324 1.387 1.449 1.512 1.574 1.637 1.827 1.827 1.827 1.827 1.827 2.270 2.145 2.270 2.145 2.270 2.145 2.270 2.145 2.270 2.145 2.270 2.145 2.270 2.145 2.270 2.145 2.270 2.395 2.520 2.645 2.770 2.895 3.150 3.275 3.400 3.525	Tolerance	**************************************						
3.660 3.785 3.910 4.035	3.650 3.775 3.900 4.025	.010 .010 .010 .010	35/8 33/4 37/8 4						

SYMBOL—STANDARD PLUG WRINGING AND DRIVE FITS STANDARD HOLE WRINGING FIT, USE WITH ST'D SHAFT

WRINGING FIT, USE WITH ST'D SHAFT DRIVE FIT, USE WITH DRIVE FIT SHAFT

DIA. IN INCHES SYMBOL-FREE HOLE BUNNING AND SLIDING FITS

FREE HOLE
USE WITH STANDARD SHAFT]

	SHAFT		INCHES			
faximum	Minimum	Tolerance		Maximum	Minimum	Tolerance
1 Aximum  . 3750 . 4375 . 5000 . 5625 . 6250 . 6875 . 7500 . 8125 . 9375 . 1.0000 1.0625 1.1250 1.1875 1.2500 1.1825 1.3250 1.3250 1.3325 1.3750 1.5625 1.7500 1.8750 1.8750 1.8750 1.8750 1.8750 2.2500 2.2500 2.2500 2.2500 2.2500 2.2500 2.3750 3.3750 3.3750 3.3750 3.3750 3.3750 3.3750		Tolerance  .0003 .0005 .0005 .0005 .0005 .0005 .0007 .00007 .0007 .0007 .0000	**************************************	Maximum  .3760 .4385 .5015 .5040 .6265 .6890 .7515 .8140 .8765 .8140 .8765 .1.1270 .1.1895 .1.2520 .1.3145 .1.5025 .1.5650 .1.6275 .1.5650 .1.8775 .1.4905 .1.8150 .1.8775 .1.9400 .2.1280 .2.1280 .2.2780 .2.3780 .3.1285 .3.1285 .3.2535	Minimum  .3755 .4380 .5008 .5038 .6258 .6883 .7508 .8133 .8758 .8133 .1.0010 .1.1260 .1.1260 .1.1260 .1.13135 .1.2510 .1.3135 .1.5012 .1.3760 .1.4385 .1.5012 .1.5637 .1.6887 .1.7512 .1.8137 .1.8762 .1.913 .1.8762 .1.913 .1.8762 .1.913 .1.8762 .1.913 .1.8762 .1.913 .1.8762 .1.913 .1.8762 .1.913 .1.8762 .1.913 .1.8762 .1.913 .1.8762 .1.913 .1.8762 .1.913 .1.9	Tolerance  .0005 .0007 .0007 .0007 .0007 .0007 .0007 .0010 .0010 .0010 .0010 .0010 .0013 .0013 .0013 .0013 .0013 .0013 .0015

Continued from page 6

SYMBOL—STANDARD PLUG WRINGING AND DRIVE FITS STANDARD HOLE WRINGING FIT, USE WITH STANDARD SHAFT DRIVE FIT, USE WITH DRIVE FIT SHAFT			DIA. IN INCHES	RUNNIN	BOL-FREE G AND SLID 'REE HOL TH STANDAE	ing fits E
Maximum	Minimum	Tolerance		Maximum	Minimum	Tolerance
		,	45555555555555555555555555555555555555	4 .8795 5 .0050 5 .1300 5 .2550 5 .3800 5 .5055 5 .6305 5 .7555 6 .8005 6 .0070 6 .13270 6 .3820 6 .5075 6 .6325 6 .7575 7 .0080	4.8775 5.0030 5.1280 5.2530 5.3780 5.6035 5.6285 5.7535 6.0040 6.1290 6.2540 6.3790 6.6045 6.6295 6.7545 6.8795 6.8795	.002 .002 .002 .002 .002 .002 .002 .003 .003

### PRESS AND SHRINK FITS

Press fits.—Either one or both parts are given a slight taper as  $\frac{1}{16}$  to  $\frac{1}{16}$  in. per foot. The allowance between a hole in a cast iron hub and a steel shaft to be pressed in, may be taken as about .004 in., and for a steel hub and shaft .003. Press fits are not as satisfactory as shrink for resisting torsional stresses.

Shrink fits.—Both hole and shaft are generally cylindrical altho sometimes a slight taper is given. For cast iron and steel shrink fits an allowance of .0015 times the diameter of the shaft plus .005 in. may be used. Some companies make no difference in allowance between press and shrink fits.

# BRONZE BEARING LIMIT STANDARD

STANDARD SHAFT BEARING PLUG ALLOWANCE FOR RUNNING FIT

				RUNNI	NG FII
Size	Maximum	Minimum	Tolerance	Maximum	Minimum
5%	.6273	.6258	.0015	.0033	.0008
5/8 11/16	.6898	.6883	.0015	.0033	.0008
3/4	.7523	.7508	.0015	.0033	.0008
18/16	.8148	.8133	.0015	.0033	.0008
18/16 7/8 15/16	.8773	.8758	.0015	.0033	.0008
15/16	.9398	.9383	.0015	.0033	.0008
1	1.0030	1.0010	.002	.0040	.0010
11/16	1.0655	1.0635	.002	.0040	.0010
11/8	1.1280	1.1260	.002	.0040	.0010
$1\frac{3}{16}$ $1\frac{1}{4}$	1.1905	1.1885	.002	.0040	.0010
11/4	1.2530	1.2510	.002	.0040	.0010
15/16	1.3155	1.3135	.002	.0040	.0010
13/8	1.3780	1.3760	.002	.0040	.0010
13/8 17/16	1.4410	1.4385	.0025	.0045	.0010
11/2	1.5037	1.5012	.0025	.0047	.0012
19/16	1.5662	1.5637	.0025	.0047	.0012
15/2	1.6287	1.6262	.0025	.0047	.0012
111/16	1.6912	1.6887	.0025	.0047	.0012
$1\frac{3}{4}$	1.7537	1.7512	.0025	.0047	.0012
113/16	1.8162	1.8137	.0025	.0047	.0012
11/8	1.8787	1.8762	.0025	.0047	.0012
115/16	1.9412	1.9387	.0025	.0047	.0012
2	2.0045	2.0015	.003	.0055	.0015
$2\frac{1}{8}$	2.1295	2.1265	.003	.0055	.0015
$2\frac{1}{4}$	2.2545	2.2515	.003	.0055	.0015
23/8	2.3795	2.3765	.003	.0055	.0015
$2\frac{1}{2}$	2.5045	2.5015	.003	.0055	.0015
25/8	2.6295	2.6265	.003	.0055	.0015
23/4	2.7545	2.7515	.003	.0055	.0015
$\frac{\overline{2}}{2}$	2.8795	2.8765	.003	.0055	.0015
3	3.0050	3.0020	.003	.0065	.0020
$\frac{31/8}{31/4}$	3.1300	3.1270	.003	.0065	.0020
31/4	3.2550	3.2520	.003	.0065	.0020
33/8	3.3800	3.3770	.003	.0065	.0020
31/2	3.5050	3.5020	.003	.0065	.0020
35/8	3.6300	3.6270	.003	.0065	.0020
$\frac{3\frac{3}{4}}{3\frac{7}{8}}$	3.7550	3.7520	.003	.0065	.0020
31/8	3.8800	3.8770	.003	.0065	.0020
4	4.0055	4.0020	.0035	.0070	.0020
41/8	4.1305	4.1270	.0035	0070	` .0020

LIMIT OF WEAR ON PLUG GAUGES

Standard Plugs	Free Hole, Roughing and Special Plugs
Tolerance of .0003 to .0005—.0002 " " .0005 " .0015—.0003	Tolerance of .0005 to .001—.0003 " " .001 " .005—.0005 " " over .005—.001

# U. S. PATENT OFFICE DRAWINGS

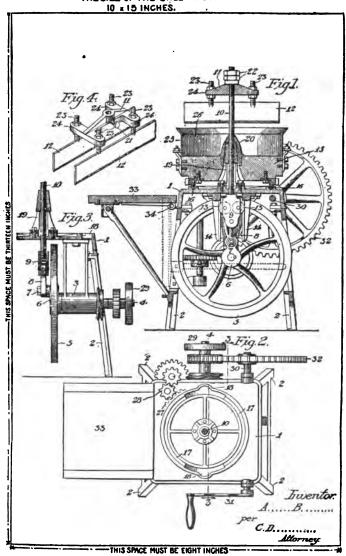
Drawings must be made upon pure white paper of a thickness corresponding to two-sheet or three-sheet Bristol board. The surface of the paper must be calendered and smooth. India ink alone must be used, to secure perfectly black and solid lines.

The size of a sheet on which a drawing is made must be exactly 10 by 15 ins. One inch from its edges a single marginal line is to be drawn, leaving the "sight" precisely 8 by 13 ins. Within this margin all work and signatures must be included. One of the shorter sides of the sheet is regarded as its top, and, measuring downward from the marginal line, a space of not less than  $1\frac{1}{4}$  ins. is to be left blank for the heading of title, name, number and date.

All drawings must be made with the pen only. Every line and letter (signatures included) must be absolutely black. This direction applies to all lines, however fine, to shading, and to lines representing cut surfaces in sectional views. All lines must be clean, sharp and solid, and they must not be too fine or crowded. Surface shading, when used, should be open. Sectional shading should be made by oblique parallel lines, which may be about one-twentieth of an inch apart. Solid black should not be used for sectional or surface shading. Free-hand work should be avoided wherever it is possible to do so.

Drawings should be made with the fewest lines possible consistent with clearness. Shading (except on sectional views) should be used only on convex and concave surfaces, where it should be used sparingly, and may even there be dispensed with if the drawing be otherwise well executed. The plane upon which a sectional view is taken should be indicated on the general view by a broken or dotted line, which should be designated by numerals corresponding to the number of the sectional view. Heavy lines on the shade sides of objects should be used, except where they tend to thicken the work and obscure letters of reference. The light is always sup-

THE SIZE OF THE SHEET MUST BE EXACTLY



posed to come from the upper left hand corner at an angle of 45 degs.

The scale to which a drawing is made ought to be large enough to show the mechanism without crowding, and two or more sheets should be used if one does not give sufficient room to accomplish this end; but the number of sheets must never be more than is absolutely necessary.

The different views should be consecutively numbered. Letters and figures of reference must be carefully formed. They should, if possible, measure at least one-eighth of an inch in height, so that they may bear reducing to one twenty-fourth of an inch; and they may be much larger when there is sufficient room. They must be so placed in the close and complex parts of drawings as not to interfere with a thorough comprehension of the same, and therefore should rarely cross or mingle with the lines. When necessarily grouped around a certain part they should be placed at a little distance, where there is available space, and connected by lines with the parts to which they refer. They should not be placed upon shaded surfaces, but when it is difficult to avoid this, a blank space must be left in the shading where the letter occurs, so that it shall appear perfectly distinct and separate from the work. If the same part of an invention appear in more than one view of the drawing it must always be represented by the same character, and the same character must never be used to designate different parts.

The signature of the applicant should be placed at the lower right hand corner of each sheet, and the signatures of the witnesses, if any, at the lower left hand corner, all within the marginal line, but in no instance should they trespass upon the drawings. The title should be written with pencil on the back of the sheet. The permanent names and title constituting the heading will be applied subsequently by the office in uniform style.

All views on the same sheet must stand in the same direction and must if possible stand so that they can be read with the sheet held in an upright position. If views longer than the width of the sheet are necessary for the proper illustration of the invention the sheet may be turned on its side. The space for heading must then be reserved at the right and the signatures placed at the left, occupying the same space and position as in the upright views and being horizontal when the sheet is held in an upright position. One figure must not be placed upon another or within the outline of another.

Drawings transmitted to the U. S. Patent Office should be sent flat, protected by a sheet of heavy binder's board; or should be rolled for transmission in a suitable mailing tube, but should never be folded.

An agent's or attorney's stamp, or advertisement or written address will not be permitted upon the face of a drawing, within or without the marginal line.

WEIGHT OF WOOD PATTERNS COMPARED TO WEIGHT
OF CASTINGS

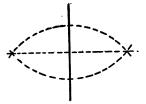
A pattern weighing one pound (less weight of core boxes) made of	Cast Iron Lbs.	Brass '	Bronze Lbs.	Copper Lbs.	Zine Lbs.
Pine or fir	11.7	18.8 13.2 .95	19.3 13.5 .98	19.7 13.7 .99	15.5 11.2 .81
Pear		11.5	11.8	11.9	9.8

Thus if a pine pattern weighed one pound, a casting of cast iron from it would weigh 16 lbs., of brass 18.8 lbs., of bronze 19.3 lbs., etc.

### SHRINKAGE OF CASTINGS

Patterns for castings should be made larger than dimensions given on drawings to allow for shrinkage. For iron castings (gray and malleable) the allowance for shrinkage is  $\frac{1}{6}$  inch per foot, for steel  $\frac{1}{4}$  inch, for brass  $\frac{3}{6}$  inch, for lead  $\frac{1}{8}$  inch, for tin  $\frac{1}{12}$  inch and for zinc  $\frac{3}{6}$  inch.

### GEOMETRICAL CONSTRUCTIONS

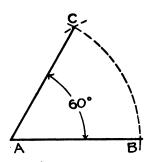


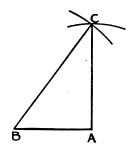
To Bisect a Straight Line and Draw a Perpendicular to It.—With the ends as centers and with a radius greater than one-half the line, describe arcs intersecting on both sides of the line. A line through the intersections will bisect the line and be perpendicular to it.

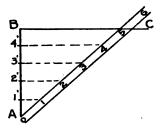
To Draw a Right Triangle, Given One Side.—Let A B be the side, and divide it into 6 equal parts. With A as center and radius equal to 8 parts describe an arc. With B as center and radius equal to 10 parts describe another arc. From their intersection C draw A C and C B, A C being perpendicular to A B.

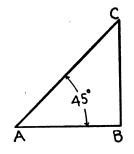
To Divide a Line Into a Number of Equal Parts when the divisions on the scale are larger than the parts. If A B is the line, draw B C perpendicular to it. Suppose A B is to be divided into 5 equal parts—take a scale or a foot rule and place one end at A and the division 5 of the scale on the line B C. Draw horizontal lines through the divisions 1, 2, 3 and 4,—then their intersections on A B as 1', 2', 3' and 4' are equal parts of the line A B.

To Lay Off a 45 Deg. Angle.—Let A B and B C be two equal lines forming a right angle. A line connecting A and C will be at an angle of 45 degs. to A B.



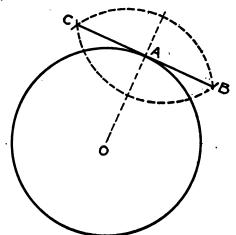




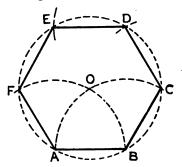


To Lay Off a 60 Deg. Angle.— From the line AB, with A as center, and any radius draw arc BC. With the same radius and B as center describe an arc cutting BC at C. Join A and C. The line AC will make an angle of 60 degs. with AB. For an angle of 30 degs. bisect BC. To Draw a Tangent to a Circle From a Point on the Circumference.

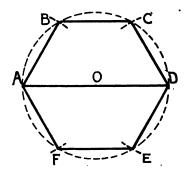
—If A is the point, draw a radial line O A. At A draw a line B C at right angles to O A, which line will be tangent to the circumference at A.



To Draw a Hexagon When the Length of One Side is Given.—Let A B be the given side, then with A B as a radius and A and B as centers draw arcs intersecting at O. With O as center and radius A B draw a circle through A and B. With the same radius and C as center describe an arc cutting the circle at D. Points E and F are obtained in a similar way. Connecting B, C, D, E, F and A gives the required hexagon.



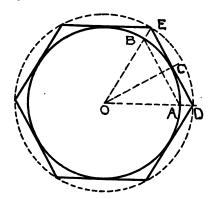
To Draw a Hexagon, Given the Long Diameter.—Bisect the long diameter A D at O. With O as center and A O as radius describe a circle. Using the same radius and A as center, draw an arc cut-



ting the circle at B and F. With D as center describe an arc cutting the circle at C and E. Connect A, B, C, D, E and F.

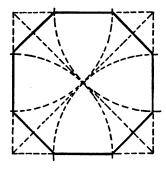
To Inscribe a Hexagon in a Circle.—Divide the circle into six parts by stepping around the circumference with dividers a chord equal to the radius. Draw lines connecting the consecutive points.

To Circumscribe a Hexagon About a Circle.—Lay off a chord A B equal to the radius of the circle, and bisect its arc at C. At C draw a tangent D E meeting O D and O E. Describe a circle with radius O D, and space O D around the circle—the points thus obtained when joined will form a hexagon.



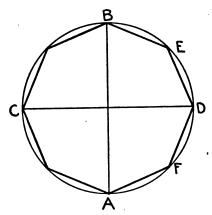
Or draw a line O D. Lay a 60 deg. triangle on O D so that it is tangent to the circle at C. The tangent drawn will be one side of the hexagon. At E draw a horizontal line tangent to the given circle. By the continued use of the 60 deg. triangle the other sides of the hexagon can be drawn.

To Inscribe an Octagon in a Square.—Draw the diagonals of the square. With the corners as centers and a radius of one-half a

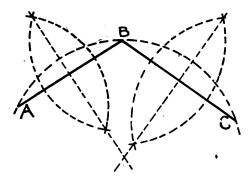


diagonal draw arcs cutting the sides of the square. Connect the intersections of the arcs and the sides of the square.

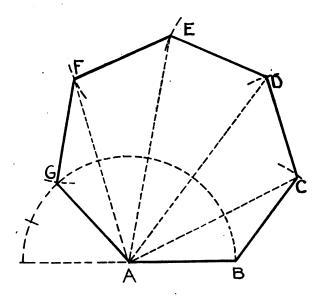
To Inscribe an Octagon in a Circle.—Draw A B perpendicular to C D. Bisect the arc B D at E, A D at F, etc. Join points B, E, D, F, etc.



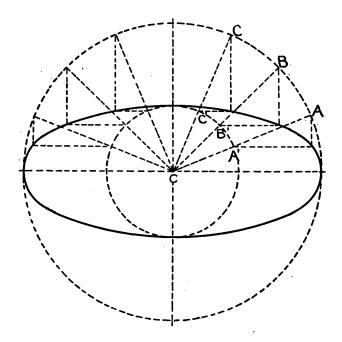
To Draw an Arc Through Three Points A, B and C.—Join the points. Bisect A B and B C, and at their centers draw perpendiculars. Where the perpendiculars meet is the center of the required arc.



To Construct a Polygon of n Sides Having Given One Side A B.—With A B as radius and A as center describe a semicircle and divide

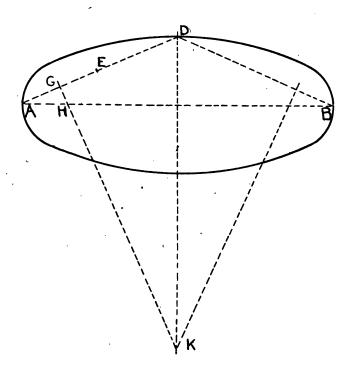


it into n parts. From n subtract 2, the remainder being the number of parts through which lines G A, A F, etc. are drawn. In the present case n = 7, and there are thus 5 parts from B to G. With A B as radius and B as center describe an arc cutting A C at C,—with the same radius and C as center describe an arc cutting A D, and so on, giving points E, F and G. By connecting the points a polygon is formed.



To Draw an Ellipse.—First Method.—With C as a center draw two circles, one with the diameter equal to the major axis of the ellipse and the other equal to the minor axis. Divide the circumference of the large circle into any number of equal parts and draw from the divisions lines to the center C. Draw vertical lines from A, B, C, etc., and horizontal from A', B', C', etc. The intersections of the vertical and horizontal lines will be points on the ellipse.

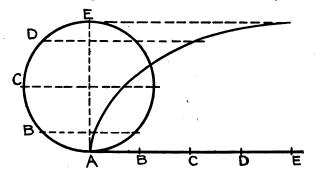
Second Method.—Lay off D E equal to the difference between the major and minor axes of the required ellipse. Bisect A E and erect a perpendicular to A D at G, cutting A B at H and D K at K. Follow the same procedure on B D. Then H and K are cen-



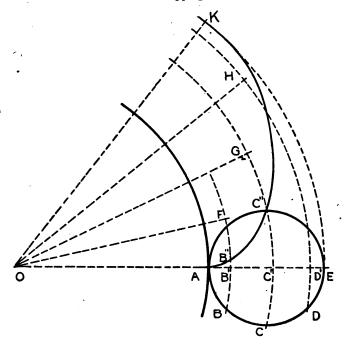
ters for two arcs approximately forming part of an ellipse—the centers for the other two arcs are found in a similar manner to that just outlined.

Cycloid.—This curve is traced by a point on the circumference of a circle rolling on a straight line without slipping. If A E is the diameter of the generating circle, divide the semi-circumference into n equal parts, and lay off the arcs A B, A C, etc., along the base

line A E. On horizontal lines through B, C, etc., lay off A B, A C, etc. A curve through the ends of these lines will be a cycloid.

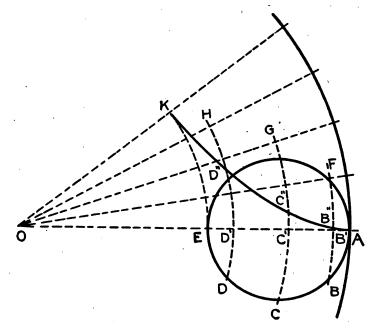


Epicycloid.—A curve generated by a point on the circumference of a circle which rolls without slipping on the outside of another



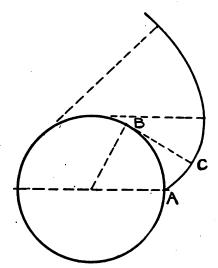
circle—is an epicycloid. Divide the semi-circumference of the rolling circle into n equal parts (in the present case into 4) and lay off the arcs A B, A C, A D and A E on the circumference of the base circle. With O as center draw arcs through B, C, D, E cutting the extended radii of the base circle at F, G, H, K. From F, G, H lay off arcs equal to B B', C C', D D'. A curve passing through B'', C'', etc., is an epicycloid.

Hypocycloid.—This curve is generated by a point on the circumference of a circle which rolls without slipping on the inside of



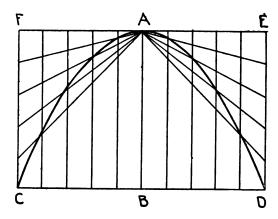
another circle. Divide the semi-circumference of the rolling circle into n equal parts (in the present case into 4) and lay off the arcs A B, A C, A D on the circumference of the base circle. With O as center draw arcs through B, C, D, E cutting the radii of the base circle at F, G, H, K. From F, G, H lay off arcs equal to B B', C C', D D'. A curve passing through B'', C'', etc. is a hypocycloid.

Involute.—A curve traced by the end of a taut string unwound from the circumference of a circle is an involute. If B C is tangent



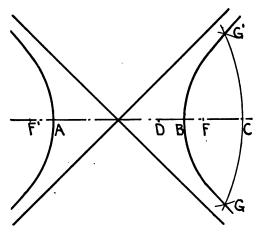
to the circle, lay off on it, the arc A B—then the point C is on the involute. By drawing more tangents other points can be found.

Parabola.—Height A B and base C D given. Divide C D into



any number of even parts as 10, and erect perpendiculars. Divide the sides C F and D E into the same number of parts as C B and B D. From the divisions on C F and D E draw lines to the apex A. Where these lines cut the perpendiculars from C D are points in the parabola.

**Hyperbola.**—Let A B be the distance between the two branches of the hyperbola, and F and F' the foci. Take any distance as F' C and with F' as center describe an arc. Lay off F' D = A B.



With F as center and radius D C describe an arc cutting the previous one at G and G', which are points on the hyperbola. Other points can be found in a similar way.

### LAYING OFF ANGLES WITH A TWO-FOOT RULE

• To lay off an angle, open the ends of the rule to the distance given in the following table. Thus for a 45 deg. angle open the rule until the ends are 9.20 ins. apart.

Degrees	Inches	Degrees	Inches	Degrees	Inches
1 2 3 4 5 7.5 10	.21 .422 .633 .837 1.04 1.57 2.09 3.015	15 20 25 30 35 40 45 50	3.12 4.17 5.21 6.21 7.20 8.21 9.20 10.12	55 60 65 70 75 80 85 90	11.08 12 12.89 13.76 14.61 15.43 16.21 16.97

TABLE FOR THE DIVISION OF THE CIRCUMFERENCE OF A CIRCLE

			<del></del>		
Number of	Angle of	Length of	Number of		Length of
Divisions	Correspond-	Chord in	Divisions	Correspond-	Chord in
in the	ing Division	Decimal	in the	ing Division	Decimal
Circum-	of Circle;	Fraction	Circum-	of Circle;	Fraction
ference	Degrees	of Radius	ference	Degrees	of Radius
3	120	1.73206	52	6.55	0.120356
4	90	1.41422	53	6.47	0.118032
5	72	1.17558	54	6.40	0.11629
5 6 7 8 9	60	1	55	6.32	0.113966
7.	51.25	0.86732	56	6.25	0.111644
8	45	0.76536	57	6.18	0.1099
9	40	0.68404	58	6.12	0.108158
10	36	0.61804	59	6.06	0.106414
11	32.43	0.563	60	6	0.104672
12	30	0.51764	61	5.54	0.102928
13	27	0.4782	62	5.48	0.101186
14	25	0.4448	63	5.42	0.99442
15	24	0.41582	64	5.37	0.0977
16	22.30	0.39018	65	5.32	0.096538
17	21.10	0.36734	66	5.27	0.094794
18	20	0.3473	67	5.22	0.093632
19	18.56	0.32894	68	5.17	0.091888
20	18	0.31286	69	5.13	0.090765
21	17.08	0.29792	70	5.08	0.089564
22	16.21	0.2841	71	5.04	0.088402
23	15.39	0.272	72	5	0.087238
24	15	0.26106	73	4.55	0.085496
25	14.24	0.25066	74	4.51	0,084332
26	13.50	0.24086	75	4.48	0.083752
27	13.20	0.23218	76	4.44	0.083588
28	12.51	0.22352	77	4.40	0.081426
29	12.24	0.216	78	4.36	0.080264
30	12	0.20906	79	4.33	0.0791
31	11.36	0.20212	80	4.30	0.078518
32	11.15	0.19574	81	4.20	0.077356
33	10.54	0.18996	82 83	4.23	0.076194
34	10.35	0.18416		4.20 4.17	0.075612 0.07445
35	10.17	0.17894	84 85	4.14	0.073868
36 37	9.43	0.17432	86	4.11	0.073808
37 38	9.43	0.1691 0.16504	87	4.08	0.072706
38 39	9.28	0.1604	88	4.05	0.070962
40	9.13	0.15692	89	4.02	0.07038
41	8.46	0.15286	90	4.02	0.069798
42	8.34	0.14938	91	3.57	0.0686362
43	8.22	0.1459	92	3.54	0.0680546
44	8.10	0.14242	93	3.52	0.0674732
45	8.10	0.13952	94	3.49	0.0663104
46	7.49	0.13603	95	3.47	0.0657288
47	7.39	0.133128	96	3.45	0.0651474
48	7.30	0.130806	97	3.42	0.064566
49	7.20	0.127904	ll 98	3.40	0.0639844
50	7.12	0.125582	99	3.38	0.063403
51	7.03	0.122678	100	3.36	0.0628216
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## SECTION II

#### **FASTENINGS**

BOLTS—NUTS—SCREWS—THREADS FOR BOLTS, NUTS, SCREWS AND
PIPE—TAP DRILLS—NAILS—SPIKES—KEYS—GIBS AND
KEYS—T SLOTS—COTTERS

#### BOLTS

### MEASUREMENT OF BOLTS, SCREWS AND RIVETS

The length of flat head screws, stove bolts and countersunk oval head screws includes the head and half the head of round head wood screws—but excludes the head of round and fillister head machine screws and round head stove bolts.

The length of rivets is exclusive of the head except countersunk heads, where the length of the head is included.

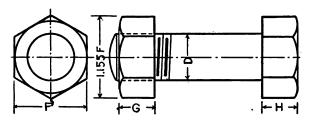
The diameter of screws is measured by the Brown and Sharpe gauge, see page 43.

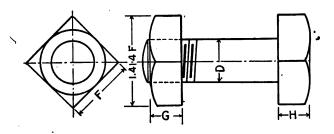
The diameter of structural rivets is given in inches or fractions thereof. See Structural Details, pages 270 and 271.

#### MATERIALS

The material selected depends on the purpose the bolt is to be used for. The U. S. Navy for class B open hearth carbon steel requires a tensile strength of 58,000 lb. per sq. in., elastic limit 30,000 lb. per sq. in., elongation in 8 ins. of 289 and be bent cold 180 degs. without showing fracture. Special bolts as Society of Automotive Engineers hexagon head cap screws can be obtained with a tensile strength of 100,000 lb. per sq. in. and elastic limit of 60,000. Bolts, screws and nuts are also made of bronze and composition.

United States Standard Bolt Heads and Nuts





Finished	Head	Finished Nut				
F	н	F	G			
1.5 D + ½6"	D — 1/16"	1.5 D + 1/16"	.5 F — ½6"			

Hexagon heads and nuts.—The distance between opposite corners (the long diameter) =  $1.155 \times$  the distance between sides (the short diameter).

Square heads and nuts.—The distance between opposite corners (the long diameter) =  $1.414 \times$  the diameter between sides (the short diameter).

FINISHED HEXAGON HEADS AND NUTS

Dia.	Threads	Diameter		Height	Dia.	Threads	Diar	neter	Height
bolt	per in.	Short	Long	neight	bolt	per in.	Short	Long	Height
1/4/5/16/3/8/7/16/5/8/3/4/8 1 1/4/8/11/3/8	20 18 16 14 13 12 11 10 9 8 7 6	7,66 17,52 5,8 23,32 13,16 29,32 1 13,16 1 3,4 1 15,16 2 1,8	1/2 39/64 23/52 53/64 15/66 11/64 11/9/52 113/66 21/64 21/64 21/64 22/64	3.66 3.66 3.66 3.66 3.66 1.66 1.66 1.66	1½ 15/8 13/4 17/8 21/4 2½ 23/4 31/4 33/4 4	6 5 <sup>1</sup> / <sub>2</sub> 5 5 4 <sup>1</sup> / <sub>2</sub> 4 4 3 <sup>1</sup> / <sub>2</sub> 4 3 <sup>1</sup> / <sub>4</sub> 3 <sup>1</sup> / <sub>4</sub> 3 <sup>1</sup> / <sub>4</sub>	25/16 21/2 21/2 21/8 37/16 33/16 43/16 49/16 41/5 55/16 61/16	243,64 257,64 37,64 35,76 31,782 413,82 427,82 53,53 67,64 636,64 631,62	17/16 19/16 111/16 113/16 115/16 23/16 211/16 215/16 33/16 311/16 311/16 315/16

U. S. Standard is the same as the Franklin Institute. For working stress see U. S. Standard threads, page 59.

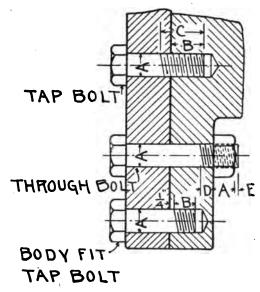
## • MANUFACTURERS' SQUARE AND HEXAGON BOLT HEADS

No universal standard has been adopted by all manufacturers. The following table gives dimensions commonly used:

Dia. of bolt	Short dia.	Height	Dia. of bolt	Short dia.	Height
1/4 5/16 3/8 7/16 1/2	3/8 15/32 9/16 21/32 3/4 27/32	3/6 15/64 9/32 21/64 3/8 27/64 15/82	3/4 7/8 1 11/8 11/4 13/8	1 1/8 1 5/16 1 1/2 1 11/6 1 7/8 2 1/16	9/16 21/32 3/4 27/32 15/16 11/42
9/16 5/8	27/32 15/16	15/82	11/2	$2\frac{1}{4}$	11/8

[Russell, Burdsall & Ward Bolt & Nut Co., Port Chester, N. Y.]
For threads per inch see U. S. Standard Bolt Heads.

## SCREW ENDS OF STANDARD HEXAGON-HEADED BOLTS



[Niles-Bement-Pond Co., New York, N. Y.]

A = diameter of bolt  $B = 1\frac{1}{2}A$   $C = 1\frac{1}{2}A + \frac{1}{4}$ "

 $D = \frac{1}{8}$  for bolts up to and including  $\frac{5}{8}$  diameter and  $\frac{1}{4}$  for those larger.

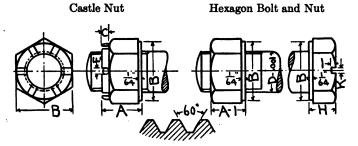
 $E=\frac{1}{6}$ " for bolts up to and including  $\frac{1}{6}$ " diameter and  $\frac{1}{6}$ " for those larger.

Height or thickness of nut is taken as equal to the diameter of the bolt, which is approximately true.

Studs in cast iron—depth of tap should be the same as for tap bolts, viz.: 1½ times the diameter of the stud.

Drilled holes which are to be tapped should not extend into spaces subject to pressure.

# SOCIETY OF AUTOMOTIVE ENGINEERS BOLTS AND NUTS



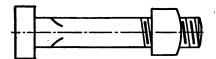
S. A. E. Screw Thread

D = Diameter of Screw	D x 1.5 + $\frac{1}{4}$ in. = Length of
P = Pitch of Thread	Threaded Portion
B = Short dia. of Nuts and Screw Heads	$\frac{P}{8}$ = Flat Top
$\frac{1}{P}$ = Number of threads per in.	d = Diameter of Cotter Pin

D	1/4	5/16	3/8	7/16	1/2	%6	5/8	11/16	3/4	1/8	1
Thds per in.	28	24	24	20	20	18	18	16	16	14	14
A	<sup>9</sup> / <sub>52</sub>	21/64	13/82	29/64	9/16	39/64	23/32	49/64	13/16	29/82	1
A-1	7/82	17/64	21/64	3/8	7/16	81/64	35/84	19/82	21/32	49/64	7∕8
В	7/16	1/2	9/16	5/8	3/4	1/8	15/16	1	11/16		17/16
C	3/82	3/52	1/8	1/8	³∕16	8/16	1/4	1/4	14	1/4	1/4
E	5/64	5/64	1/8	1/8	1/8	5/32	5/32	5/2	5/82	5/2	5/82
H	<sup>3</sup> ⁄16	15/64	%2 %2	21/64	3/8	27/64	15/32	33/64	%16	21/32	3/4
I	3/32	764	1/8	1/8	1/8	1/8	1/8	1/8	1/8	1/8	1/8
K	1/16	1 <sub>16</sub>	3/22	³ <b>%2</b>	3/32	3/32	3/52	8/82	8 <b>√2</b>	3/52	8/82
d	1/16	1/16	8/82	3/82	3/82	1/8	1/8	1/8	1/8	1/8	1/8
Tap drill.	<b>₹</b>	17/64	23/64	3/8	7/16	1/2	916	3%4	43%4	25/32	29/52

Heads and nuts semi-finished.

## DECK BOLTS



Round head, square under.

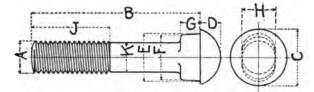
				Diameter	:	
		3/8"	7/16"	1/2"	9/16 "	5/8"
		lbs.*	lbs.*	lbs.*	lbs.*	lbs.*
83	1¾	9½				
Length Over All in Inches	2	10½	161⁄2	22	1	
Ħ.	21/4	111/2	171/2	221/2		
F F	21/2	121/2	181/2	23	331/2	40
ver	$2\frac{3}{4}$	13½	191⁄2	241/2	34	42
<del>t</del> ь 0	3			26	341/2	44
[eng	31⁄2	••••		29	371/2	48
_	4	••••		32	40½	52
	4½	• • • •		35	44	56
Size	of Head	3⁄4 x 1∕8	7⁄8 x ³∕16	1 x 3/16	1 x 1/4	11/8 x 1/4
Size	of Nut	5/8 x 5/16	23/22. X 3/8	13/6 x 7/6	29/ <sub>32</sub> x ½	1 x 33/64
Thre	ead per In.	16	14	13	12	11

[Hoopes & Townsend, Philadelphia, Pa.]

May be obtained black or galvanized.

<sup>\*</sup>Approximate weight per 100.

TRACK BOLTS



Track bolts are manufactured with U. S. Standard rolled thread, buttress and U. S. Standard cut thread. With rolled and buttress threads the diameter of the threaded portion is about ½6 in. greater than the unthreaded, while with cut threads the diameter of the threaded and unthreaded portion is the same. Bolts may be obtained with either square or hexagon nuts.

U. S. STANDARD ROLLED THREAD TRACK BOLT

		He	ad	Shoulder				Length of	Dia.	Nut		
Dia. A	Length B	С	D	E	F	G	н	thread J	Shank K	Height	Width across flats	
3 8 1/2 1/2 5/8 3/4 2/2 5/8 1/8 15/6 1 1 1/16	Per order	11/6 13/6 11/2 11/4 19/2 15/6 11/2 15/8 11/6	15/32 1/2 17/32 9/16 5/8 21/2	17,52 11,66 29,52 11,66 11,66 11,66 17,52 17,52 13,8 13,8	1/2/ 21/2/ 7/8 11/2/ 11/3/2 13/6 13/6 111/2/ 111/2/	7/16	11,32 29,64 37,64 11,16 23,52 3,4 13,16 7,8 15,16	Per	11,52 29,52 37,64 11,16 23,52 3,4 13,16 7,8 15,16	3/8 1/2 5/8 3/4 3/4 7/8 1 1	11/6 7/8 11/6 11/4 11/4 13/8 17/6 15/8	

[Illinois Steel Co., Chicago, Ill.]

Bolts can be obtained with cut, rolled and rolled buttress threads.

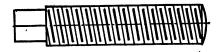
## Boiler Patch Bolts or Tap Rivets



Diameter	1/2"	5/8"	3/4"	7/8"	1"
Threads per inch	14	12	12	12	12
Length from largest diameter of bevel to point.	\$4 7/8 1 11/8 11/4 11/2	3/4 7/8 1 11/8 11/4 11/2	7/8 1 11/8 11/4 11/2	1 1½8 1¼4 1½2	· i 1½ 1½ 1½ 1½

[Hoopes & Townsend, Philadelphia, Pa.]

### BOILER STAY BOLTS



34", 136", 78", 156", 1", 116", 118", 136" and 114" dia. All diameters have 12 threads per inch. Length of threaded part from 2½" up,—cut to order. Stay bolts after being screwed into place may have nuts on the ends, instead of being riveted over.

[Hoopes & Townsend, Philadelphia, Pa.]

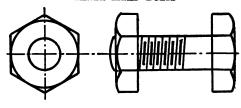
TAP BOLTS
Square and Hexagon Heads



Diameter	ж"	16"	3/8"	7∕16″	1/2"	5/8"	%"	1∕8″	1"	11/6"	11/4"
Threads per inch	20	18	16	14	13	11	10	9	8	7	7
Sizes of square and hexagon heads	3/8 X 3/16	15/2 X 15/4	% x %	31/64 31/64	3/4 x 3/8	16/6 X 16/6	11/8 x %	15/16 X 21/42	1½ x ¾	111/6 X 37/2	17/8 X 15/16

[Hoopes & Townsend, Phila., Pa.]

### PLANER HEAD BOLTS



Dia. of screw Short dia. of head Thickness of head	11/8"	1 1/8 " 3/8 "	5/8" 11/4" 3/8"	11/6" 11/4 3/8"	1 1/16 " 1/2"

Length under head to extreme point all sizes 1",  $1\frac{1}{4}$ ",  $1\frac{1}{2}$ ",  $1\frac{3}{4}$ ", 2".

All sizes have 12 threads per inch.

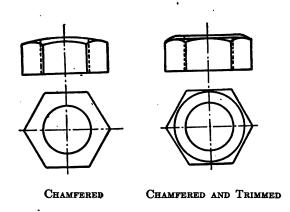
Bolts have either square or hexagon heads.

Nuts same size as heads.

[Hartford Machine Screw Co., Hartford, Conn.]

### NUTS

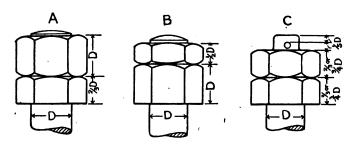
For U. S. and Franklin Institute standard hexagon and square nuts see page 26. For S. A. E. (Society Automotive Engineers) hexagon nuts see page 29. Nuts can be obtained hot pressed, cold punched or milled from bars.



### DEVICES TO PREVENT NUTS FROM COMING LOOSE

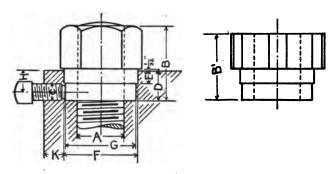
Nuts can be prevented from coming loose by lock or check nuts, set screws or split pins. In the latter case castellated nuts are often used. See pages 29 and 38.

### LOCK OR CHECK NUTS



As the greatest load is on the top nut this should be the largest as shown in A. Spanners are seldom thin enough to take a thin bottom nut, and the nuts are sometimes arranged as in B which is convenient but faulty theoretically. C is a compromise of A and B, both nuts being the same size. Short diameter of nuts same as U. S. Standard—which see.

### NUTS WITH SET SCREWS



### Hexagon Head:

Head-Standard U.S. Nut.

A = dia. of bolt or stud

 $B = 1\frac{1}{2}A + \frac{1}{8}$ 

 $C = \frac{A}{8} + \frac{1}{4}$ 

D = 1%C

 $\mathbf{E} = \mathbf{H} - \frac{\mathbf{C}}{2} .$ 

 $F = 1\frac{1}{2}A + \frac{1}{16}$ 

 $G = F - \frac{1}{2}$ ; depth of G = C

 $H = 1\frac{1}{8}C$ 

K for wrot iron and brass =  $C + \frac{1}{16}$ "

" cast iron =  $\frac{13}{16}C + \frac{1}{16}$ "

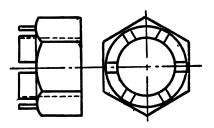
### Slotted Head:

Head-see Slotted Nuts.

B' = A + D, other dimensions same as for hexagon head.

There is another type having a collar with the depth E and diameter F, below the ring with a diameter G. With this design the nut cannot slip by the set screw.

CASTELLATED HEXAGON NUTS



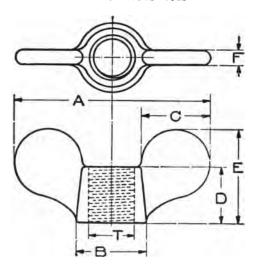
Screw Diameter	Total Thickness of Nut	Height of Castle	Diameter of Nut Across Flats of Hex.	Diameter of Castle	Diameter of Facing	Depth of Facing	Number of Slots in Castle	Depth of Slots in Castle (to round bottom)	Width of Slot in Castle	Diameter of Cotter Pin Used	Threads per inch
1/4	%2	3/82	7/16	7/16	7/16	164	6	3/52	5/64	1/16	28
5/16	21/64	3/52	1/2	1/2	1/2	164	6	3/2	5/64	1/16	24
3/8	13/32	1/8	9/16	9/16	9/16	1/64	6	1/8	1/8	3/82	24
7/16	29/64	1/8	5/8	5/8	5/8	164	6	1/8	1/8	3/52	20
1/2	<sup>9</sup> ⁄16	3/16	3⁄4	3/4	3/4	1/64	6	3/16	1/8	3/52	20
%6	<sup>39</sup> ⁄64	3/16	7∕8	7/8	7⁄8	1/64	6	3/16	5/82	1/8	18
5⁄8	23/32	1/4	15/16	15/16	15/16	1/64	6	1/4	5/22	1/8	18
11/16	49/64	1/4	1	1	1	1/64	6	1/4	5/82	1/8	16
<u>¾</u>	13/16	1/4	11/16	11/16	11/16	1/64	6	1/4	5 <b>√2</b> 2	1/8	14
<b>⅓</b> 8	<sup>29</sup> ⁄ <sub>32</sub>	1/4	11/4	11/4	11/4	1/64	6	1/4	5/82	1/8	14

[Hartford Machine Screw Co., Hartford, Conn.]

This nut can be kept from coming loose by cotter pin through the slots. For Society Automotive Engineers castellated nut see page 29.

# PLANER HEAD NUTS (See Planer Head Bolts)

## THUMB OR WING NUTS



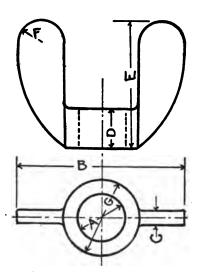
A	В	C	D	E	F	Т
5/8 23/32	1/4 9/32 5/2	7,32 1,4	3/16 7/32	13/32 7/16 17/32	3/52 3/32	3/2*-56† 1/8 -40
23 52 13 16 17 52 15 16 115 52	9 32 5 16 7 16 1 2	932 7/16 15/32	11,32 3/8	5/8 11/6	1/8 1/8 5/32	3/6 -24 1/4 -20 5/6 -18
$\frac{1}{2}\frac{32}{6}$	916 5/8 3/1	1/2 9/16 3/4	7/8 7/16 1/2 9/16 5/8	34 1316 9/6	552 552 552 552 816 752 144 144	5 <sub>16</sub> —18  3 <sub>8</sub> —16  7 <sub>6</sub> —14
2 <sup>5</sup> / <sub>6</sub> 2 <sup>19</sup> / <sub>52</sub> 2 <sup>31</sup> / <sub>52</sub> 3 <sup>7</sup> / <sub>52</sub>	13/16 7/8	13 16 15 16	5/8 23/2	16 5/8 23/12	3/16 7/32	$\begin{vmatrix} 1 & -13 \\ 2 & -12 \\ 3 & -12 \end{vmatrix}$
37/22	15/52	$1\frac{1}{16}$ $1\frac{1}{8}$	23,32 13,16 15,16	23 52 13 16 15 16	1/4	34 —10

[Billings & Spencer, Hartford, Conn.]

\* Diameter.

<sup>†</sup> Threads per inch.

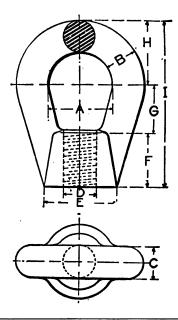
THUMB OR WING NUTS-Continued



A*	Threads per inch	. В	c	D	E	F	G
8/16 1/4 5/16	24	11/8	3/16	3/16	11/8	3/16	3/8
1/4	20	11/4	3/16	<sup>3</sup> /16	11/4	<sup>3</sup> /16	1/2 5/8
5/16	18	15/8	<sup>3</sup> ⁄16	1/4	13/8	1/4	
3/8	16	111/16	1/4	1/4 5/16	1%	1/4	11/16
7/16	14	2	1/4	<b>3</b> /8	15/8	5/16	3⁄4
1/2	13	21/8	5/16	<sup>7</sup> ⁄16	13/4	5/16	₹8
<b>5</b> /8	11	25/8	5/16	9/16	17/8	3/8	11/8
3/4	10	211/16	5/16	5/8	2	3/8	13/16

<sup>\*</sup> A can be tapped and threaded as thumb nuts on page 39. Wing nuts may be made of cast iron, composition or of drop forged steel.

EYE NUTS

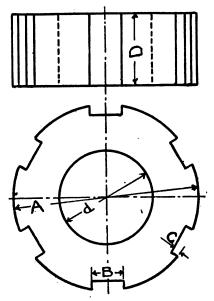


Size	A Inches	B Inches	C Inches	In. U. S. S.	E Inches	F Inches	G Inches	H Inches	I Inches
3/8 1/2 5/8 3/4	7/8 11/8 13/8 11/2	5/16 7/16 9/16 3/4	1/4 3/8 1/2 3/4	3/8*-16† 1/2 -13 5/8 -11 8/4 -10	3/4 1 11/4 13/4	3/4 1 11/4 11/4	3/4 1 11/4 11/8	3/4 1 11/4 11/2	2½ 3 3¾ 3½ 3½
$\frac{7}{8}$ $\frac{1}{1\frac{1}{4}}$ $\frac{1}{1\frac{1}{2}}$	$1\frac{5}{8}$ $1\frac{3}{4}$ $2$ $2\frac{1}{2}$	7/8 1 11/4 13/8	3/4 7/8 11/8 11/4	$     \begin{array}{r}       7_8 - 9 \\       1 - 8 \\       1 \frac{1}{4} - 7 \\       1 \frac{1}{2} - 6     \end{array} $	2 2½ 2½ 3½ 3½	$1\frac{1}{4}$ $1\frac{5}{8}$ $1\frac{7}{8}$ $2\frac{1}{8}$	1 1½ 1¾ 1¾ 1¾	$\begin{array}{c} 1  {}^{11} 16 \\ 1  {}^{7} \! {}_{8} \\ 2  {}^{1} \! {}_{4} \\ 2  {}^{5} \! {}_{8} \end{array}$	$3^{15}_{16}$ $4^{3}_{4}$ $5^{1}_{2}$ $6^{1}_{2}$
$\frac{134}{2}$	3 3½	1½ 15/8	13/8 11/2	$1\frac{3}{4} - 5$ $2 - 4\frac{1}{2}$	3½ 4	23/8 3	2 2½	3 3¾8	73/8 87/8

<sup>\*</sup> Diameter.

<sup>†</sup> Threads per inch.

## SLOTTED ROUND NUTS



d = diameter of bolt.

A = .2d

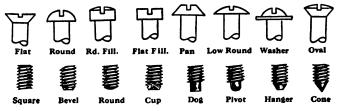
C = .13d

B = .3d

D = .75d

# SCREWS

### STYLES OF HEADS AND SCREW POINTS



Note.—Rd. Fill. = Round Fillister.

Flat Fill. = Flat Fillister.

Table of Decimal Equivalents of Screw Gauge For Machine and Wood Screws, Brown & Sharpe Standard The difference between consecutive sizes is .01316 inch

No. of Screw Gauge	Size in Decimals of in.	No. of Screw Gauge	Size in Decimals of in.	No. of Screw Gauge	Size in Decimals of in.
000	.03152	9	.17628	20	. 32104
00	.04468	10	.18944	21	.33420
0	.05784	11	.20260	22	.34736
1	.07100	12	.21576	23	. 36052
2	.08416	13	.22892	24	.37368
3	.09732	14	.24208	25	.38684
4	.11048	15	. 25524	26	.40000
5	. 12364	16	.26840	27	.41316
6	. 13680	17	.28156	28	.42632
7	.14996	18	. 29472	29	.43948
8	.16312	19	.30788	30	. 45264
				•	

Wood Screws (Standard and Drive)

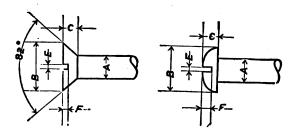
Standard Wood Screws
(Iron and Brass)



Standard wood screws, if driven with a hammer, loose their holding power. Screws perpendicular to the grain have about 25% more holding power than those parallel to the grain.

1

DIMENSIONS OF HEADS
(Standard Wood Screws)



Num- ber of	A Dia.		Flat	Head			Round	Head	
Screw Gauge	in ins.	В	C	E	F	В	С	E	F
0	.0578	.1105	.0303	.025	.0101	.1060	.0524	.025	.0314
1	.0710	.1368	.0378	.027	.0126	.1302	.0598	.027	.0359
2	.0842	. 1631	.0454	.030	.0151	.1544	.0672	.030	.0403
3	.0973	.1894	.0530	.032	.0177	.1786	.0746	.032	.0448
4	.1105	.2158	.0605	.034	.0202	.2028	.0820	.034	.0492
5~	.1236	.2421	.0681	.036	.0227	.2270	.0894	.036	.0536
6	.1368	.2684	.0757	.039	.0252	.2512	.0968	.039	.0580
7	. 1500	.2947	.0832	.041	.0277	.2754	.1042	.041	.0625
8	.1631	.3210	.0908	.043	.0303	.2996	.1116	.043	.0670
9	.1763	.3474	.0984	.045	.0328	.3238	.1190	.045	.0714
10	. 1894	. 3737	1059	.048	.0353	.3480	.1264	.048	.0758
11	.2020	.4000	.1135	.050	.0378	.3701	.1338	.050	.0803
12	.2158	.4268	.1210	.052	.0403	.3922	.1412	.052	.0847
13	.2289	.4526	.1286	.054	.0429	.4143	.1486	.054	.0891
14	.2421	.4790	.1362	.057	.0454	.4364	.1560	.057	.0936
15	.2552	.5053	.1438	.059	.0479	.4585	.1634	.059	.0980
16	.2684	. 5316	. 1513	.061	.0504	.4806	.1708	.061	.1024
17	.2816	. 5579	.1589	.063	.0530	.5027	.1782	.063	.1069
18	.2947	. 5842	.1665	.066	.0555	.5248	. 1856	.066	.1114
20	.3210	.6368	.1816	.070	.0605	.5690	.2004	.070	.1202
22	.3474	.6865	. 1967	.075	.0656	.6106	.2152	.075	.1291
24	.3737	.7421	.2118	.079	.0706	. 6522	.2300	.079	.1380
26	.4000	.7948	.2270	.084	.0757	.6938	.2448	.084	.1469
28	.4263	.8474	.2421	.088	.0807	.7354	.2596	.088	.1558
30	.4526	.9000	.2573	.093	.0858	.7770	.2744	.093	.1646

[Am. Screw Co., Prov., R. I.]

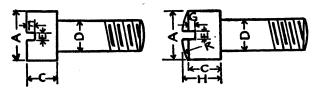
# **FASTENINGS**

DIAMETER AND LENGTH (Standard Wood Screws)

8	.452	884400 24 24
88	.426	88 44 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
98	8	884400 72 72
22	.374	999964400 444 x x
22	347	2149999644400 XX XXX X X
82	.321	77% XXX X X X
81	284	HANN ANN N N
17	.281	
16	268	24% <del>44%</del> 44% <del>4</del> 4
15	.255	7.7% 7.7% 7.7% X
14	242	24% 44% 44% X X
12	228	XXX XXX XXX X
12	.215	ZZZ ZZZ ZZZ Z
11	203	2,72,72,82,22,22,22,22,22,22,22,22,22,22,22,22
2	189	Z ZZZ ZZZ ZZZZ
6	.176	2222 ZZZ 222X
oc o	.163	**************************************
2	.150	LARKE LING
9	.136	7.72.27. 7.72.20 2.72.27.27.27.27.27.27.27.27.27.27.27.27
20	.123	ZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZ
4	110	**************************************
8	760.	72/2/2/2/2/2/2/2/2/2/2/2/2/2/2/2/2/2/2/
69	98.	7.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2
-	120:	7.2.7.2
0	.057	74%
Number of Screw Gauge.	Diameter, ins	Length, ins

For dimensions of heads, see page 44. Wood screws are sold by the gross.

CAP SCREWS



FLAT FILLISTER OR ROUND HEAD

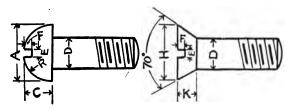
OVAL FILLISTER HEAD

D and C	A	Threads per in.	E	F	G	н	R
1/8	3/16	40	.032	1/16	5/64	964	1/4
<sup>3</sup> /16	1/4	24	.040	1/16	3/82	7/22	<sup>5</sup> /16
1/4	3/8	20	.064	1/16	3/52	% <sub>2</sub>	1/2
5/16	7∕16	18	.072	5/64	1/8	<sup>23</sup> /64	5/8
3/8	<sup>9</sup> /16	16	.091	8/52	964	15/82	3⁄4
<sup>7</sup> ⁄16	5⁄8	14	. 102	7%4	11/64	1/2	₹8
1/2	3/4	13	.114	1/8	<sup>8</sup> /16	9/16	11/16
9/16	<sup>13</sup> /16	12	.114	964	7/52	41/64	11/8
5/8	. <b>⅓</b> 8	11	.128	5/82	15/64	45/64	11/4
3⁄4	1	10	. 133	<sup>3</sup> ⁄16	%2	27/32	11/2
1∕8	11/8	9	. 133	7/32	<sup>21</sup> /64	63/64	15/8
1	11/4	8	165	1/4	3/8	11/8	13/4

### SQUARE AND HEXAGON HEADS

Dia. of screw	1/4	5/16	3/8	7/16	1/2	9/16	5/8	3/4	7/8	1	11/8	11/4
Dia. of sq. head	3/8	7/16	1/2	9/16	5/8	11/16	3/4	7/8	11/8	11/4	13/8	11/2
Dia. of hex. head	7/16	1/2	9/16	5/8	3/4	13/16	7/8	1	11/8	11/4	13/8	$1\frac{1}{2}$
Height of sq. and hex. heads	1/4	5/16	3/8	7/16	1/2	9/6	5/8	3/4	7/8	1	11/8	11/4

CAP SCREWS-Continued



BUTTON HEAD

FLAT OR COUNTERSUNK HEAD

D	A	С	E	F	R	н	K
1/8 3/6 1/4 5/6 3/8 1/2 9/6 5/8 3/4	7,52 5,16 7,16 9,16 9,16 13,16 15,16 1	7.64.53.53.55.55.55.55.55.55.55.55.55.55.55.	.035 .051 .072 .091 .102 .114 .114 .114 .133 .133	364 1/16 84 852 764 11/6 11/6 11/6 3/2 11/6 3/2 3/2 11/6 3/2 3/2 3/2 3/2 3/2 3/2 3/2 3/2 3/2 3/2	7.64.53.23.25.53.25.25.8 7.9.52.65.85.33.23.25.8 18.15.12.25.8	14 38 15 22 58 34 13 16 7/8 1 1 1/8 1 3/8	3/52 9/54 5/52 17/54 17/54 17/54 5/66 23/54 7/16

On all screws of 1 inch and less in diameter, and 4 inches long and under, threads are cut three quarters of the length. Longer than 4 inches, threads are cut one-half of length. Cap screws are also made with hexagon heads. For number of threads per inch, see table, page 46.

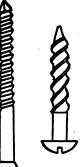
[Atlas Bolt & Screw Co., Cleveland, Ohio.]

### HANGER SCREWS



Dias. 3%", 7/6", 1/2", 5%", 3/4", 7/8," 1". Overall lengths from 21/2" up, advancing by 1/2".

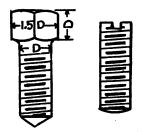
DRIVE SCREWS



DIMENSIONS OF FLAT, ROUND AND OVAL HEADS

Number of screw gauge	<b>.4</b>	2	9	2	8	6	10	11	12	13	14	15	16	18	ଛ
Diameter, ins	.110	.123	.136	.150	.163	.176	.189	.203	.215	. 228	.242	.255	.268	.294	321
Length, ins	**************************************	**************************************	KAKA KKA KKA	HEAR AND AND	77.000 77.00 77.00 7.00 7.00 7.00 7.00	77.77 74.4 74.4 7.	77.77. 77.7 77.7 X	XXXX XXX XXX X	KANA AKA X	22/2 24/2 24/2 2/)	***** **** **** **	7% 727 727 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	. %%" ¼¼%" ¼¼% %	_ <u> </u>	

## SET SCREWS



# SQUARE HEADLESS HEAD

D = dia. of screw.

Dia. of screw	1/4	5/16	3/8	1/18	1/2	%	5/8	34	3/8	1	11/6	11/4
Threads per inch	20	18	16	14	12 or 13	12	11	10	9	8	7	7

May be obtained with conical, dog, oval, cup or flat points. See page 42.

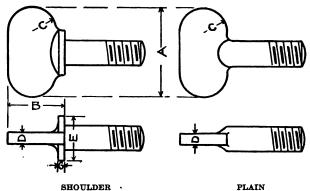
## SAFETY OR SOCKET SET SCREWS



Dias in ins.	Length ins.	U. S. Standard Threads per in.
1/4	5/16	20
6/8	5/16 or 3/8	18
3/8	878 " 1/2	16
7/16	716 " 1/2	14
1/2	1/2 " 5/8	13
9/16	9/6	12
5/8	5/8 " 3/4 3/4 " 1	11 10
1 8	1 " 1½ 1 " 1¼	9. 8

[Hartford Mach. Screw Co., Hartford, Conn.]

THUMB SCREWS



ULDER · PI

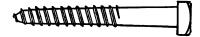
Dia.	Threads per inch	A	В	С	D	E*	G*
3 16 14 5 16 8 8 7 16 1 2	24 20 18 16 14	$ \begin{array}{c}                                     $	1/2 5/8 3/4 7/8 1 1 1/8	3/6 1/4 5/6 3/8 7/6 1/2	1/8 1/8 3/16 3/16 1/4	3/7/9/5/8/4/8	3/22 3/22 1/8 1/8 1/8

 $<sup>\ ^{*}</sup>$  E and G apply only to shoulder thumb screws.

LENGTH OF SCREWS

Dia.				Len	igth			
\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	1/2 1/2 1/2 1/2 1/2 1/2	3/4 3/4 3/4 	1 1 1 1 1	1 1/4 1 1/4 1 1/4 1 1/4 1 1/4 1 1/4	1½ 1½ 1½ 1½ 1½ 1½ 1½	2 2 2 2 2 2	21/2 21/2 21/2 21/2 21/2 21/2	3 3 3

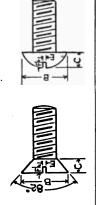
## COACH OR LAG SCREWS .



Cone or gimlet points. Screws with gimlet points can be obtained from  $\frac{5}{6}$  to  $\frac{3}{4}$  dia. Square or hexagon heads.

App				iches)	erew (Ir	ter of So	Diame			
len of the for	11/4	11/8	1	<b>₹8</b>	34	%6 & 5/8	1/2	7/16	3/8	4 ± 5/18
dia et			s)	inche	to poin	er head	th unde	Leng		
To 1 22 22 33 44 44 55 66 66 77 77	6 6½ 7 7½ 8 9 10 11	5 5½ 6 6½ 7½ 8 9 10 11	3½ 4½ 5 5½ 6½ 7 7½ 8 9 10	3 3 4 4 5 5 5 6 7 7 8 9 10 11 12	21/3 31/4 41/4 55/4 66/4 77/4 8 9 10 11 12	2 2 3 3 4 4 4 5 5 6 6 7 7 7 8 9 10 11 12	1½ 2½ 3 ½ 4½ 5 5½ 6½ 7 7 ½ 9 10 11 12	11/2 22/2 31/2 41/2 55/2 66/7 77/8 9	1½ 2 ½ 3 3½ 4 4½ 5 5½ 6	1½ 2 2½ 3 3½ 4 4½ 55½ 6
					er inch	hreads p	T			·····
	3	3	3	41/2	41/2	5	6	7	7	10
			n)	hexago	are and	ups) sb	e of hea	Size		
Wic acre fla	17/8	111/16	11/2	15/16	11/8	27/42 15/16	*	31/42	%6	15/52
Thi ne	15/16	27/62	3/4	21/2	%	2764 1565	3/8	21,64	%	16 15/4

STANDARD MACHINE SCREWS-DIMENSIONS



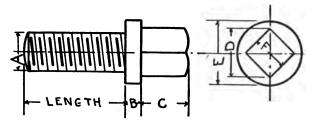
Number	Diameter		Flat Head	Head			Round Head	Head			Fill	Fillister Head	79	ļ
or Screw Gauge	Inches	В	၁	E	H	В	သ	E	F	В	υ	Å	田	<b>F</b>
G	0649	1901	20.00	080	1310	1544	0879	080	0400	1950	933	1	8	
9 03	.0973	1894	.0530	88	0177	1786	.0746	88	2448	1561	983	0.120	35	888
4	.1105	.2158	.0605	.034	.0202	2028	.0820	8.	.0492	.1772	0720	0166	8	44.5
10	.1236	.2421	.0681	.036	.0227	.2270	.089 <del>4</del>	88	.0536	1984	9080	0186	980	9640
9	.1368	.2684	.0757	680	.0252	.2512	8960	68	0280	.2195	.0892	.0205	8	0549
_	.1500	.2947	.0832	25.	.0277	.2754	1042	3	.0625	2408	8260	.0225	8	0602
00 (	.1631	3210	8060	550	8080	2006	1116		.0670	.2617	.1063	.0245	.043	.0654
<del>တ</del> ဂု	.1763	.3474	488	550	.0328	3238	1190	.045	.0714	. 2828	.1149	.0265	.045	.0707
29	1894	.3737	600	85.0	5655	3480	1204	840	.0758	9040	.1235	.0285	.048	.0460
2;	8012.	.4203	1210	200	3	3877	. 1412	720	25.	3462	.1407	.0324	.052	9880
4.5	12421	.4790	1302	3	, 5, 5,	4304	0901	.057	9860.	3888	1578	.0364	.057	.0971
99	2009	0190.	1010	188	500	1200	2021	38	1024	.4307	1750	.0403	8	.1077
96	2010	2828	9191	38	98	5800	0001	98	1004	67.7	1921	2443	8	.1182
38	3474	895	1967	27.2	989	2019	9159	27.5	1001	20102	5000	36	5	1288
12	3737	7421	2118	620	9020	6522	2300	8	380	200	2436	566	200	1001
28	4000	.7421	. 1967	<b>8</b> 6	9990	.6938	.2448	180	1469	6419	2808	090	8	1805
88	.4263	.7948	.2118	880.	9020	.7354	.2596	888	.1558	.6841	2779	1490	88	1710
ଛ	.4526	.8474	.2270	.093	.0757	.7770	.2744	.093	. 1646	.7264	.2951	.0681	86	1816
1		2	1		- 17		-							ĺ

D\* = round of head. F\* = depth of slot. For threads per inch and size of drill see page 53.

STANDARD MACHINE SCREW—THREADS PER INCH AND SIZE OF DRILL

Screw	Dia. of body ins.	Threads per in.	No. of drill	Size of drill ins.	Screw Gauge	Dia. of body ins.	Threads per in.	No. of drill	Size of drill ins.
2 3 4 5 6 7 8 9 10 12	.0842 .0973 .1105 .1236 .1368 .1500 .1631 .1763 .1894 .2158	48, 56, 64 48, 56 32, 36, 40 32, 36, 40 30, 32, 36 30, 32, 36 24, 30, 32 24, 30, 32 20, 24	42 38 35 30	.0730 .0820 .0935 .1015 .1100 .1285 .1360 .1440 .1495 .1730	14 16 18 20 22 24 26 28 30	.2421 .2684 .2947 .3210 .3474 .3737 .4000 .4263 .4526	18, 20, 24 16, 18, 20 16, 18, 20 16, 18 16, 18 14, 16, 18 14, 16 14, 16 14, 16	13 6 1 D J N P R U	. 1850 . 2040 . 2280 . 246 . 277 . 302 . 323 . 339 . 368

# COLLAR SCREWS

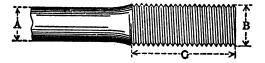


A	Threads per in.	В	С	D	E	F
5/6 3/8 7/6 1/2 5/8 3/4 7/8 1 1/4	18 16 14 13 11 10 9 8 7	964 5542 11/4 3/16 7/22 1/4 9/22 5/16 11/32 8	7/65 1/22 9/66 5/8 3/4 1 1/8 11/4 13/8	2764 3364 1952 11/16 5564 31/52 15/52 13/6 13564	17,32 5,6 23,32 13,16 1 1,13,16 1,3,6 1,9,16 1,3,4 1,15,16	5/6 3/8 7/6 1/2 5/8 3/4 7/8 1 1 1/8 1 1/4

[Cincinnati Bickford Tool Co., Cincinnati, Ohio]

Lengths from  $\frac{3}{4}$ " to  $6\frac{1}{2}$ " advancing by  $\frac{1}{4}$ ".

# UPSET SCREW ENDS FOR ROUND BARS

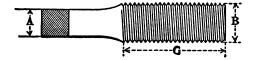


Diameter of Bar	Area of Body of Bar	Diam- eter of Screw	Length of Upset	Area at Root of Thread	Number of Threads per Inch	per	Add for Upset	Excess of Area at Root of Thread over that of
A	Dar	В	С	Inread	Inen	Dar		Body of Bar
Inches	Sq. Ins.	Inches	Inches	Sq. Ins.		Pounds	Inches	Per Cent
1/2 9/16 5/8 11/16	.196 .249 .307 .371	3/4 3/4 7/8	41/4 41/4 41/2 41/2	.302 .302 .420 .550	10 10 9 8	.668 .845 1.043 1.262	414	54 21 37 48
3/4 13/16 7/8 15/16	.442 .519 .601 .690	1 1½ 1¼ 1¼ 1¼	4½ 4¾ 4¾ 4¾ 4¾ 4¾	.550 .694 .893 .893	8 7 7 7	1.502 1.763 2.044 2.347		25 / 34 49 29
$1\\1^{1}_{16}\\1^{1}_{8}\\1^{3}_{16}$	.785 .887 .994 1.108	$1\frac{3}{8}$ $1\frac{3}{8}$ $1\frac{1}{2}$ $1\frac{1}{2}$	5 5 5 5	1.057 1.057 1.295 1.295	6 6 6	2.670 3.014 3.379 3.766	41/4	35 19 30 17
$1\frac{1}{4}$ $1\frac{5}{16}$ $1\frac{3}{8}$ $1\frac{7}{16}$	1.227 1.353 1.485 1.623	$1\frac{5}{8}$ $1\frac{3}{4}$ $1\frac{3}{4}$ $1\frac{7}{8}$	51/4 51/4 51/4 51/2	1.515 1.744 1.744 2.048	5½ 5 5 5	4.173 4.600 5.049 5.518	4½ 5 4 4¾	23 29 18 26
$1\frac{1}{2}$ $1\frac{9}{16}$ $1\frac{5}{8}$ $1\frac{11}{16}$	1.767 1.918 2.074 2.237	2 2 2½ 2½ 2½	5½ 5½ 5¾ 5¾ 5¾	2.302 2.302 2.650 2.650	4½ 4½ 4½ 4½ 4½	6.008 6.520 7.051 7.604	51/4 41/2 5 41/4	30 20 28 18

# UPSET SCREW ENDS FOR ROUND BARS-Continued

Diameter of Bar	Area of Body of Bar	Diameter of Screw	Length of Upset	Area at Root of Thread	Number of Threads per Inch	Weight per Foot of Steel Bar	Add for Upset	Excess of Area at Root of Thread over that of
A		В						Body of Bar
Inches	Sq. Ins.	Inches	Inches	Sq. Ins.		Pounds	Inches	Per Cent
$1\frac{3}{4}$ $1\frac{13}{16}$ $1\frac{7}{8}$ $1\frac{15}{16}$	2.405 2.580 2.761 2.948	$2\frac{1}{4}$ $2\frac{1}{4}$ $2\frac{3}{8}$ $2\frac{1}{2}$	5 <sup>3</sup> / <sub>4</sub> 5 <sup>3</sup> / <sub>4</sub> 6 6	3.023 3.023 3.419 3.715	41/2	8.178 8.773 9.388 10.020	48/4 4 41/2 5	26 17 24 26
$2 \\ 2\frac{1}{16} \\ 2\frac{1}{8} \\ 2\frac{3}{16}$	3.142 3.341 3.547 3.758	$2\frac{1}{2}$ $2\frac{5}{8}$ $2\frac{5}{8}$ $2\frac{3}{4}$	6 6½ 6¼ 6¼ 6¼	3.715 4.155 4.155 4.619	4 4 4	10.68 11.36 12.06 12.78	4½ 4¾ 4 4½	18 24 17 23
$2\frac{1}{4}$ $2\frac{5}{16}$ $2\frac{3}{8}$ $2\frac{7}{16}$	3.976 4.200 4.430 4.666	27/8 27/8 3 31/8	$6\frac{1}{2}$ $6\frac{1}{2}$ $6\frac{1}{2}$ $6\frac{1}{2}$ $6\frac{3}{4}$	5.108 5.108 5.428 5.957		13.52 14.28 15.07 15.86	5½ 4½ 4¾ 5½	28 22 23 28
$2\frac{1}{2}$ $2\frac{9}{16}$ $2\frac{5}{8}$ $2\frac{11}{16}$	4.909 5.157 5.412 5.673	3½ 3¼ 3¼ 3¼ 3¾ 3%	634 634 634 7	5.957 6.510 6.510 7.087	31/2	16.69 17.53 18.40 19.29	43/4 51/4 41/2 5	21 26 20 25
$2\frac{3}{4}$ $2^{13}$ $16$ $2\frac{7}{8}$ $2^{15}$ $16$	5.940 6.213 6.492 6.777	3 <sup>3</sup> / <sub>8</sub> 3 <sup>1</sup> / <sub>2</sub> 3 <sup>5</sup> / <sub>8</sub> 3 <sup>5</sup> / <sub>8</sub>	7 7 7¼ 7¼ 7¼	7.087 7.548 8.171 8.171		20.20 21.12 22.07 23.04	4½ 4¾ 5¼ 4¾ 4¾	19 22 26 21
3 3½ 3¼ 3¾ 3³/8	7.069 7.670 8.296 8.946	3 <sup>3</sup> / <sub>4</sub> 3 <sup>7</sup> / <sub>8</sub> 4 4 <sup>1</sup> / <sub>8</sub>	7½ 7½ 7½ 7½ 7¾	8.641 9.305 9.993 10.706	3 3	24.03 26.08 28.20 30.42	5 5 <sup>1</sup> / <sub>4</sub> 4 <sup>3</sup> / <sub>4</sub> 4 <sup>3</sup> / <sub>4</sub>	22 21 20 20
$3\frac{1}{2}$ $3\frac{5}{8}$ $3\frac{3}{4}$ $3\frac{7}{8}$	9.621 10.321 11.045 11.793	4 <sup>1</sup> / <sub>4</sub> 4 <sup>1</sup> / <sub>2</sub> 4 <sup>5</sup> / <sub>8</sub> 4 <sup>3</sup> / <sub>4</sub>	8 8 8 <sup>1</sup> ⁄ <sub>4</sub> 8 <sup>1</sup> ⁄ <sub>2</sub>	11.329 12.743 13.544 14.220	23/4 23/4	32.71 35.09 37.56 40.10	4½ 5¼ 5¼ 5¼ 5	18 23 23 21
4	12.566	5	81/2	15.763	21/2	42.73	51/4	25

# UPSET SCREW ENDS FOR SQUARE BARS



Side of Square Bar	Area of Body of Bar	Diam- eter of Screw	Length of Upset	Area at Root of Thread	Number of Threads per Inch	Weight per Foot of Steel Bar	Add for Upset	Excess of Area at Root of Thread Over that of Body of Bar
Inches	Sq. Ins.	Inches	Inches	Sq. Ins.		Pounds	Inches	Per Cent
1/2 9/16 5/8 11/16	.250 .316 .391 .473	3/4 7/8 1	41/4 41/2 41/2 41/2	.302 .420 .550 .550	9	.850 1.076 1.328 1.607		21 33 41 17
3/4 13/16 7/8 15/16	.563 .660 .766 .879	$ \begin{array}{c c} 1\frac{1}{8} \\ 1\frac{1}{4} \\ 1\frac{3}{8} \\ 1\frac{3}{8} \end{array} $	43/4 43/4 5 5	.694 .893 1.057 1.057		1.913 2.245 2.603 2.989	5 5¾	23 35 38 20
$1\\1^{1}_{16}\\1^{1}_{8}\\1^{3}_{16}$	1.000 1.129 1.266 1.410		5 5¼ 5¼ 5¼ 5¼	1.295 1.515 1.515 1.744	$   \begin{array}{c c}     5\frac{1}{2} \\     5\frac{1}{2}   \end{array} $	3.400 3.838 4.303 4.795	$\frac{5\frac{1}{2}}{4\frac{1}{4}}$	29 34 20 24
$1\frac{1}{4}$ $1\frac{5}{16}$ $1\frac{3}{8}$ $1\frac{7}{16}$	1.563 1.723 1.891 2.066	17/8	5½ 5½ 5½ 5½ 5¾	2.048 2.048 2.302 2.650	5 4½	5.312 5.851 6.428 7.026	41/4	31 19 22 28
$1\frac{1}{2}$ $1\frac{9}{16}$ $1\frac{5}{8}$ $1\frac{11}{16}$	2.250 2.441 2.641 2.848	$ \begin{array}{c c} 2\frac{1}{4} \\ 2\frac{3}{8} \end{array} $	53/4 53/4 6 6	2.650 3.023 3.419 3.419	41/2	7.650 8.300 8.978 9.682	$\begin{vmatrix} 4\frac{1}{2} \\ 5 \end{vmatrix}$	18 24 30 20
$1\frac{3}{4}$ $1^{13}/6$ $1\frac{7}{8}$ $1^{15}/6$	3.063 3.285 3.516 3.754	25/8 25/8	6 6¼ 6¼ 6¼ 6¼	3.715 4.155 4.155 4.619	4	10.410 11.170 11.950 12.760	5 4 <sup>1</sup> ⁄ <sub>4</sub>	21 26 18 23

UPSET SCREW ENDS FOR SQUARE BARS-Continued

Side of Square Bar	Area of Body	Diam- eter of Screw	Length of Upset	Area at Root of Thread	Number of	Weight per Foot of Bar	Add for Upset	Excess of Area at Root of Thread
<u>,</u> <b>A</b>	of Bar	<b>B</b>	С		Threads per Inch			Over that of Body of Bar
Inches	Sq. Ins.	Inches	Inches	Sq. Ins.		Pounds	Inches	Per Cent
$2 \\ 2^{1}/6 \\ 2^{1}/8 \\ 2^{3}/6$	4.000 4.254 4.516 4.785	21/8 21/8 3 31/8	$     \begin{array}{c}       6\frac{1}{2} \\       6\frac{1}{2} \\       6\frac{1}{2} \\       6\frac{3}{4}     \end{array} $	5.108 5.108 5.428 5.957	4 4 3½ 3½	13.60 14.46 15.35 16.27	5 4 <sup>1</sup> ⁄ <sub>4</sub> · 4 <sup>1</sup> ⁄ <sub>2</sub> 5	28 20 20 24
$2\frac{1}{4}$ $2\frac{5}{16}$ $2\frac{3}{8}$ $2\frac{7}{16}$	5.063 5.348 5.641 5.941	31/8 31/4 33/8 38/8	634 634 7 7	5.957 6.510 7.087 7.087	3½ 3½ 3½ 3½ 3½	17.22 18.19 19.18 20.20	41/4 48/4 51/4 41/2	18 22 26 19
$2\frac{1}{2}$ $2^{9}$ $16$ $2^{5}$ $2^{11}$ $16$	6.250 6.566 6.891 7.223	3½ 35/8 35/8 33/4	7 7¼ 7¼ 7¼ 7¼	7.548 8.171 8.171 8.641	3½ 3¼ 3¼ 3¾ 3	21.25 22.33 23.43 24.56	$4\frac{3}{4}$ $5\frac{1}{4}$ $4\frac{1}{2}$ $4\frac{3}{4}$	21 24 19 · 20
$2\frac{3}{4}$ $2^{13}$ $16$ $2\frac{7}{8}$ $2^{15}$ $16$	7.563 7.910 8.266 8.629	37/8 37/8 4 41/8	7½ 7½ 7½ 7½ 7½ 7½	9.305 9.305 9.993 10.706	3 3 3	25.71 26.90 28.10 29.34	5½ 4½ 4¾ 5	23 18 21 24
3 ,3½ 3¼ 3¾ 388	9.000 9.766 10.563 11.391	41/8 43/8 41/2 45/8	7¾ 8 8 8¼	10.706 12.087 12.743 13.544	3 2½ 2¾ 2¾ 2¾	30.60 33.20 35.92 38.73	4½ 5¼ 5 5	19 24 21 19
$3\frac{1}{2}$ $3\frac{5}{8}$ $3\frac{3}{4}$ $3\frac{7}{8}$	12.250 13.141 14.063 15.016	47/8 5 51/8 51/4	8½ 8½ 8½ 8¾ 8¾	15.068 15.763 16.658 17.572	$\begin{array}{c} 2\frac{5}{8} \\ 2\frac{1}{2} \\ 2\frac{1}{2} \\ 2\frac{1}{2} \\ 2\frac{1}{2} \end{array}$	41.65 44.68 47.82 51.05	5½ 5¼ 5 4¾	23 20 18 17
4	16.000	5½	9	19.267	23/8	54.40	51/4	20

The weight of steel in round and square bars (pages 54 and 56) is 486.9 lb. per cu. ft. or .28 lb. per cu. in.

#### THREADS FOR BOLTS, NUTS, SCREWS AND PIPE

#### DEFINITIONS

(National Screw Thread Commission, Washington, D. C.)

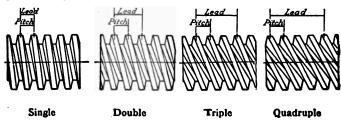
Screw Thread.—A ridge of uniform section wound in the form of a helix on the inside or outside surface of a cylinder or cone.

Screw Helix.—The path of a point moving at a uniform angular rate on a cylindrical or conical surface and at the same time moving at a uniform axial rate.

Major Diameter (formerly known as outside diameter).—The largest diameter of the thread on the screw or nut. The term major diameter replaces the term outside diameter as applied to the thread of a screw and also the term full diameter as applied to the thread of a nut.

Minor Diameter (formerly known as core diameter).—The smallest diameter of the thread on the screw or nut. The term minor diameter replaces the term core diameter as applied to the thread of a screw and also the term inside diameter as applied to the thread of a nut.

Pitch Diameter.—On a straight screw thread the diameter of an imaginary cylinder which would pass through the threads at such points as to make the width of the threads and the width of the spaces cut by the surface of the cylinder equal.



Pitch.—The distance from a point on a screw thread to a corresponding point on the next thread measured parallel to the axis.

 $Pitch = \frac{1}{\text{Number of threads per inch.}}$ 

Lead.—The distance a screw thread advances axially in one turn. On a single thread screw, the lead and pitch are identical; on a double thread screw the lead is twice the pitch, on a triple thread screw the lead is three times the pitch, etc.

Angle of Thread.—The angle included between the sides of the thread measured in an axial plane.

Helix angle.—The angle made by the helix of the thread at the pitch diameter with a plane perpendicular to the axis.

Crest.—The top surface joining the two sides of a thread.

Root.—The bottom surface joining the sixes of two adjacent threads.

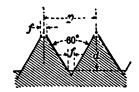
Crest Clearance.—Defined on a screw form as the space between the top of a thread and the root of its mating thread.

Fit.—The relation between two mating parts with reference to ease of assembly, for example:

Wrench fit Close fit Medium fit Loose fit

The quality of fit is dependent upon both the relative size and the quality of finish of the mating parts.

## THREADS FOR BOLTS AND NUTS United States Standard



L

$$p = pitch = \frac{1}{No. \text{ thds. per in.}}$$

$$d = depth = p \times .64952$$

$$f = flat = \frac{p}{8}$$

•			,	Area in Sq	uare Inches	Tensile	Working
Dia.	Dia. No. of Threads Poor of Thread	Dia. of Tap Drill	Bolt	Bottom of Thread	Tensile Strength at Stress of 6000 lbs. per Sq. In.  160 270 410 560 760 1000	Strength at Stress of 6000 lbs. per Sq. In.	
1/4/16/8/8/16/8/16/8/4/8/8/4/8	20 18 16 14 13 12 11 10 9	0.185 0.240 0.294 0.345 0.400 0.454 0.507 0.620 0.731	18,64 1,4 5,16 23,64 27,64 15,52 17,52 41,64 3,4	0.049 0.076 0.110 0.150 0.196 0.248 0.307 0.442 0.601	0.026 0.045 0.068 0.093 0.126 0.162 0.202 0.302 0.419	270 410 560 760	260 680 1210

(Continued on page 60)

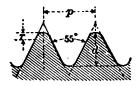
THREADS FOR BOLTS AND NUTS—Continued
United States Standard

				Area in Sq	uare Inches	Tensile	Working
Dia.	Dia. Threads Root of	Dia. at Root of Thread	Dia. of Tap Drill	Bolt B	Bottom of Thread	Strength at Stress of 6000 lbs. per Sq. In.	Strength at Stress of 6000 lbs. per Sq. In.
1 11 15 15 15 15 15 15 15 15 15 15 15 15	876665554414 4433114 (848)812188	0.838 0.939 1.064 1.158 1.283 1.389 1.490 1.615 1.711 1.961 2.175 2.425 2.629 2.879 3.100 3.317 3.567 4.028 4.028 4.255 4.480 4.730 4.953 5.203	55,25,25,25,25,25,25,25,25,25,25,25,25,2	0.785 0.994 1.227 1.485 1.767 1.074 2.405 2.761 3.142 3.976 4.909 5.940 7.069 8.296 9.621 11.045 12.566 14.186 14.186 15.904 17.721 19.635 21.648 23.758 23.758 23.758	0.551 0.694 0.893 1.057 1.295 1.515 1.746 2.051 2.302 3.023 3.719 4.602 5.428 6.510 7.548 8.641 9.963 11.340 12.750 14.215 15.760 17.570 19.260 21.250	3300 4160 5350 6340 7770 9090 10470 12300 13800 18100 22300 27700 32500 39000 45300 51800 59700 68000 76500 85500 94000 116000 116000 127000	1790 2470 3470 4260 5500 6630 7830 9470 10800 14700 18500 23600 28000 45000 50100 55000 74000 82500 93000 103000 114000
6	21/4	5.423	51/2	28.274	23.090	138000	124000

Tap drill sizes given provide for a slight clearance at the root of thread to facilitate tapping and reduce tap breakage. Where full threads are required use the diameters specified for root of thread.

$$p = pitch = \frac{1}{Number of threads per in.}$$
  
 $d = depth = p \times .866$ 

Whitworth Threads
(Standard in Great Britain)



$$p = pitch = \frac{1}{Number of threads per in.}$$

$$d = depth = p \times .64033$$

$$r = radius = p \times .1373$$

Diameter Ins.	Threads per in.	Diameter at Root of Thread	Radius	Diameter Ins.	Threads per Inch	Diameter at Root of Thread	Radius
1/4 5/16 3/8 7/16	20 18 16 14	.186 .241 .295 .346	.0069 .0076 .0086 .0098	17/8 2 21/4 21/2	4½ 4½ 4 4	1.590 1.715 1.930 2.180	. 0305 . 0305 . 0343 . 0343
1/2 9/16 5/8 3/4	12 12 11 10	.393 .456 .508 .622	.0114 .0114 .0125 .0137	$2\frac{3}{4}$ $3\frac{1}{4}$ $3\frac{1}{2}$	3½ 3½ 3½ 3¼ 3¼	2.384 2.634 2.856 3.105	.0393 .0393 .0422 .0422
7/8 1 11/8 11/4	9 8 7 7	.732 .840 .942 1.067	.0152 .0176 .0196 .0196	3 <sup>3</sup> ⁄ <sub>4</sub> 4 4 <sup>1</sup> ⁄ <sub>2</sub> 5	3 3 2 <sup>7</sup> / <sub>8</sub> 2 <sup>3</sup> / <sub>4</sub>	3.320 3.573 4.0546 4.5343	.0458 .0458 .0477 .0499
$1\frac{3}{8}$ $1\frac{1}{2}$ $1\frac{5}{8}$ $1\frac{3}{4}$	6 6 5 5	1.161 1.286 1.368 1.494	.0229 .0229 .0275 .0275	5½ 6	$2\frac{5}{8}$ $2\frac{1}{2}$	5.0121 5.48 <b>7</b> 7	. 0523 . 0549

British Standard Fine Threads

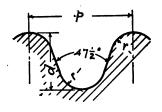
British standard fine threads have the same form as Whitworth,

but in the British there are more threads per inch.

Dia.	Threads per in.	Dia.	Threads per in.	Dia.	Threads per in.
1/4 9/12 5/16 3/8 7/16	26 26 22 22 20 18 16	916 5 8 1116 34 18,6	16 14 14 12 12 12	1 1 <sup>1</sup> / <sub>8</sub> 1 <sup>1</sup> / <sub>4</sub> 1 <sup>3</sup> / <sub>8</sub> 1 <sup>1</sup> / <sub>2</sub>	10 9 9 8 8

#### British Association Standard Thread (B. A. S.)

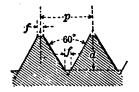
(Used for small screws)



$$r = \frac{2p}{11} d = .6p$$

Brit. Ass'n	• Di	a.	Pit	ch Dia. at			Dia.		Pitch		Dia. at root of
Num- ber	Ins.	Mm.	Ins.	Mm.	thread Mm.	Num- ber	Ins.	Mm.	Ins.	Mm.	thread Mm.
0 .	236	6.0	.0394	1.00	4.8	13	.047	1.20	.0098	.25	.90
1  .	209	5.3	. 0354	.90	4.22	14		1.00	.0091.	.23	.72
2 .	. 185	4.7	.0319	.81	3.73	15	. 035	.90	.0083	.21	.65
3  .	. 161	4.1	.0287	.73	3.22	16	.031	.79	.0075	.19	.56
4 .	. 142	3.6	.0260	.66	2.81	17	.028	.70	.0067	.17	.50
5 .	.126	3.2	.0232	.59	2.49	18	. 024	.62	.0059	.15	.44
6  .	.110	2.8	.0209	.53	2.16	19	.021	,54	.0055	.14	.37
7 .	.098	2.5	.0189	.48	1.92	20	.019	.48	.0047	.12	.34
	.087	2.2	.0169	.43	1.68	21	.017	.42	.0043	.11	.29
	.075	1.9	.0154	.39	1.43	22	.015	.37	.0039	.10	.25
10  .	.067	1.7	.0138	.35	1.28	23	.013	.33	.0035	.09	.22
	.059	1.5	.0122	.31	1.13	24	.011	.29	.0031	.08	.19
12  .	.051	1.3	.0110	,28	.96	25	.010	.25	.0028	.07	.17

#### French (Metric) Standard Thread



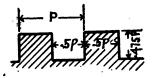
p = pitch

 $f = flat = \frac{p}{8}$ 

 $d = depth = p \times .64952$ 

Diameter	Pitch	Diameter	Pitch	Diameter	Pitch
Mm.	Mm.	Mm.	Mm.	Mm.	Mm.
3 4 5 6 7 8 9 10 12 14	0.5 0.75 0.75 1.0 1.0 1.0 1.5 2.0	16 18 20 22 24 26 28 30 32 34	2.0 2.5 2.5 2.5 3.0 3.0 3.5 3.5	36 38 40 42 44 46 48 50 52 56	2.0 4.0 4.5 4.5 4.5 5.0 5.0 5.5

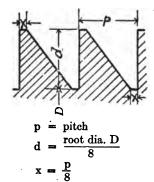
#### Sellers Square Thread



p = pitch

Dia. Ins.	Threads per in.	Dia. root of thread	Dia. Ins.	Threads per in.	Dia. root of thread	Dia. Ins.	Threads per in.	Dia. root of thread
1/4 5/16 8/8 7/16 1/2	10 9 8 7 6½ 6	.162 .215 .265 .312 .365 .416	5/8 11/16 3/4 18/16 7/8 15/16	5½ 5 5 4½ 4½ 4½	.466 .512 .575 .618 .680 .718	1 1½ 1¼ 1¾ 13% 1½ 15%	4 3½ 3½ 3 3 2¾	.781 .875 1.000 1.083 1.208 1.307

#### Buttress Thread

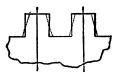


Buttress thread takes load in one direction.

#### Acme Thread

# f-J-P----

Comparison of Acme and Square Threads.



$$p = pitch$$
  
 $d = depth = .5p + .01 in.$ 

flat top f = .3707pflat bottom = .3707p - .0052 in.

Number of Threads per In.	Pitch of Single Thread	Depth of Thread	Width at Top of Thread	Width at Bottom of Thread	Space at Top of Thread	Thickness at Root of Thread
1	1.000	.5100	.3707	.3655	.6293	.6345
1 <sup>1</sup> / <sub>3</sub>	.750	.3850	.2780	.2728	.4720	.4772
2	.500	.2600	.1853	.1801	.3147	.3199
3	.333	.1767	.1235	.1183	.2098	.2150
4	.250	.1350	.0927	.0875	.1573	.1625
5	.200	.1100	.0741	.0689	.1250	.1311
6	.166	.0933	.0618	.0566	.1049	.1101
7	.142	.0814	.0529	.0478	.0899	.0951
8	.125	.0725	.0463	.0411	.0787	.0839
9	.111	.0655	.0413	.0361	.0699	.0751

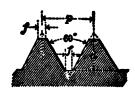
#### S. A. E. Standard Thread

Society of Automotive Engineers (S. A. E.) standard thread has the United States standard form, but has more threads per inch.

$$p = pitch = \frac{1}{n}$$

$$d = depth = p \times .6495 = \frac{.6495}{n}$$

$$f = flat = \frac{p}{8}$$



Diameter Ins.	Decimal Equivalent Outside Diameter	Threads per Inch	Basic Pitch Diameter	Root Diameter	(d) Depth of Thread .6495 n
1/4 5/16 3/8 7/16 1/2 9/16 5/8 11/16 3/4 7/8 1	.250 .3125 .375 .4375 .500 .5625 .625 .6875 .750 .8750 .8750 .8751	28 24 24 20 20 18 18 16 16 14 18 12	.2269 .2855 .3480 .4050 .4675 .5264 .5889 .6469 .7094 .8286 .8389 .9536	.2038 .2585 .3210 .3725 .4350 .4903 .5528 .6063 .6688 .7822 .8028 .9072	.0231 .0270 .0270 .0325 .0325 .0361 .0361 .0406 .0406 .0464 .0361
1 1 4 1 3 8 1 1 2	1.250 1.375 1.500	12 12 12 12	1.1959 1.3209 1.4459	1.1418 1.2668 1.3918	.0541 .0541 .0541

Threads Recommended by National Screw Thread Commission, Washington, D. C.

[1919-1920]

Symbols.—For using formulæ for expressing relations of screw threads and for use on drawings the following list should be used. For definitions see page 58

or dennitions see page 58	
Major diameter	Ð
(corresponding radius)	d
Pitch diameter	E
(corresponding radius)	е
Minor diameter	<b>K</b> .
(corresponding radius)	k
Angle of thread	<b>A</b> .
(One-half angle of thread)	a
Number of turns per inch	N
" "threads " "	n
Lead	$P = \frac{1}{N}$
Pitch or thread interval	$p = \frac{1}{n}$
Helix angle	8
Tangent of helix angle	$S = \frac{P}{3.1416 \times E}$
Width of basic flat at top, crest or root	$\mathbf{F}$
Depth of basic truncation	f
" " sharp V thread	H
" " National (U.S.) form of thread	h
Included angle of taper	Y
(One-half included angle of taper)	<b>y</b>
PDS 3 1 A 13 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	

The basis of the system is the initial letters of the series, preceded by the diameter in inches (or the screw number) and number of threads per inch, all in Arabic characters, followed by the classification of fit in Roman numerals.

Examples Mark
National Coarse Thread System. To specify a threaded part 1 inch diameter, 8 threads per inch, Class one fit.
National Fine Thread System. Threaded 1"—14—NF—III part 1" diameter, 14 threads per inch, Class three fit.

Threads Recommended by National Screw Thread Commission, Washington, D. C.—Continued

#### [1919-1920]

National Form, Special Pitch. Threaded 1"—12—N—IV part 1" diameter, 12 threads per inch, Class four fit.

Form of Thread.—The national form of thread profile, known previously as the United States Standard or Sellers' Profile, is recommended by the Commission (National Screw Thread Commission, Washington, D. C.) and shall hereafter be known as the National Form of Thread.

- a. Where Used.—The national form shall be used for all screw thread work except when otherwise specified for special purposes.
- b. Specifications.—The basic angle of thread (A) between the sides of the thread measured in an axial plane shall be 60 degs. The line bisecting this 60 deg. angle shall be perpendicular to the axis of the screw thread.

The basic flat at the root and crest of the thread form will be  $\frac{1}{8} \times p$ . The basic depth of the thread form will be .649519  $\times p$  =  $\frac{.649519}{}$ 

Where p = pitch in inches.

n = number of threads per inch.

c. Clearance in Nut.—(1) Clearance at minor diameter.—A clearance shall be provided at the minor diameter of the nut by removing the thread form at the crest by an amount equal to ½ to ¼ of the basic thread depth. (2) Clearance at major diameter.—A clearance at the major diameter of the nut shall be provided by decreasing the depth of the truncation triangle by an amount equal to ½ to ½ of its theoretical value.

Thread Series Recommended.—National Coarse Threads and National Fine Threads. The National Coarse Threads (see Table 1) are recommended for general use in engineering work, in machine construction where conditions are favorable to the use of bolts, screws and other threaded components where quick and easy assembly of the parts is desired, and for all work where conditions do not require the use of fine pitch threads.

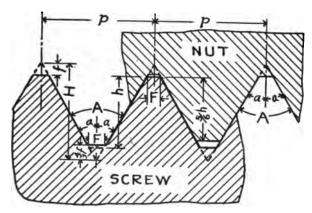
TABLE 1-NATIONAL COARSE THREAD SERIES

Identifi	cation	Basi	c Diamet	ers	,	Thread Data	
1	2	3	4	5	6	7	8
Num- bered and Frac-	n Number of Threads	D Major Dia.	E Pitch Dia.	K Minor Dia.	Metric Equivalent of Major Dia.	p Pitch	h Depth of Thread
tional Sizes	per In.	In.	In.	In.	Mm.	In.	In.
1 2 3 4 5	64 56 48 40 40		0.0958		2.184 2.515 2.845	0.0156250 0.0178572 0.0208333 0.0250000 0.0250000	0.0116 0.0135
6 8 10 12	32 32 24 24	0.138 0.164 0.190 0.216	0.1437 0.1629	0.0974 0.1234 0.1359 0.1619	4.826	0.0312500 0.0312500 0.0416667 0.0416667	0.0203 0.0203 0.0271 0.0271
14 5 16 3 8 7 16 12	20 18 16 14 13	0.3125 0.3750 0.4375	0.2175 0.2764 0.3344 0.3911 0.4500	0.2403 0.2938 0.3447	7.938 9.525	0.0500000 0.055556 0.0625000 0.0714286 0.0769231	0.0361 0.0406
9/16 5/8 3/4 7/8	12 11 10 9 8	0.6250 0.7500 0.8750	0.5084 0.5659 0.6850 0.8028 0.9188	0.5069 0.6201 0.7307	15.88 19.05 22.22	0.0833333 0.0909091 0.1000000 0.1111111 0.1250000	0.0590 0.0650 0.0722
$1\frac{1}{8}$ $1\frac{1}{4}$ $1\frac{1}{2}$ $1\frac{3}{4}$ $2$	7 7 6 5 4½	1.2500 1.5000 1.7500	1.0322 1.1572 1.3917 1.6201 1.8557	1.0644 1.2835 1.4902	31.75 38.10 44.45	0.1428572 0.1428572 0.1666667 0.2000000 0.2222222	0.0928 0.1083 0.0299
$2\frac{1}{4}$ $2\frac{1}{2}$ $2\frac{3}{4}$ $3$	4½ 4 4 4	2.5000 2.7500	2.1057 2.3376 2.5876 2.8376	2.1752 $2.4252$	63.50 69.85	0.2222222 0.2500000 0.2500000 0.2500000	0.1624 0.1624

The National Fine Threads (see Table 2) are recommended for general use in automotive and aircraft work, for use where the de-

sign requires both strength and reduction in weight, and where special conditions require a fine thread, as for instance, on large sizes where sufficient force cannot be secured to set properly a screw or bolt of coarse pitch, by exerting on an ordinary wrench the strength of a man. The form of thread for coarse and fine threads is the same as outlined in the paragraph Form of Thread.

National Form of Thread for Minimum Nut and Maximum Screws



In the figure no allowance is shown. This condition exists in Class II. Medium Fit where both the minimum nut and the maximum screw are basic.

#### Notation

$= 60^{\circ}$	Angle of thread.
= 30°	One-half angle of thread.
$=\frac{1}{n}$	Pitch
=	Number of threads per inch.
= .866025p	Depth of 60° sharp V thread.
= .649519p	" " standard form thread.
= .541266p	
= .125000p	Width of flat at crest and root of standard form.
= .108253p	
= 1/8 H	
= 1/6 h	Depth of truncation.
	= 30° = \frac{1}{n} = = .866025p = .649519p = .541266p = .125000p = .108253p = 1/8 H

TABLE 2-NATIONAL FINE THREAD SERIES

Identif	ication	Basi	c Diamet	ers		Thread Data	
1	2	3	4	5	6	7	8
Num- bered and Frac-	n Number of Threads	D Major Dia.	E Pitch Dia.	K Minor Dia.	Metric Equivalent of Major Dia.	p Pitch	h Depth of Thread
tional Sizes	per In.	In.	In.	In.	Mm.	In.	In.
0 1 2 3 4	80 72 64 56 48	0.060 0.073 0.086 0.099 0.112	0.0519 0.0640 0.0759 0.0874 0.0985	0.0550 0.0657 0.0758	1.524 1.854 2.184 2.515 2.845	0.0125000 0.0138889 0.0156250 0.0178571 0.0208333	0.00902 0.01014 0.01160
5 6 8 10 12	44 40 36 32 28	0.125 0.138 0.164 0.190 0.216	0.1102 0.1218 0.1460 0.1697 0.1928	0.0955 0.1055 0.1279 0.1494	3.175 3.506 4.166 4.826 5.486	0.0227273 0.0250000 0.0277778 0.0312500 0.0357143	0.01476 0.01624 0.01804 0.02030
14 516 3/8 716 1/2	28 24 24 20 20	0.3750 0.4375	0.2268 0.2854 0.3479 0.4050 0.4675	0.2584 0.3209 0.3726		0.0357143 0.0416667 0.0416667 0.0500000 0.0500000	0.02706 0.02706 0.03248
9/6 5/8 3/4 7/8	18 18 16 14 14	0.6250 0.7500 0.8750	0.5264 0.5889 0.7094 0.8286 0.9536	0.5528 0.6688 0.7822	15.88 19.05	0.0555556 0.0555556 0.0625000 0.0714286 0.0714286	0.03608 0.04060 0.04640
11/8 11/4 11/2 18/4 2	12 12 12 12 12 12	1.2500 1.5000 1.7500	1.0709 1.1959 1.4459 1.6959 1.9459	1.1418 1.3918 1.6418	31.75 38.10 44.45	0.0833333 0.0833333 0.6833333 0.0833333 0.0833333	0.05413 0.05413 0.05413
$2\frac{1}{4}$ $2\frac{1}{2}$ $2\frac{3}{4}$ $3$	12 12 12 10	2.5000 2.7500	2.1959 2.4459 2.6959 2.9350	$2.3918 \\ 2.6418$	63.50 69.85	0.0833333 0.0833333 0.0833333 0.1000000	0.05413 0.05413

#### Classification of Fits.

Class I Loose fit Includes screw thread work of rough commercial quality, such as hose couplings, etc.

Class II Medium fit

Subdivision "A" (Regular) Includes the great bulk of screw thread work of ordinary quality of finished and semi-finished bolts and nuts, machine screws, etc.

Subdivision "B" (Special)

Includes the better grade of interchangeable screw thread work, such as high grade automobile and aircraft bolts and nuts.

Class III Close fit Includes screw thread work requiring a fine snug fit, somewhat closer than the medium fit special. In this class of fit selective assembly of parts may be required.

Class IV Wrench fit Subdivision "A"

Includes screw threads used in light sections with moderate stresses, such as aircraft and automobile engine work.

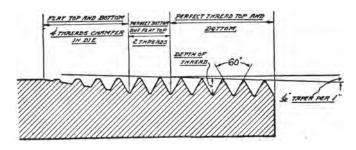
Subdivision "B"

Includes screw threads used in heavy sections with heavy stresses, such as steam engine and heavy hydraulic work.

#### PIPE THREADS

The standard in the United States is the Briggs, and in Great Britain is the Whitworth. In Briggs, the pipe is tapered 1/16 in. per in.

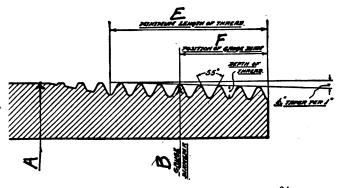
Briggs Pipe Threads



N = number of threads per inch. Depth of thread =  $\frac{.8}{N}$ Length of perfect thread =  $\frac{.8D + 4.8}{N}$  where D represents the actual outside diameter of pipe.

	Pipe Diamet	ters _	Threads	Depth	Length of	Total Length
Nomi- nal Pipe Size	Actual Inside	Actual Outside	per Inch	of Thread	Perfect Threads	of Thread on Pipe
1/8 1/4 1/4 1/4 1/2 2 1/2 3 1/2 4 1/2 5 6 7 8 9	.270 .364 .494 .623 .824 1.048 1.380 1.610 2.067 2.468 3.067 3.548 4.026 4.508 5.045 6.065 7.023 7.982	.405 .540 .675 .840 1.050 1.315 1.660 1.900 2.375 2.875 3.500 4.000 4.500 5.563 6.625 7.625 8.625	27 18 18 14 14 11 11 12 11 12 11 12 8 8 8 8 8 8 8 8 8	.029 .044 .044 •.057 .057 .069 .069 .100 .100 .100 .100 .100	. 19 .29 .30 .39 .40 .51 .54 .55 .58 .89 .95 1.00 1.10 1.16 1.26 1.36 1.46	.412 .624 .630 .819 .831 1.03 1.06 1.07 1.10 1.64 1.70 1.80 1.85 1.91 2.01 2.11
9 10	9.000 10.019	9.625 10.750	8 8	.100 .100	1.57 1.68	$\begin{bmatrix} 2.32 \\ 2.43 \end{bmatrix}$

#### Whitworth or British Standard Pipe Threads



 $N = number of threads per inch. Depth of thread = \frac{.64}{N}$ 

Nom-	A	В			Е	F
inal Bore of Pipe Ins.	Approx. Outside Dia. of Pipe Ins.	Gauge Dia. Top of Thread Ins.	Single Depth of Thread Ins.	Number of Threads per Inch	Length of Thread on Pipe Ins.	Dist. of Gauge Dia. from End of Pipe Ins.
1 1 1 1 2 2 2 2 3 3 3 3 3 3 3 3 3 3 3 3	13.17.18.18.18.18.18.18.18.18.18.18.18.18.18.	.383 .518 .656 .825 .902 1.041 1.189 1.309 1.650 2.116 2.347 2.587 2.960 3.210 3.460 3.700 3.950 4.200	.0230 .0335 .0335 .0455 .0455 .0455 .0580 .0580 .0580 .0580 .0580 .0580 .0580 .0580 .0580 .0580	28 19 14 14 14 11 11 11 11 11 11 11 11	8 8 8 6 6 6 6 7 8 8 8 8 6 8 7 8 8 8 8 8	53 6 4 4 4 8 8 8 8 8 2 2 8 8 6 6 6 6 8 8 8 7 7 7 7 8 8 11 11 13 13 7 7 7 7 8

(Continued on page 74)

15

16

17

18

	A	В			E	F
Nom- inal Bore of Pipe Ins.	Approx. Outside Dia. of Pipe Ins.	Gauge Dia. Top of Thread Ins.	Single Depth of Thread In.	Num- ber of Threads per In.	Length of Thread on Pipe Ins.	Dist. of Gauge Dia. from End of Pipe Ins.
4	416	4.450	.0580	11	15/8	1
41/2	5	4.950	.0580	ii	15/8	١١٠١
5	$4\frac{1}{2}$ $5$ $5\frac{1}{2}$	5.450	.0580	ii	134	11/8
5 <sup>1</sup> / <sub>2</sub> 6 7 8	6 2	5.950	.0580	ii	17/8	l î¼
6 4	61/2	6.450	.0580	ii	2	1 1 4 1 3 8
7	71/2	7.450	.0640	10	21/8	13%
8	81/2	8.450	.0640	10	$2\frac{1}{4}$	11/2
	91/2	9.450	.0640	10	21/4	1 1/2
10	$10\frac{1}{2}$	10.450	.0640	10	23/8	15/8
11	$11\frac{1}{2}$	11.450	.0800	8	$2\frac{1}{2}$	15/8
12	$12\frac{1}{2}$	12.450	.0800	8 8	$2\frac{1}{2}$	15/8
13	1334	13.680	.0800	8	$2\frac{5}{8}$	15/8
14	$14\frac{3}{4}$	14.680	.0800	8	23/4	134

#### Whitworth or British Standard Pipe Threads-Continued

Threads for Pipe and Fire Hose Couplings Recommended by National Screw Thread Commission, Washington, D. C., 1919–1920

.0800

.0800

0800

.0800

8 8 8

The Commission favored the adoption in practically its present shape of the Briggs standard pipe thread size as recommended by the Am. Society of Mechanical Engineers and the fire hose coupling as established by National Fire Protective Association.

#### NATIONAL PIPE THREADS

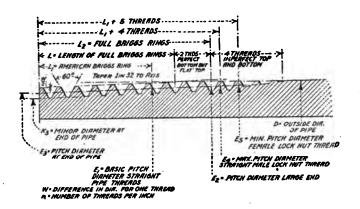
Formulæ for Basic Size. (See Table 3, page 76)

$$\begin{split} L &= \frac{0.8D \, + \, 4.8}{n} & E_3 \, = \, K_3 \, + \, \frac{0.8}{n} \\ K_3 &= D \, = \, \frac{0.05D \, + \, 1.9}{n} & E_2 \, = \, E_3 \, + \, \frac{L_2}{16} \\ E_1 &= E_3 \, + \, \frac{L_1}{16} & w \, = \, \frac{1}{16 \, n} \\ L_2 &= L \, + \, 2 \left( \frac{1}{n} \right) \end{split}$$

15.680

16.680

18.680



### National Fire Hose Coupling Threads. Form of Thread, see page 67.

#### National Fire Hose Couplings

#### Basic Min. Coupling Dimensions

Nom-	Num- ber of	Pitch	Depth of Thread		liameter	Pitch dia.	Minor dia.	Allow-
inal Size	threads per inch	Ins.	Ins.	Mm.	Ins.	Ins.	Ins.	Ins.
2.50 3.00 3.50 4.50	7.5 6.0 6.0 4.0	.13333 .16667 .16667 .25000	.0955 .1243 .1243 .1765	78.550 92.837 108.712 147.320	3.0925 3.6550 4.2800 5.8000	2.9970 3.5307 4.1556 5.6235	2.9015 3.4063 4.0313 5.4470	.03 .03 .03 .05

#### Basic Max. Nipple Dimensions

2.50         7.5         .13333         .0955         77.788         3.0625         2.9670         2.8715           3.00         6.0         .16667         .1243         92.075         3.6250         3.5006         3.3763           3.50         6.0         .16667         .1243         107.950         4.2500         4.1256         4.0013           4.50         4.0         .25000         .1765         146.050         5.7500         5.5735         5.3970
---

TABLE 3-NATIONAL PIPE THREAD SERIES-TAPER, STRAIGHT PIPE THREAD AND LOCK NUT SIZES AND BASIC DIMENSIONS

-			11	Max. Pitch	Min. Pitch					
Depth of Thread		Pitch Dia. at End of Pipe	Dia. at Gauge Notch Basic Straight	Straight Male Lock Nut Thread		Outside Dia. of Pipe	e Thickness Full Briggs Ring	Inches Thickness American Briggs Ring	Pitch Dia. at Large End	Difference in Dia. for One Thread
0.8n	1	E3	Ē	ធី	ž.	Ω	1	ų	E .	A
.0296	<u> </u>	0.3635	0.3748	0.3840	0.3863	0.405	0.2638	0.180	0.3800	0.00232
0.044		0.6120	0.6270	0.6410	0.0444	0.675	0.4078	2.5	0.6375	0.00347
.0571		0.9677	0.9888	1.0067	1.0112	1.050	0.5457	0.33	1.0018	0.00446
9690	_	1.2136	1.2386	1.2604	1.2658	1.315	0.6828	0.400	1.2563	0.00543
9 9 9 9 9 9		1.5571	1.5834	1.6051	1.6106	96	0.7068	0.420	1.8013	0.00543
0.0696		2.2690	2.2963	2.3180	2.3234	2.375	0.7565	0.436	2.3163	0.00543
100		3.3406	3.3885	3.4198	3.4276	3.500	1.2000	0.766	3.4156	0.00781
88		3.8375	3.8888	3.9201	3.9279	4.4 005 005	1.2500	0.821	3.9156	0.00781
888		4.8212	4.8859	4.9172	4.9250	5.000	1.3500	0.875	4.9156	0.00781
3 5		0.300	0.1180	0.4000	0.1001	9000	1.1000	0.85	0.1100	0.00101
38		7.4460	2.5080	7.5340	7.5410	625 7.625	1.5125	200	7.5410	0.00781
98		8.4340	8.500	8.5310	8.5390	8.625	1.7120	1.083	8.5410	0.00781
188	_	10.5450	10.6210	10.6520	10.6600	10.750	1.9250	1.210	10.6660	0.00781
1000		12.5340	,12.6190	12.6500	12.6580	12.750	2.1250	1.360	12.6870	0.00781
38	_	14.7750	13.8730	13.9040	13.9120	14.000	2.2500	1.562	13.9160	0.00781
900		15.7620	15.8760	15.9060	15.9150	18.00	2.4500	1.812	15.9160	0.00781
3	_	000/1	06/8.71	17.9000	17.9140	18.000	2.000	3.5	0018.71	0.000
965		19.7380	19.8700	19.9020	19.9100	88	2.8500	2.125	19.9160	0.00781
38	_	23.7120	23.8610	23.8920	23.9000	25.000.75	3.2500	2.375	23.9160	0.00781

TAP DRILLS
FOR STANDARD PITCH THREADS

	U. 8	s. s.	Whit	worth	8. A	. E.		U. 8	8. 8.	Whit	worth
Thread Diameter	Threads per Inch	Tap Drill Size	Threads per Inch	Tap Drill Size	Threads per Inch	Tap Drill Sise	Thread Diameter	Threads per Inch	Tap Drill Sise	Threads per Inch	Tap Drill Size
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	50 40 32 20 18 16 14 13 11 11 10 9 9 8 7 7 6 6 6	11 4 4 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	48 40 24 20 18 16 14 12 11 10 10 9 8 7 7 6 6 5	13.64 37.64 31.64 35.64 31.62	28 24 20 20 20 18 16 16 	No. 2 a a a a a a a a a a a a a a a a a a	17.6 X 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	55 44 4 4 4 4 3 3 3 3 3 3 3 3 3 3 3 3 3	114 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1772 1772 1772 1772 1772 1772 1772 1772	1 % 1 %

Above Tap Drill Sizes are computed to allow approximately 75% of full thread.

#### NAILS

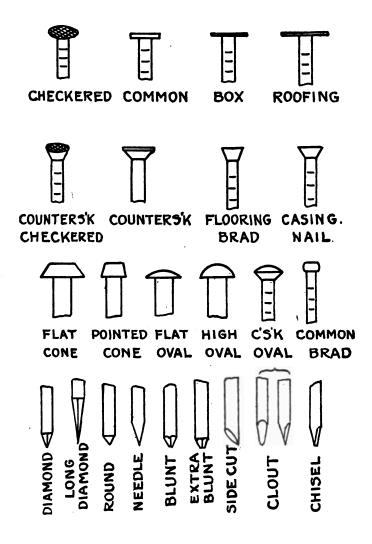
Wire nails have a circular cross section, the steel wire gauge is used for designating their diameter. The length is given in the penny system, the letter d being the selected symbol, thus a

Cut nails have a rectangular cross section, with taper from head to point.

A keg of nails weighs 100 lbs.

Cement coated nails have practically twice the holding power of common wire nails. Cement coated nails (as manufactured by Wickwire Bros., Cortland, N. Y.) are like common nails except in the style of head.

#### NAIL HEADS AND POINTS



COMMON NAILS

Size	Length	Steel Wire Gauge	Approx. No. to Lb.
2d	1 inch	No. 15	876
· 2d 3d 4d 5d 6d	11/2 "	" 121/2	568 316
	134 "	" 12½ " 11½	271 181
7d 8d 9d	21/4 " 21/2 "	" 11½ " 10¼	161 106
10d	234 "	" 10¼ " 9	96 69
12d 16d	31/2 "	" 9 " 8	63 49
<b>20</b> d <b>30</b> d	4 " 4½ "	" 9 " 8 " 6 " 5	31 24
40d <b>50</b> d	5 " 5½ "	" 4 " 3	18 14
<b>60</b> d	6 "	" 2.	11

#### COMMON BRADS

Size	Length	Steel Wire Gauge	Approx. No. to Lb.
2d 3d 4d 5d 6d 7d 8d 9d 10d 12d 16d 20d	Length  1 inch 114 " 112 " 134 " 214 " 214 " 214 " 314 " 314 " 314 "	No. 15 " 14 " 12½ " 12½ " 11½ " 10¼ " 10¼ " 9 " 8 " 6	876 568 316 271 181 161 106 96 69 64 49
30d 40d 50d 60d	41 <sub>2</sub> " 5 " 51 <sub>2</sub> " 6 "	" 5 " 4 " 3 " 2	24 18 16 11

#### FLOORING BRADS

Sizes 6d, 7d, 8d, 9d, 10d, 12d, 16d and 20d have the same length as common brads but average one gauge lighter.

CLINCH NAILS (Flat Oval Head)

Size	Length	Steel Wire Gauge	Approx. No. to Lb.
2d 3d 4d 5d 6d 7d 8d 9d	1 inch 1½ " 1½ " 1¾ " 2 " 2½ "	No. 14 " 13 " 12 " 12 " 11 " 11 " 10	710 429 274 235 157 139 99
9d 10d 12d 16d 20d	234 " 3 " 314 " 312 " 4 "	" 10 " 9 " 9 " 8 " 7	90 69 62 49 37

#### CASING NAILS

Size	Length	Steel Wire Gauge	Approx. No. to Lb.
2d	1 inch	No. 15½	1010
3d 4d	11/4 "	" 14½ " 14	635 473
5d 6d	13/4 "	" 14 " 12½	406 236
2d 3d 4d 5d 6d 7d 8d 9d	21/4 " 21/2 "	" 12½ " 11½	210 145
<b>10</b> d	23/4 "	" 11½ " 10½	132 94
12d 16d	31/2 "	" 10½ " 10	87 71
20d 30d	41/2 "	" 9 " 9	62 46
<b>40</b> d	5 "	" 8	35 

#### ROOFING NAILS

Size	No. 8	No. 9	No. 9½	No. 10
Dia. of head, ins	1/2	1/2	1/2	7/6 & 1∕2

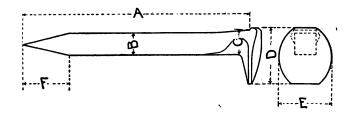
Lengths, all sizes, 34, 78, 1, 118, 114, 112, 134 ins. [Wickwire Bros., Cortland, N. Y.]

#### **SPIKES**

#### SQUARE

#### Railroad Spikes

A standard railroad spike has a square cross section with a chisel point as in figure below. Reverse point has the cutting edge parallel to the length of the head—this type of spike is often used on bridge stringers, where the stringers run parallel to the track.



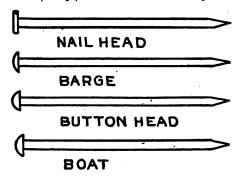
			He	ead		Approx.
Length	Thickness of shank	Thickness of neck	Length	Width	Length of taper	number per keg of 200 lbs.
<u>A</u>	В	С	D	E	F	200 108.
$\frac{2\frac{1}{2}}{21}$	5/16	5/16 3/	3/4	5/8 3/8	5/8 3/4 3/	2200 1520
$\frac{21/2}{3}$ $\frac{31/2}{3}$	3/8	5 16 3/8 3/8 3/8	1	5/8 3/4 3/4 3/.	34 34 37	1340 1170
$\frac{3}{4}$ $\frac{3}{2}$	7/16	16	11/8	7/8	7/8	684 620
4	1/2 1/2	916 916	11/4	11/16	1 1/8	600 536
4½ 5 5 5 5½	1/2	9/16 9/16 5/	$ \begin{array}{c} 1\frac{1}{4} \\ 1\frac{1}{4} \\ 1\frac{7}{16} \end{array} $	11/16 11/16	1 11/2	490 370
$\frac{5}{5}\frac{1}{2}$	9/16 9/16 9/16 5/8	916 5/8 5/8 3/4	17/16 19/16	$ \begin{array}{c c} 1\frac{1}{4} \\ 1\frac{1}{4} \\ 1\frac{3}{8} \end{array} $	1½ 1½ 1½	340 269
	/8	74	1 2/16	1 1/8	11/4	209

[Illinois Steel Co., Chicago, Ill.]

Spikes are made of Bessemer or open hearth steel having the following properties: Tensile strength, 55,000 lb. per sq. in.; yield point, 27,500 lb. per sq. in.; elongation, 25 per cent in 2 ins. The body of the full-size finished spike shall bend cold through 180 degs.

flat on itself, without cracking on the outside portion. The head of the full-size finished spike shall bend backward to the line of the face of the spike, without cracking on the outside of the bent portion.

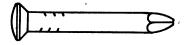
Nail, Barge, Button and Boat Head Spikes



(Approximate number per keg of 200 lb.)

Inches		Length of Spike—Inches										
Inc	3	4	5	6	7	8	9	10	11	12	14	16
5/8 1/8 3/8 1/4	1320 1660 3000	1140 1360 2375	940 1230 2050	450 600 800 1175 1825	375 590 650 990	260 335 510 600 880	240 300 400 525	220 275 360 475	205 260 320	190 240 230	175	160

#### ROUND



These can be obtained with chisel or diamond points and with flat heads.

ROUND—Continued

Size	Length	Am. Steel Wire Gauge	Approx. No. to
10d	3 inch	No. 6	41
12d	3¼ "	" 6	38
16d	31/2 "	" 5	30
<b>20d</b>	4 "	" 4	23
30d 40d	4½ " 5 "	" 3	17
<b>40d</b>	5 "	" 2	13
50d	5½ "	" 1	10
<b>60</b> d	6 "	" 1	8
7 inch	7 "	" 0	7
8 "	8 "	" 00	6
9 "	9 "	" 00	5
10 "	10 "	3% inch	4
12 "	12 "	88 "	3

KEYS
For Shafts, Gears, Pulleys and Couplings

Dia. of Shaft	Size of Key	Dia. of Shaft	Size of Key	Dia. of Shaft	Size of Key
In. 13/6 11/4 13/8 17/16 28/16 11/5/8 16 11/5/8 16 11/5/8 16 12/5/8 16 12/5/8 16 12/5/8 16 12/5/8 16 16 16 16 16 16 16 16 16 16 16 16 16	In. 732 732 732 732 732 732 732 732 732 732	In. 3 3 3 4 3 3 4 4 4 4 4 5 5 5 6 6 6 6 6 6 7 7 7 6	In. 11/6 x 11/6 11/6 x 13/6 x	In. 71/2 716/6 8 81/2 81/2 81/2 9 97/6 91/2 91/2 101/6 11 11/2 11/2 1	In.  11/16 x 11/1 13/16 x 13/1 13/16 x 13/1 13/16 x 13/1 13/16 x 15/1 13/16 x 15/1 15/16 x 15/1 11/16 x 17/1 11/16 x 17/1 11/16 x 11/1

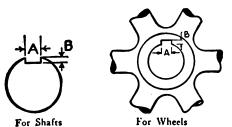
[Cresson-Morris Co., Phila., Pa.]

#### SPECIAL KEYS FOR HEAVY MACHINERY

Dia. of Shaft	Sise of Key	Dia. of Shaft	Size of Key	Dia. of Shaft	Size of Key
In. 215 66 3 1/8 33/6 31/4 37/6 31/2 318/16 41/16	In. 78 x 56 78 x 58 1 x 34 1 x 34 1 x 34	In. 415/6 5 57/6 5 1/2 515/6 6 67/16 6 15/2 7 77/16	In.  1 1/4 x 7/8  1 1/4 x 7/8  1 1/4 x 7/8  1 1/4 x 7/8  1 1/2 x 1  1 1/4 x 1	In. 71/2 715/6 8 87/6 81/2 815/6 9 97/6 91/2 915/6	In.  134 x 114 2 x 136 2 14 x 112

[Cresson-Morris Co., Phila., Pa.]

#### KEY SEATS IN SHAFTS AND WHEELS



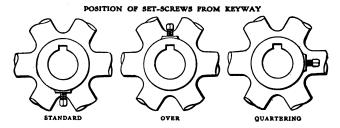
Diameter	Key	-way	Diameter	Key	-way	Diameter	Key	-way
of Shaft	A Width	B Depth	of Shaft	A Width	B Depth	of Shaft	A Width	B Dep
15% to 11% 1 5% to 15% 113% to 21% 2 5% to 23% 213% to 33% 3 5% to 33% 3 15% to 44% 4 5% to 43%	3/8 1/2 5/8 3/4 7/8	18/8/4/5/8/8/8/8/8	511 to 61/4 66 to 71/4 75 to 71/4 8 to 81/4 85 to 91/4 90 to 101/4 105 to 111/4 111 to 121/4	1½ 1¾ 2 2 2½ 2½ 2½ 3	3/4/4/8/8/8/7/7/7/8/8/8/8/8/8/8/8/8/8/8/8	145% to 151% 155% to 161% 165% to 171% 175% to 181% 185% to 191% 195% to 201% 205% to 211% 215% to 221%	384 4 414 414 414 5 5 5 5 14	1 1 1 1 1 1 1

[Dodge Sales & Eng'g Co., Mishawaka, Ind.]

#### Notes on Keys and Key Seats

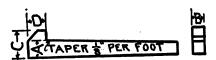
On pulleys and gears the key seat is under an arm on all sizes up to 74 ins. dia., when practical with a set screw over the keyway. Large pulleys and gears having 8 arms, when made in two parts have the key seat in the center of one half, that is between two arms.

The following represents practice at Gisholt Machine Co., Madison, Wis. For shafts up to 113/6" dia., Woodruff keys. Sliding parts for shafts up to 113/6" dia. square keys and over this diameter flat keys. For hollow shafts and sleeves not transmitting their full power, use a key for a shaft of ½ the diameter of the hollow shaft or sleeve. If full power is transmitted use if possible the standard key for solid shafts, if this is not possible then 2 keys for a shaft of ½ the diameter of the sleeve.



Key seats as left milled by cutters are measured from the bottom of the key seats. Key seats with drilled or square ends are measured from the ends.

#### GIB HEAD KEYS

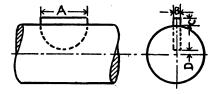


Gib head keys are used when the small end of the key is inaccess-

ible; with the exception of the head they are the same as tapered keys.  $\cdot$ 

A	В	C	D	A	В	С	D
1/8	1/8	1/4	1/62	15/8	15/8	23/4	17/8
18 8.6 1.4 5.16 3.8 7.16 2.9 9.16 1.1 1.3 1.4 1.3 1.3 1.6 1.5 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	18 816 14 16 87 16 87 16 17 18 11 16 16 17 18 16 16 16 16 16 16 16 16 16 16 16 16 16	14 616 16 16 12 916 11 16 34 7/8	7.52 9.52 11.52 15.52 15.52 19.52 21.52 25.52 7.83 15.56	15/8 11/16 11/16 11/16/16/16/16/16/16/16/16/16/16/16/16/1	15/8 11/6 13/3/16 11/5/16 11/5/16 22/3/16/3/16/3/16/3/16/3/16/3/16/3/16/3/	223333334444444555555555555555555555555	116 16 16 16 16 16 16 16 16 16 16 16 16
5/16 3/6	5/16 3/6	9/16 11/6	13 33 15 50	1 <sup>13</sup> /6	1 <sup>13</sup> /6	3½ 3¾	21/16
716	7/16	3/4	17%	115/16	115/16	35/8	23/16
9/16	916	1	21 32 32	21/16	21/16	$\frac{3\%}{3\%}$	27/16
5/8 11/6	5/8 11/6	11/8	23 25 25	21/8	21/8	41/6	$\frac{2\frac{1}{2}}{2\frac{9}{6}}$
3/4 13/	3/4 13/	114	7/8 15/	214	21/4	41/4	25/8
7/8	7/8	11/2	1	23/8	23/8	41/2	23/4
1 1 1 1	1 16/16	1% 1%	11/16	$\frac{27}{16}$	$\frac{27}{16}$	45/8	$2^{13}$
11/16	11/16	113/16	13/16	29/16	29/16	47/8	215/10
13/16	13/16	115/16	13/8	211/16	211/16	5	31/16
15/6	15/6	2 21/8	11/16	$\frac{23}{4}$ $\frac{213}{6}$	23/4 213/6	$\frac{51/8}{51/8}$	31/8
13/8	13/8	214	19/16	27/8	27/8	514	31/4
11/6 11/8 13/6 11/4 15/6 13/8 17/6 11/2 19/6	$1^{1}_{1/6}$ $1^{1}_{1/8}$ $1^{3}_{1/6}$ $1^{1}_{1/4}$ $1^{5}_{1/6}$ $1^{3}_{1/6}$ $1^{1}_{2}$ $1^{9}_{1/6}$	$1\frac{1}{8}$ $1\frac{3}{16}$ $1\frac{1}{4}$ $1\frac{5}{16}$ $1\frac{5}{16}$ $1\frac{15}{16}$	$1^{1/16}$ $1^{1/8}$ $1^{3/16}$ $1^{5/16}$ $1^{5/16}$ $1^{1/8}$ $1^{1/2}$ $1^{1/8}$ $1^{1/8}$ $1^{1/8}$	3	3	$\frac{5\frac{7}{4}}{5\frac{3}{8}}$	31/2
1%	19/16	25/8	113/16			. •	

#### WOODRUFF KEYS



Woodruff keys are suitable for shafts up to  $2\frac{1}{2}$  ins. diameter,

#### WOODRUFF KEYS-Continued

but they cannot be used as sliding keys.

Num- ber of Key	Dia. of Key	Thick- ness B	Depth of key- way C	D	Ultimate shearing strength lbs.	Num- ber of Key	Dia. of Key	Thick- ness B	Depth of key- way C	D	Ultimate shearing strength lbs.
1 2 3 4 5 6 7 8 9 10 11 12 A 13 14 15 B 16 17 18 C	12220000000000000000000000000000000000	TO THE THE PERSON STREET OF TH	Satistical designations of the same of the	***************************************	1,566 2,350 3,132 2,937 3,915 4,894 4,700 5,872 7,050 8,221 9,591 10,961 9,375 10,937 12,500 10,545 12,305 14,062 17,575	19 20 21 D E 22 23 F 24 25 G 26 27 28 29 30 31 32 33 34	111111111111111111111111111111111111111		A the track the	5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	11,718 13,671 15,630 23,436 17,187 21,484 25,750 23,437 28,125 15,910 20,888 25,312 29,702 53,850 69,525 76,781 83,918

[Whitney Mfg. Co., Hartford, Conn.]

#### WOODRUFF KEYS TO USE WITH VARIOUS SHAFTS

Dia. of Shaft	Numbers of Keys— see above table	Dia. of	Numbers of Keys	Dia. of Shaft	Numbers of Keys
5/6-3/8 7/6-1/2 9/6-5/8 11/6-3/4	1 2, 4 3, 5 3, 5, 7 6, 8	7/8-15/16 1 11/16-11/8 13/16 11/4-15/16	6, 8, 10 9, 11, 13 9, 11, 13, 16 11, 13, 16 12, 14, 17, 20	$1\frac{3}{8}-1\frac{7}{16}$ $1\frac{1}{2}-1\frac{5}{8}$ $1\frac{11}{16}-1\frac{3}{4}$ $1\frac{13}{16}-2$ $2\frac{1}{16}-2\frac{1}{2}$	14, 17, 20 15, 18, 21, 24 18, 21, 24 23, 25 25

If the pulley or gear to be keyed on the shaft has an exceptionally long hub, then two keys should be fitted.

#### KEYWAYS FOR MILLING CUTTERS



Square Keyway

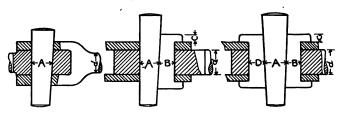
Dia. hole, H	29/6-3 1/6 3/6 .060
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#### Half-Round Keyway

[Pratt & Whitney, Hartford, Conn.]

#### GIBS AND KEYS

(Cottered Joints)



Taper of key 1/20 to 1/100, if more than 1/25 the key is likely to slip.

d = dia. of rod

= .2d

A = 1.2d

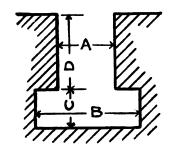
D = .4d

Thickness of key at center = .3 d

B = .4d

#### MISCELLANEOUS FASTENINGS

T SLOTS



Width of Slot A Ins	Dia. of Neck of Cutter	Width of Slot B	Depth C	Extreme Limit D
516 3/8 7/6 1/2 5/8 3/4 7/8	9 52 11, 52 3 8 7 6 17, 52 21, 52 26, 52 2 9, 52	5 8 11/6 11/6 116/6 115/6 15/6 15/6 15/6 15	5 22 7 22 7 22 9 22 11 22 11 16 13 16	3/8 7/16 7/16 9/16 3/4 1 11/16 13/16

[Brown & Sharpe, Prov., R. I.]

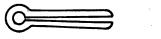
BOLT HEADS FOR T SLOTS

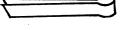
bolt bo	le of sq. Thicknes lt head of head	<b>525</b>
1.4 5.46 3.8 7.8 1.65 5.8	9/16	
	1/4 5/4 3/6 3/8 1/2 5/2 5/3	1/4

#### SPRING COTTERS

Wire Gauge	Diameter	Lengths*	Wire Gauge	Diameter	Lengths*
13 12 11 10 9 8	3/32 7/64 1/8 9/64 5/52 11/64	½ to 2 ½ " 2 ½ " 2 ½ " 2½ ¼ " 2½ ¼ " 2½ ½ " 2½	7 6 5 4 1	3/16 13/64 7/32 1/4 5/16	34 to 3 34 " 3 1 " 3 1 " 4 1 " 4

<sup>\*</sup> Advancing by 1/4".





**Spring Cotter** 

Flat Spring Key

#### FLAT SPRING KEYS

Width	Length									
8/8 1/2 5/8 3/4	1¼ 1¼	1½ 1½	134 134 134	2 2 2 2	2½ 2½ 2¼ 2¼ 2¼	2½ 2½ 2½ 2½ 2½ 2½	28/4 23/4 28/4 28/4 23/4	3 3 3	3½ 3½ 3½	3½ 3½

[F. P. Smith & Co., Sharon Hill, Pa.]

#### SECTION III

#### POWER TRANSMISSION

SHAFTING — QUILL DRIVES — COUPLINGS — CLUTCHES — COLLARS

— BEARINGS — PULLEYS — MULE STANDS — BELTING

— BELT DRIVES — ROPE SHEAVES AND PULLEYS —

CHAINS FOR TRANSMITTING POWER—SPROCKETS

— GEARING: SPUR, MITRE, BEVEL, WORM,

HERRINGBONE—THRUST OF SPIRAL

AND HELICAL GEARS

#### SHAFTING

Rolled shafts for power transmission in mills and factories can be obtained up to 8 ins. dia., and in stock lengths 10, 12, 14, 16, 18, 20, 22 and 24 ft. lengths. For general use the sizes in the table are recommended.

Dia.	Weight lbs. per ft.	Dia.	Weight lbs. per ft.	Dia.	Weight lbs. per ft.
$\begin{array}{c} 13_{16} \\ 17_{16} \\ 11_{16} \\ 11_{16} \\ 11_{5} \\ 23_{16} \end{array}$	3.76 5.52 7.60 10.02 12.78	$2\frac{7}{16}$ $2^{15}/16$ $3\frac{3}{16}$ $3^{7}/16$ $3^{15}/16$	15.86 23.04 27.13 31.56 41.40	47/6 4 <sup>15</sup> /6 57/6 5 <sup>15</sup> /6	52.58 65.10 78.95 94.14

Forged steel shafting is preferable to rolled for sizes 6 ins. dia. and above, as it is stronger and more homogeneous. Forged steel shafting as manufactured by Dodge Manufacturing Co. has the following characteristics: tensile strength per sq. in. 60,000 to 70,000 lbs., elastic limit 30,000 to 36,000 lbs., elongation in 2 ins. 25 to 30%, reduction in area 40%.

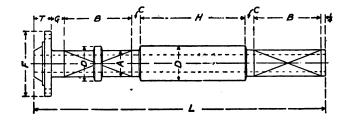
Shafting in machine shops should run at about 160 rev. per min., and in wood working shops 250.

Shafting should be supported so the deflection is not greater than .01 in. per ft. See pages 93 and 106.

#### QUILL DRIVES

For heavy duty and where it is necessary to use a clutch on the driving shaft, quill drives can be installed to advantage.

A quill is a hollow shaft, usually cast iron, larger in diameter than the line shaft. The quill is supported by independent bearings (indicated by crosses in the figure) the clutch is attached to the face F, and at H is keyed the pulley. The clutch when disengaged is stationary. The line shaft supported by its own bearings revolves but does not come in contact with the quill. The quill relieves the line shaft of the weight of the pulley and belt pull.



DIMENSIONS IN INCHES

Shaft Sizes	A	В	С	D	G	н	F and T	Keyseat in Swell
$2^{15}_{16}$ $3^{7}_{16}$ $3^{16}_{16}$ $4^{7}_{16}$ $4^{15}_{16}$ $5^{7}_{16}$ $6^{7}_{16}$ $6^{15}_{16}$ $6^{7}_{16}$ $6^{7}_{16}$	511/16 33/16 611/16 77/16 83/16 811/16 93/16 1011/16 1011/16 1111/16	12 14 14 16 16 18 18 21 21 24 24	3/4/4/4/4/3/3/3/3/3/3/3/3/3/3/3/3/3/3/3	$6^{11}_{16}$ $7^{3}_{16}$ $7^{11}_{16}$ $8^{7}_{16}$ $9^{3}_{16}$ $9^{11}_{16}$ $10^{3}_{16}$ $11^{13}_{16}$ $11^{11}_{16}$ $12^{11}_{16}$ $13^{3}_{16}$	13/4 13/4 2 2 2 21/4 21/4 21/2 23/4 23/4	Not less than width of face of pulley.	Determined by size of clutch used.	11/4x1/4 11/2x1/4 13/4x1/4 13/4x1/4 2 x3/8 2 1/4x3/8 21/4x3/8 21/4x3/8 23/4x3/8 3 x3/8

[T. B. Wood's Sons Co., Chambersburg, Pa.]

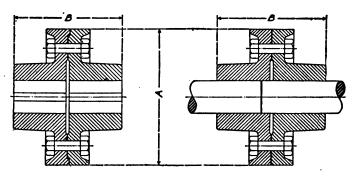
Horse Powers of Shafting under Different Conditions

n '1	. 1	200	114 48 48	73 105 145	194 406 406	610	:::	:::									
with no D*R 50			13 38	885			<del></del>										
with D		400			155 203 325	488 699 963		:::									
ower v	nute	300	288	44 878	117 152 244	366 524 723	998 1296	::::									
n of po	er mi	er mi	250	855.42	36 72 72	97 127 203	305 437 602	832 1080 1373	1715								
missio	Revolutions per minute	200	72161	838	78 101 163	244 350 482	966 1099	1372 1688 2048									
trane	Revolu	150	5 9 14	4322	58 122 122	183 262 361	499 648 824	1029 1266 1536									
For simple transmission of power with no bending strains.  H. P. = D <sup>1</sup> R 50		100	ကစ္	8225	39 81 81	122 175 241	333 432 549	686 844 1024									
For		09	ಚಣಾ	7 01 14	19 25 41	87 120	166 216 275	343 422 512									
- 041		500	188	48 70 97	129 169 271	407	:::										
DaR 75	Revolutions per minute	ıţe	ıţe	ıţe	400	169	38	104 135 217	326 466 642	:::	:::						
<b>1 2 1</b>		300	7 12 19	838	163	244 350 481	999	:::									
with bearings H. P. = $\frac{D^4R}{75}$		250 300 400	100	458	385 135	882	555 720 915	1143									
t.		200	488	388	25 88 108 88	163 233 321	444 576 732	915 1125 1365									
For line shafts, every 8 ft.		evolu	150	89 10	2228	513 813	122 175 241	333 432 549	686 844 1024								
or li		100	0.40	041	884	81 117 161	222 288 366	457 563 683									
Ĕ		50	-0100	10	13 27 27	<b>4%8</b>	1248	220 281 341									
5 44		200	8 10 10	848	200 162 162	244	:::	.: : :									
strains, D <sup>3</sup> R		400	5 15	23 83 46	81 130	195 280 385	:::	:::									
"	Revolutions per minute	per minut	per minut	per minut	300	11	17 25 34	46 61 97	146 210 290	520 :	:::						
heavy s, etc. H. P.					per	per 1	per	per 1	per 1	per 1	per 1	per	per	per :	250	3.3 10	2212
hafts,	tions	200	2. 8.5.6	23,12	25 64 63	98 140 192	265 345 440	550 675 820									
ad sl with	evolu	150	8.1.8	9 13 17	884	73 105 144	888	412 506 614									
For head shafts, shafts with gears,	A2	100	±.62 €.65.44	9882	328	<b>458</b>	133 173 220	275 337 410									
¥ ,		92	010	ω <b>4</b> .0	8 10 16	488	86 110	137 170 205									
Dis.	Dia. of Shaft Ins.			115/6 23/6 27/6	211/6	315% 47% 415%	57% 6 63%	8 8 8									

Dodge Sales & Eng'g Co., Mishawaka, Ind.] [In formulæ—D = dia. of shaft, and R = rev. per min.

### COUPLINGS

#### FLANGE COUPLINGS



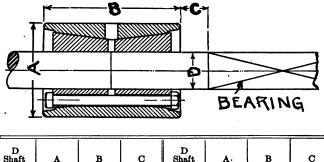
Male and Female Type

Standard Plain Face Type

Shaft Sizes	A .	В	Shaft Sizes	A	В
13/6 17/6 111/6 115/6 23/6 27/6 211/6 215/6	6 6 8 4 7 1 4 8 8 1 / 2 9 9 3 / 4	45/8 51/8 53/4 63/8 67/8 73/8 73/8 73/8	311.6 318.6 47.6 418.6 57.6 518.6	12 12½ 13½ 16¼ 17½ 19 20	10 10 <sup>5</sup> / <sub>8</sub> 13 <sup>5</sup> / <sub>8</sub> 14 <sup>3</sup> / <sub>8</sub> 15 <sup>1</sup> / <sub>8</sub> 16 <sup>1</sup> / <sub>8</sub> 16 <sup>3</sup> / <sub>4</sub>
3 <sup>3</sup> / <sub>16</sub> 3 <sup>7</sup> / <sub>16</sub>	10 1/2 11 1/4	878 988	77/16 715/16	20 21 22½ 24	18½ 19½

Couplings are forced on shafts by hydraulic press and keyed. Shafts are then centered in a lathe and the couplings faced. Number of bolts = .78 dia. of shaft + 2. Bolt dia. = .13 dia. of shaft +  $\frac{1}{4}$ ". Total thickness of web = .5 dia. of shaft +  $\frac{3}{8}$ ".

# Double Cone Compression Couplings



D Shaft Sizes Ins.	A	В	С	D Shaft Sizes Ins.	A.	В	С
115/6 23/6 27/6 211/6 215/6 33/6 37/6 311/6 315/6	5½ 6 65% 7 77% 8¼ 9 95% 10½ 11¼	7 <sup>1</sup> / <sub>8</sub> 8 <sup>5</sup> / <sub>8</sub> 9 <sup>1</sup> / <sub>2</sub> 10 <sup>1</sup> / <sub>4</sub> 11 <sup>1</sup> / <sub>2</sub> 12 <sup>1</sup> / <sub>4</sub> 13 14 <sup>1</sup> / <sub>4</sub> 15 16 <sup>1</sup> / <sub>2</sub>	3 3 3 4 4 1 2 4 1 7 2 4 1 7 2 8 6 6 3 4	415 6 57 6 515 6 67 6 67 16 715 6 715 6 87 16 815 16	12 <sup>1</sup> / <sub>4</sub> 13 <sup>1</sup> / <sub>4</sub> 14 15 <sup>1</sup> / <sub>4</sub> 16 <sup>1</sup> / <sub>4</sub> 17 <sup>1</sup> / <sub>2</sub> 18 <sup>1</sup> / <sub>2</sub> 20 <sup>1</sup> / <sub>2</sub>	18 19\$4 211/2 2314 25 27 29 32 32	7½ 8¼ 9 9 <sup>8</sup> ¼ 10½ 11¼ 12 13½ 13½

[T. B. Wood's Sons Co., Chambersburg, Pa.]

The coupling consists of shell, two cones and bolts. Each cone has a keyway cut in it as also in each end of the shafts. By drawing up the bolts an equal pressure is exerted on the cones, which are compressed and drawn into the outside shell. With this type of coupling the shafts may be slightly out of alignment yet transmit power satisfactorily.

Universal Giant Compression Couplings

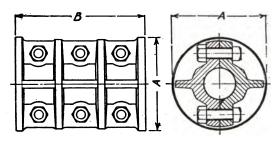
	-B	
	<u> </u>	
· · · · · · · · · · · · · · · · · · ·	T	
		BEÁRING

D Shaft	Dime	ensions in	Inches	D Shaft	Dime	nsions in l	nches
Sizes Inches	A	В	С	Sizes Inches	A	В	C
$\begin{array}{c} 15/16 \\ 13/16 \\ 17/16 \\ 111/16 \\ 115/16 \\ 23/16 \\ 27/16 \end{array}$	45/8 53/8 61/4 61/2 73/8 73/4 9	3 <sup>3</sup> / <sub>4</sub> 4 <sup>3</sup> / <sub>8</sub> 5 <sup>1</sup> / <sub>4</sub> 6 <sup>1</sup> / <sub>8</sub> 7 77/ <sub>8</sub> 8 <sup>3</sup> / <sub>4</sub>	2 2 <sup>1</sup> / <sub>4</sub> 2 <sup>5</sup> / <sub>8</sub> 3 <sup>1</sup> / <sub>8</sub> 3 <sup>1</sup> / <sub>2</sub> 4 4 <sup>3</sup> / <sub>8</sub>	$\begin{array}{c} 2^{11} & _{16} \\ 2^{15} & _{16} \\ 3^{3} & _{16} \\ 3^{7} & _{16} \\ 3^{11} & _{16} \\ 3^{15} & _{16} \end{array}$	9 <sup>1</sup> ⁄ <sub>4</sub> 10 10 <sup>3</sup> ⁄ <sub>4</sub> 12 12 <sup>1</sup> ⁄ <sub>2</sub> 13	9 <sup>5</sup> / <sub>8</sub> 10 <sup>1</sup> / <sub>2</sub> 10 <sup>1</sup> / <sub>2</sub> 11 <sup>3</sup> / <sub>8</sub> 12 <sup>1</sup> / <sub>4</sub> 13	47/8 51/4 51/4 53/4 61/4 63/4

[T. B. Wood's Sons Co., Chambersburg, Pa.]

This type of coupling is suitable for repairing a broken shaft quickly. It is designed to use without shaft keys, and consists of a slotted sleeve with a reverse taper on the outside, and compression flanges. By tightening bolts in the flanges, they are drawn together causing the sleeve to grip the shaft. To obtain an even grip the flanges should be equidistant.

RIBBED COMPRESSION COUPLINGS



Dia. of Shaft	<b>A</b>	В	Number of Bolts	Dia. of Bolts
13/6 17/6 11/1/16 11/5/16 28/16 27/16 21/1/16 21/5/16 33/16 37/16 31/16	4½ 4¾ 5 6 6¾ 7¼ 7½ 8¾ 9¼ 10 105% 12 135%	5½ 6¼ 7 8¼ 8½ 9½ 10% 113¼ 123¼ 134¼ 14¼ 16½ 18½	4 4 4 4 6 6 6 6 6 6	

Keys are required.

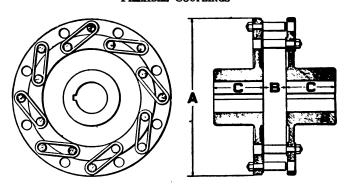
[T. B. Wood's Sons Co., Chambersburg, Pa.]

#### RING COMPRESSION COUPLINGS

These couplings consist of two half sleeves tapered on the outside and two forged steel rings bored to match at each end. In fitting couplings to shafts the rings are driven towards each other, forcing the sleeves to grip the shafts. Keys are required.

Shaft dia.	115/16	28/16	27/16	211/16	215/16	33/16	37/16	311/16	315/16	47/16	415/16	57/16	515/16
Length of coupling	8	9	10	11	12	13	14	15	16	18	20	22	24

FLEXIBLE COUPLINGS

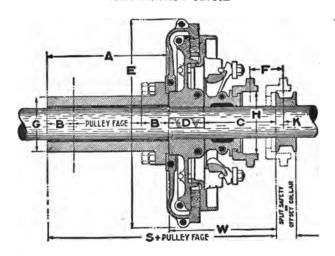


Outside Diameter A Inches	Masimum Shaft Diameter Inches	No. of Links	B Inches	C Inches	H. P. at 100 Rev. Steady Load
5 7	15/16 13/	3 3 4 3 4 4 6 6 8 8 8 8	1	134 212 3 312 312 4 6 6 7 7 9 9 1112 13	1 23/4
9	13/16	4	112	3 2	434
12	17/16 115/16	3	21/6	316	111/2
12 12	23/16	4	21%	31/6	11½ 15
15	27/6	4	21%	4	21
18	33/16	4	35/8	6	47
15 18 18		6	35/8	6	47 67
24	315 16 315 16	6	35/8	7	98
24	47/16 415/16	8	35/8	7	130
30	415 16	* 6	35/8 51/4 51/4 51/4 51/4	9-	225
30	5%	8	51/4	9	300
36	510/10	8	514	111/2	380
36	67/6 615/16	10	514	111/2	480
42		10	61/4	13	680
42	716	12	614	13	820
48	715/16	12	61/4	14	960 1220
54 54	8716 81516	12 14	71/	15	1420
60	07/16	16	717	1614	1710
72	97/16 10 <sup>15</sup> /16	12	71/	15 15 16½ 18	2360
72	117/16	14	717	18	2770
72	11156	16	714 714 714	18	3160

[Cresson-Morris Co., Phila., Pa.]

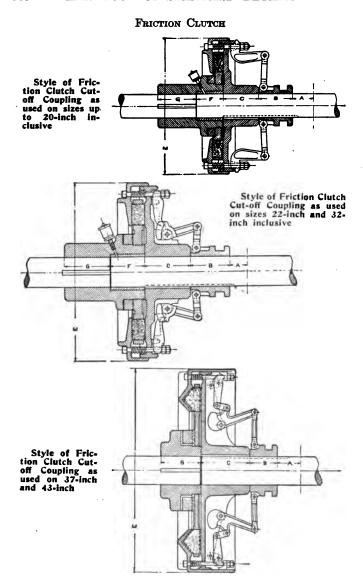
CLUTCHES

### SPLIT FRICTION CLUTCH



Clutch Sises Ins.	Max. dia.of Shaft	В	C	D	E	F	G	н	К	S	w
10 12 14 16 18 20 22 24 28 30 36 42 48 54 60 72	2½ 3 3½ 4½ 5 6 6 6½ 7 7½ 8 10 10 12 12 15	21/2 21/2 21/2 3 3 3 3 3 3 3 3 4 3 1/2 2 1/2 2 1/2 3 3 3 3 3 3 3 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2	678 713/8 83/4 87/8 813/8 95/8 11 11 11 12/8 16/3/4	334 444 444 444 544 544 778 11 12 12 16	14 17 19 21 23 25½ 27 29¼ 34¼ 40¼ 48 54 60¼ 67¾ 83	21/4 25/8 3 3 35/8 4 43/8 5 61/2 7 87/8 93/8 11 11 13/4	D Suit bore of	4 1/2 4 1/2 5 7 8 1/4 8 5 6 8 9 3/4 1 1 1 3/4 1 1 4 3/4 1 1 9 1/2 1 9 1/4 1 1 1 9 1/4 1 1 9 1/4 1 1 9 1/4 1 1 9 1/4 1 1 9 1/4 1 1 9 1/4 1 1 9 1/4 1 1 9 1/4 1 1 9 1/4 1 1 9 1/4 1 1 9 1/4 1 1 9 1/4 1 1 9 1/4 1 1 9 1/4 1 1 9 1/4 1 1 9 1/4 1 1 9 1/4 1 1 9 1/4 1 9 1/	1 3 4 4 5 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	15% 16% 17% 19 19 19% 20% 23% 25% Use quills	1058 1194 1234 13 13 1354 1436 1634 1854 2254 2254 3036 3634

[Dodge Sales & Eng'g Co., Mishawaka, Ind.]

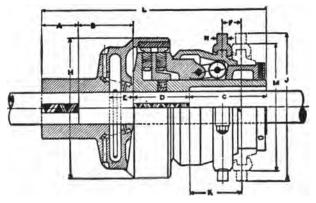


# FRICTION CLUTCH—Continued

Clutch	ter of	t Speed Foff d Run	H. P. at 50 R. P. M. oder normal conditions	Di	mension	ns of W	hole Clu	tches O	nly	Weight Pounds
Size of Clu Inches	Diameter Shaft	Highest Cut- Should	H. 100 R under cond	A	В	С	Е	F	G	We
5 6 8 10 12 14 16 18 20 22 24 28 32	12/16 17/16 17/16 11/16 11/16 22/16 21/16 21/16 33/16 37/16 37/16 37/16	400 400 400 350 350 275 250 225 200 200 200 200	134 21/2 5 7 12 18 25 34 45 55 65 85 112	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2½ 2½ 2½ 3 4 5½ 5 6¼ 6 6¾ 7½	23 3 4 1 4 1 5 1 1 5 1 1 4 1 4 1 4 1 4 1 4 1	734 9 11 13 15½ 18 20¼ 22¼ 25½ 28 29¾ 34 39	2 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	3½ 4 4¼ 5 6 6½ 7 7 7 3½ 8 9	33 42 68 115 202 295 367 479 715 862 1010 1269 1765

[Moore & White Co., Phila., Pa.]

# SAFETY TYPE MULTIPLE DISC SOLID CLUTCH COUPLING



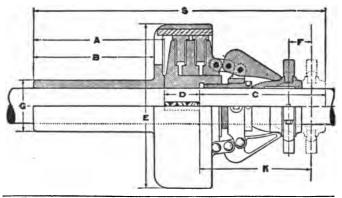
Clutch Size, Inches	A	В	С	D	E	F	н	J	к	L	М	N
6 8 10 12 14	2 2¼ 3 3½ 4	284 314 384 412 5	41/8 47/8 53/8 73/6 73/8	3 4 4½ 5 5%	1 1/4 1 8/8 1 5/8 1 1/1 1/6 1 7/8	1 1 1¼ 1¾ 1¾ 1¾	75% 101% 125% 151% 171%	8 10% 115% 133% 16½	284 388 311/16 53/16 61/16	1178 1438 1658 2038 2218	678 914 1038 1178 1434	9 16 5 8 11 16 13 16 15 16

# Horse Power Capacities, Largest Bores and Safe Speeds Multiple Disc Solid Clutch Coupling

Clutch Size, Inches	H. P. at 100 R. P. M.	Largest Possible Bore, Inches	Size of Shaft Equal in Capacity to Coupling, Inches	Speed Allowable for Coupling as Ordinarily Made
6	4	2	17/16	560
8	8	23/4	115/16	520
10	15	31/4	23/16	480
12	25	334	$2^{3}_{16}$ $2^{7}_{16}$	440
14	40	41/2	215/16	400

[Dodge Sales & Eng'g Co., Mishawaka, Ind.]

# Solid Friction Clutch



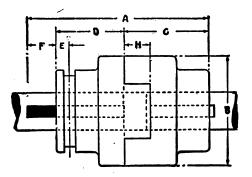
Size of		t Shaft								Ī
Clutch Ins.	Reg.	Speci.	A	В	C	D	E	F	K	s
4 5 6 7 8 9	1½ 1½ 1¾ 2 2¼ 2½ 3		4½ 5 6 7 8 10	4 4 <sup>1</sup> / <sub>2</sub> 5 <sup>1</sup> / <sub>2</sub> 6 <sup>1</sup> / <sub>4</sub> 7 <sup>1</sup> / <sub>4</sub> 9 <sup>1</sup> / <sub>4</sub> 10 <sup>1</sup> / <sub>4</sub>	434 434 638 678 712 758 712	1½ 1¾ 1½ 1½ 2½ 2¼ 2¼ 2¾ 2½	53/8 61/2 711/6 87/8 101/8 113/8 125/8	3/4 3/4 11/4 11/4 11/2 11/2	43/8 43/8 57/8 63/8 7 7 67/8	10 <sup>3</sup> ⁄ <sub>4</sub> 11 <sup>1</sup> ⁄ <sub>2</sub> 14 <sup>1</sup> ⁄ <sub>4</sub> 16 17 <sup>3</sup> ⁄ <sub>4</sub> 20 21
12 14	$\frac{3}{3\frac{1}{2}}$	4 5	12 13	11 12	8½ 9	$\frac{2^{\frac{5}{4}}}{3}$	15½ 175%	11/4	734 81/8	$ 23\frac{1}{4} $ $ 25 $
16	41/2	6	14	13	97/8	41/8	191/2	11/2	9′°	28

[Dodge Sales & Eng'g Co., Mishawaka, Ind.]

This clutch is adapted particularly for use on countershafts and other places where a solid clutch is required.

Size of	Max. Rev.	Horse	Size of	Max. Rev.	Horse
Clutch, ins.	per Min.	Power	Clutch, ins.	per Min.	Power
4	500	5½	9	500	23
5	500	9	10	500	
6	500 500	12 16	12 14	450 400	40 59 102
8	500	19	16	400	170

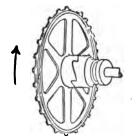
JAW CLUTCH



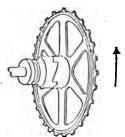
Shaft Size, Ins.	A	В	С	D	Е	F	н	Shaft Size, Ins.	A	В	C	D	E	F	н
15/6 1 3/6 1 11/6 1 11/6 2 5/6 2 17/6 2 11/6 2 15/6 2 15/6	634 758 838 918 978 1032 1158 1238	314 416 514 578 616 7 734 818	31/8 31/8 41/8 41/8 41/8 51/8 55/8	21/2 27/8 31/8 31/2 38/4 45/8 47/8	1,5,8,8,16,15,4,4,8,8,17,8,8	11/8 11/4 13/8 11/2 15/8 13/4 17/8 2 21/8	7/8 1 11/8 11/8 11/4 11/4 11/4 11/4 11/4 11/4	3 7/16 315/16 4 7/16 4 15/16 5 7/16 6 1/2	141/8 153/8 165/8 183/4 201/4 22 233/4 251/2	938 1016 1134 13 1434 1618 1714 1834	63/2 7 73/8 83/2 93/4 10 103/4 113/4	538 6 614 714 734 812 914 934	13/16	23/8 21/2 3 31/4	234

[Dodge Sales & Eng'g Co., Mishawaka, Ind.]

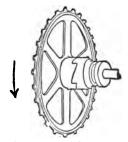
# SPIRAL JAW CLUTCH ARRANGEMENTS Clutch Drives Wheel



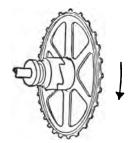
Right-Hand Clutch



Left-Hand Clutch

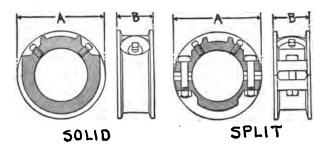


Left-Hand Clutch



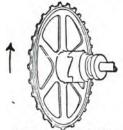
Right-Hand Clutch

### SOLID AND SPLIT SAFETY COLLARS

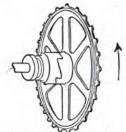


(See opposite page for table)

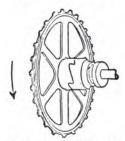
# SPIRAL JAW CLUTCH ARRANGEMENTS Wheel Drives Clutch



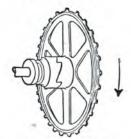
Left-Hand Clutch



Right-Hand Clutch



Right-Hand Clutch



Left-Hand Clutch

# SOLID AND SPLIT SAFETY COLLARS—for figure see page 104.

Shaft	Solid C	ollars	Split C	ollars	Shaft	Solid C	ollars	Split Collars		
Size Inches	A	В	A	В	Size Inches	A	В	A	В	
13/16	27/16	13/8	31/8	13/8	63/4	107/8	31/2	11	31/2	
$\frac{17}{16}$ $1^{11}$ $16$	3316	$\frac{15/8}{15/8}$	$\frac{33/8}{35/8}$	$\frac{15/8}{15/8}$	7 71/4	$10\frac{7}{8}$ $11\frac{3}{8}$	$\frac{3\frac{1}{2}}{3\frac{1}{2}}$	$\frac{11}{11\frac{5}{8}}$	$\frac{3\frac{1}{2}}{3\frac{1}{2}}$	
115/10	37/16 41/16	$\frac{15}{8}$ $\frac{17}{8}$	37/8 4 <sup>11</sup> / <sub>16</sub>	15/8	7½ 7¾ 7¾	11 <sup>3</sup> / <sub>8</sub> 11 <sup>7</sup> / <sub>8</sub>	3½ 3½	$\frac{11\frac{5}{8}}{12}$	31/2	
$2^{3}_{16}$ $2^{7}_{16}$ $2^{11}_{16}$	45/10	17%	415/16	178	8	117/8	$\frac{3\frac{1}{2}}{3\frac{3}{4}}$	12 13	31/3	
215 16 215 16	$4^{9}_{16}$ $4^{15}_{16}$	17/8	5 <sup>3</sup> / <sub>16</sub> 5 <sup>7</sup> / <sub>16</sub>	17/8	81/4 81/2	13	334	13	33/	
$ \begin{array}{c} 2^{15} & 16 \\ 3^{3} & 16 \\ 3^{7} & 16 \end{array} $	5 <sup>3</sup> / <sub>16</sub> 5 <sup>7</sup> / <sub>16</sub>	2 2	5 <sup>11</sup> / <sub>16</sub> 5 <sup>15</sup> / <sub>16</sub>	$\frac{2}{2}$	83/4	$13\frac{1}{2}$ $13\frac{1}{2}$	33/4 33/4	$13\frac{1}{2}$ $13\frac{1}{2}$	$\frac{3\frac{3}{4}}{3\frac{3}{4}}$	
$\frac{3^{11}}{3^{15}}$	5 <sup>7</sup> / <sub>16</sub> 5 <sup>15</sup> / <sub>16</sub> 6 <sup>3</sup> / <sub>16</sub>	21/4 21/4	65/8	21/4 21/4	$9\frac{1}{4}$ $9\frac{1}{2}$	14 14	33/4	14 14	33/4	

(Continued on page 106.)

Shaft	Solid C	Collars	Split C	ollars	Shaft	Solid C	ollars	Split (	Collars
Size Inches	A	• в	A	В	Size Inches	A	В	A	В
4 <sup>1</sup> / <sub>4</sub> 4 <sup>1</sup> / <sub>2</sub> 4 <sup>3</sup> / <sub>4</sub> 5 5 <sup>1</sup> / <sub>4</sub> 5 <sup>1</sup> / <sub>2</sub> 5 <sup>3</sup> / <sub>4</sub>	73/8 75/8 77/8 81/8 85/8 85/8 91/8	31/4 31/4 31/4 31/4 31/4 31/4 31/4	73/4 8 81/4 81/2 9 9 91/2	31/4 31/4 31/4 31/4 31/4 31/4 31/4	9 <sup>3</sup> / <sub>4</sub> 10 10 <sup>1</sup> / <sub>4</sub> 10 <sup>1</sup> / <sub>2</sub> 10 <sup>3</sup> / <sub>4</sub> 11 11 <sup>1</sup> / <sub>4</sub>	14½ 14½ 1558 1558 1618 1618 1658	3 <sup>3</sup> / <sub>4</sub> 3 <sup>3</sup> / <sub>4</sub> 4 4 4 4	14½ 14½ 1558 1558 1618 1618 1638	3 <sup>3</sup> / <sub>4</sub> 3 <sup>3</sup> / <sub>4</sub> 4 4 4

4

4

4

SOLID AND SPLIT SAFETY COLLARS—Continued

Collars for shafts 3 ins. dia. and under have but one set screw. [Dodge Sales & Eng'g Co., Mishawaka, Ind.]

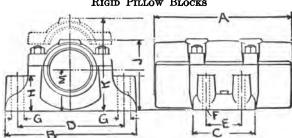
#### BEARINGS

Bearings (pillow block and hanger) in ordinary shop practice are spaced about 8 ft. apart (see page 93). The spacing should be such that the shaft deflection is not greater than .01 ins. per ft.

Length of heavy fixed bearings 2½ to 3½ times the shaft diameter; of light self adjusting 3 to  $4\frac{1}{2}$ . The allowable bearing pressure in lbs. per sq. in. of projected area babbitt or bronze lined is 100 to 155 lbs.

In locating bearings and in selecting the size of shaft it must be remembered that additional pulleys are often installed after the shafting is in place, and it is necessary to allow for them.

For oiling devices see page 107.



RIGID PILLOW BLOCKS

Shaft Sizes, Inches	A	B	С	D	E	Bolts F	G	н	J	K	M
1 % to 11% to 12% to 11% to 12% to 11% to 12% to 12% to 12% to 11% to 12% to 12	5 6 6 1 1 2 1 2 1 2 1 2 1 2 2 2 2 2 2 2 2	7 6 1/2 8 8 8 8 9 1/2 10 11 11 11 11 11 11 11 11 11 11 11 11	22278 A LETTERY A PROPERTY AND A LETTERY AND	55% 65% 66% 66% 66% 66% 66% 66% 66% 66%	4144 434 55% 614 7714 838 910	THE THE PROPERTY OF THE PROPER	TITITITITITITITITITITITITITITITITITITI	THE TANK THE TO THE TANK THE TANK THE TENT	333445556677789991113455674	4 5 5 5 6 6 7 7 5 8 5 7 7 8 8 9 5 6 8 9 5 6 10 9 4 12 12 12 12 12 12 12 12 12 12 12 12 12	1 1 4 2 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2

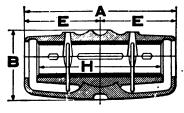
Oil holes at each end of cap are tapped to permit use of grease cups.

[Dodge Sales & Eng'g Co., Mishawaka, Ind.]

#### LUBRICATING DEVICES FOR BEARINGS

Oil and grease cups. Oil cups are usually cast into the bearing cap and filled with waste saturated with oil. Instead of oil cups, grease cups may be tapped into the cap at each end.

Capillary oilers as made by the Dodge Manufacturing Co. consist of a wood block fastened in the bottom of the bearing sleeve, having alternate saw cuts through which the oil rises by capillary attraction from the reservoir below the sleeve.



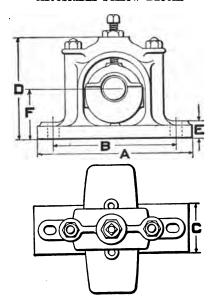
Oiling rings (see figure). The rings as the shaft revolves, bring oil from the reservoir to the shaft.

RING OILING BEARINGS-Continued

Dia, of Shaft	A	В	Е	н	Dia. of Shaft	A	В	E	н
$\begin{array}{c} 2^{7} \underline{16} \\ 2^{11} \underline{16} \\ 2^{15} \underline{16} \\ 3^{3} \underline{16} \\ 3^{7} \underline{16} \\ 3^{15} \underline{16} \\ 4^{7} \underline{16} \\ 4^{15} \underline{16} \end{array}$	12 13 14 15 16 18 20 <sup>3</sup> / <sub>4</sub> 22 <sup>1</sup> / <sub>2</sub>	53/8 57/8 63/8 67/8 71/2 83/8 93/4 113/8	6 6½ 7 7½ 8 9 10¾ 11¼	10 11 12 13 14 16 18 20	5 <sup>7</sup> /6 5 <sup>15</sup> /6 6 <sup>7</sup> /6 6 <sup>15</sup> /6 7 <sup>7</sup> /6 7 <sup>15</sup> /6 8 <sup>7</sup> /6	24½ 26¾ 29¼ 30 31¼ 31½ 31¾	11½ 11¾ 12¾ 12¾ 13¾ 14½ 15¼ 16⅓	12½ 13¾ 14½ 15½ 15½ 15¾ 15¾	22 24 26 27 28 28 28

[Cresson-Morris Co., Phila., Pa.]

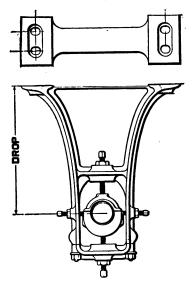
# Adjustable Pillow Blocks



-: l							Во	olta
Dia. of Shaft	A	В	С	D	E	F	No.	Size
In. 13/16 17/16 11/16/16 23/16/16 23/16/16 23/16/16 33/16/16 33/16/16/16 11/16/16 11/16/16/16/16/16/16/16/16/16/16/16/16/1	In. 71/2 81/2 101/2 11 121/2 131/2 14 16 16 17 20 221/2 231/2 25 271/2	In. 6 7 8 9 10 10 12 12 12 13 13 13 12 15 12 18 12 20 22 12	In. 21/2 3 31/2 4 41/2 5 51/2 61/2 7 71/2 8 81/2 91/2 10	In. 5 6 61/2 71/2 81/2 9 91/2 10 11 111/2 131/2 15 16 17	In. 3/4 1 1 1 1 1/4 1/4 1/4 1/4 1/4 2 2 2/2 2/2 2/2 2/2	In. 21/2 33/8 43/8 33/4 41/8 34/8 45/4 45/8 55/4 45/8 65/8 75/8 88/4	222222222222222222222222222222222222222	In. 1/2 5/8 5/8 3/4 3/4 8 1 1 1 1 1/8 1 1/

[Cresson-Morris Co., Phila., Pa.]

HANGERS-8 TO 46 IN. DROP



#### **PULLEYS**

Ordering Pulleys.—The following outline can be used to advantage in ordering pulleys.

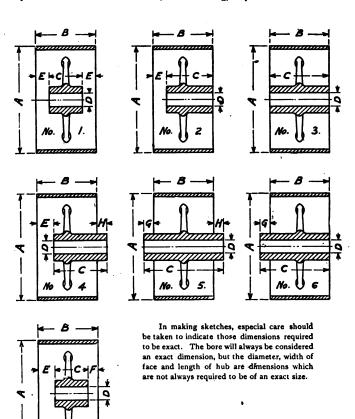
- Service.—State whether for single or double belt. If neither is specified, single belt pulleys will be furnished.
  - If greater horse power than a double belt is required, the horse power, rev. per min. and service should be given.
- Description.—State whether solid, split, clamp hub, flange or special.
  - If no description is given, plain solid pulleys will be furnished. In sending sketches, follow the instructions on page 111.
- Diameter.—Specify diameter in inches. This should be the first dimension.
  - If exact diameter is required, mention this fact and state whether measurement shall be made at crown or edge of rim. An extra charge is made for exact diameter.
- 4. Face.—Specify face in inches. This should be the second dimension given, and should be specified as the width of belt to be used, unless an exact width of face is desired, in which case this should be noted on order by having the word "exact" follow dimension of face.
- Bore.—Specify exact diameter of shaft in inches. This should be the third dimension.
  - If shaft is of an odd or special diameter make a gauge to accompany order.
  - Never send orders as pulley to be bored 115% scant, 2% full or about 14 under 3.
- Crown or Straight Face.—After specifying dimensions of pulley, state whether crown or straight face. If neither is specified, crown face pulleys will be furnished.
  - Pulleys for belts which do not shift should have crown face. Pulleys for shifting belts should have straight face.
- Keyseat or Set Screw.—State whether keyseated or set screwed or both.
  - If neither is specified, set screws only will be furnished.

If keyseated, state whether straight or taper.

Pulleys keyseated and not set screwed should have taper keyseat.

Taper keyseats will be cut with ½" taper per foot, unless otherwise specified. Split hub pulleys are recommended to have straight keyseat with set screws on top.

[Data from T. B. Wood's Sons Co., Chambersburg, Pa.]



up to 14 ins. 15 " 39

40 " 120 "

Cast-iron pulleys are known in the trade by the terms—single belt, double belt and triple belt which terms refer to leather belting. Single belt pulleys can be held on the shaft by set screws, while double belt require keys with two set screws over the keyway.

Single and double belt pulleys up to 40 ins. dia. are balanced to run at 300 ft. per min., and over 40 ins. at 3,500.

Dia. of Pulley	Width of Face	Nur	nber of
		Arms	Sets of Arms

49 and over

Number of Arms

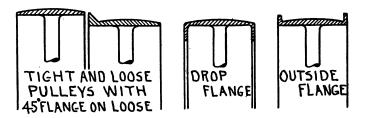
1

23

Diameter every half inch from 6 to 24 ins., every inch 25 to 50, and every 2 ins. 52 to 120. Split pulleys can be obtained in nearly all the sizes as solid.

8

For intermittent driving of a machine, tight and loose pulleys are employed—both having the same diameter with the faces crowned, or one pulley has a 45 deg. flange, with the face crowned, the flange

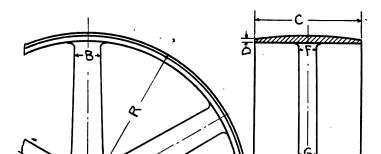


having the same outside diameter as the tight pulley at the edge of the rim, the belt surface being one inch smaller in diameter than that of the tight, thus the belt is relieved of strain when running idle. The hub of the tight pulley is flush with the edge of the rim on each side, with one end of the hub faced off. The hub of the loose pulley extends  $\frac{1}{8}$  in. beyond the edge of the rim on each side, with both ends of hub faced off.

Internal or drop flanges greatly strengthen the rim. Pulleys with such flanges are installed when heavy, tight belts are used.

Pulleys can also be obtained with external flanges at center or side.

Proportions



Width of face 
$$C=1.13 \times$$
 width of belt.  $D=\frac{1}{5}A$   $R=$  radius of pulley  $E=1\frac{1}{6}$  dia. of shaft  $A=\frac{1}{4}''+\frac{C}{4}+.014R$   $F=\frac{1}{2}B$   $G=\frac{1}{2}A$ 

Thickness of metal around shaft = .3 dia. of shaft.

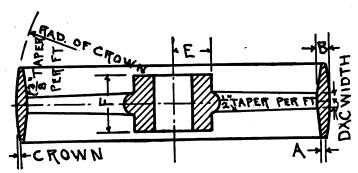
Pulleys for shifting belts should have a straight face and for non-shifting a crown. The crown up to 12 ins. in width varies with different manufacturers from  $\frac{1}{2}$  to  $\frac{1}{2}$  in., and above 12 ins. from  $\frac{1}{2}$  to  $\frac{1}{2}$  in. per foot. When a belt is shifted from one side of the center line to the other, the face should be straight.

# CROWNED CAST IRON PULLEYS (Gisholt Machine Co.,

Width of	Leat	her B	elting	<b>.</b>			1/2	5	<b>É</b>	34	7/8	1	13/4	13	<u> </u>	3/4	2	21/4
Width of	Pulle	y Fa	ce				34	7/	<b>á</b> 1		11/8	11/4	11/2	13,	<u>í</u> 2		21/4	21/2
Radius o	f Cro	wn						5	-		63/4			10	4		1	5
(Based of Width,			For	mula	of 1-	-24			-				1.1.					
Crowning	(Ris	e at (	Cente	r of B	(im.)	••••	.014	.019	0.0	19 .	024	. 029	.027	.03	7 .0	48 .	042	.052
		<u>.                                    </u>													P	ROP	ORTI	ONB
Diam	١.		6				8				10					12	,	
Face	•	2	3	4	2	3	4	5	2	3	4	5	6	2	3	4	5	6
RIM	A	1/8	3/8	1/8	1/8	1/8	1/8	1/8	1/8	3/8	1/8	1/8	%	%	%	%	1/2	%
	В	1/2	ж	%	%	1/4	%	%	1/2	14	%	1/4	3/8	1/4	%	3/6	11/4	3/8
ARM	С	3/4	3⁄4	1∕8	3/4	%	1∕8	1	1∕8	1/8	1	11/8	11/4	1∕8	₹8	1	11/8	11/4
	D	3∕8	3/8	1/16	3/4	3/8	%	1/2	3∕8	3/8	<b>1/16</b>	1/2	%	3/8	3/8	26	1/2	<b>%</b>
HUB	E	1/2	1/2	%	%	%	5/8	5/8	5/8	5/8	5/8	11/16	11/16	5/8	5/8	5/8	11/16	11/16
	F	11/2	21/4	23/4	13/4	21/4	23/4	31/2	13/4	21/4	23/4	31/2	41/2	13/4	21/4	23/4	31/2	41/2
Dian	ı.				22							24						=
Face	•	2	3	4	5	6	7	8	3	4	5	6	7	8	9	3	4	5
RIM	A	3/16	3/16	3/6	74	1/4	% 3€	1/2	1/2	7/2	1/2	1/2	1/2	1/4	1/2	36	<b>½</b>	1/2
102312	В	716 716 716 716 722 722 723 516 11/22 13/22 716					15/2	1/2	11/42	3/8	13/62	<b>1/16</b>	15/2	1/2	17/2	11/42	3/8	13/6
ARM	С	1	1	11/8	11/4	11/2	11/2	13/4	11/8	11/8	11/4	13/2	13/4	17/8	17/8	11/8	13/8	11/4
	D	7/16	1/16	3/2	%	11/16	11/16	34	1/2	3/2	%6	11/16	34	14/16	13/16	1/2	1/2	%
HUB	E	11/16	3/4	3/4	3/4	13/16	₹	₹	3/4	13/6	13/16	₹8	3/8	15/16	15/16	13/6	13%	7/8
	F	13%	21/2	31/2	41/4	51/4	6	7	23/4	31/2	41/2	51/4	6	7	8	23/4	31/2	41/2

FOR LEATHER BELTING (see Figure on page 116) Madison, Wis.

VI &	018	on,	, 77	18.																					
21/2	2	3/4	3	3	14	31/2	í	3%	4		41/2	5		51/2	6		61/2	7		8		9	10	11	
23/4	3		33/8	3	5/8	31/8	1 4	13/8	43/	8	5	53	4	6	6	1/2	7	7	14	8¾	1	0	11	12	
	$]^-$		20					25				3	3				42			5	61/2		70	70	
063	.0	56	.071	.0	82	.075	i .c	85	.09	7	095	. 11	5 .	133	. 12	26	146	.13	79	. 170	.2	<b>2</b> 2 .	217	. 258	
F	PU.	LLE	YS		_													_						_	
		14	,		L		. 1	6	_	_	L			18	<del></del>			_			20	, -			
2	3	4	5	6	2	3	4	5	6	7	2	3	4	5	6	7	8	2	3	4	5	6	7	8	
\ú	%	%	5/2	1/2	1/2	1/2	%	%	%	3/10	3/10	3/10	3/10	3/10	3/a	3/4	1/2	3/16	3/4	3/16	3/16	<b>%</b>	3/4	1/4	
14	%	<b>5</b> ∕46	11/42	3/8	1/4	%	5/16	11/2	3/8	1/16	%	5√6	11/2	3/8	13,62	1/1	1/2	%	3/10	11/2	3/8	13/62	1/16	1/2	
<b>7/8</b>	7/8	1	11/8	11/4	1	1	11/8	13/4	11/4	11/2	1	1	11/8	11/4	11/2	11/2	13/4	1	1	13/8	11/4	13/2	11/2	13/4	
1/8	3/8	7/16	3/2	%	7/6	3/16	1/2	%	%	11/16	3/16	1/16	1/2	%	11/16	11/16	3/4	3/6	7/6	3/2	%	11/16	11/16	3/4	
1/16	11/16	11/16	34	3/4	11/16	11/6	%	3/4	13/16	13/16	11/26	11/16	3/4	3/4	13/16	13/16	1/8	11/16	11/16	34	*	13/16	13/16	7/8	
34	21/4	23/4	31/2	41/2	13/4	21/4	23/4	31/2	41/2	51/4	13/4	21/2	31/2	41/4	51/4	6	7	13/4	23/2	31/2	41/4	51/4	6	7	
26							28							0							32	-		=	
6	7	8	9	3	4	5	6	7	8	.8	3	4	5	6	7	8	9	3	4	5	6	7	8	9	
1/4	1/2	1/4	*	1/4	1/2	1/42	3/4	*	1/4	*	36	?€	1/4	1/4	*	34	*	1/4	1/4	*	1/4	*	<b>%</b>	%	
16	15/6	17/2	%	11/42	3/8	13/6	<i>7</i> /16	1/2	17/2	%	11/2	3/8	7/6	15/2	3/2	17/2	%	3∕8	13/62	7/s	15/2	1/2	%	5/8	
1/2	13/4	17/8	17/8	11/4	11/4	11/2	11/2	13%	17/8	2	11/4	11/4	11/2	11/2	13/4	17/8	2	11/4	11/2	11/2	13/4	17/8	2	2	
1/6	3⁄4	13/6	13/16	%	%	11/16	11/16	3/4	18/6	1/8	%	%	11/16	11/16	*	13/16	7∕8	%	11/16	11/16	3/4	13/16	₹	₹8	
1/8	15/6	13/16	1	1/8	₹8	15/6	15/6	1	1	11/8	15 <sub>16</sub>	15/16	1	1	11/8	11/8	11/4	15/16	15/16	1	1	11/8	11/8	13/4	
14	6	7	8	23/4	31/2	41/2	51/4	6	7	8	23/4	31/2	41/2	51/4	6	7	8	23/4	314	41/2	51/4	6	7	8	
	22/22/24 0063 00	23½ 22¾ 3	23½ 23¼ 3 3 4 5 5 5 5 6 7 8 3 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	23½ 23¼ 3 22¾ 3 3¾ 20 063 .056 .071  F PULLEYS  14  2 3 4 5 ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½	23/4 3 33/8 3 20 063 .056 .071 .0 0F PULLEYS 14 2 3 4 5 6 3/4 5/4 5/4 5/4 3/4 5/4 5/4 5/4 3/4 11/4 11/4 3/4 3/4 21/4 23/4 31/4 41/4 26 6 7 8 9 3 3/4 11/4 11/4 11/4 3/4	23½ 23¼ 3 33¼ 23¼ 3 33½ 35½ 20 063 .056 .071 .082  DF PULLEYS 14 2 3 4 5 6 2 3½ 5½ 5½ 5½ 5½ 5½ 3½ 5½ 5½ 5½ 5½ 3½ 5½ 5½ 5½ 5½ 3½ 5½ 5½ 5½ 5½ 3½ 5½ 5½ 5½ 3½ 5½ 5½ 5½ 3½ 5½ 5½ 5½ 3½ 5½ 5½ 3½ 5½ 5½ 5½ 3½ 5½ 5½ 3½ 5½ 5½ 3½ 5½ 5½ 3½ 5½ 5½ 3½ 5½ 5½ 3½ 5½ 5½ 3½ 5½ 5½ 3½ 5½ 3½ 5½ 5½ 3½ 3½ 5½ 3½ 3½ 5½ 3½ 5½ 3½ 3½ 3½ 3½ 3½ 3½ 3½ 3½ 3½ 3½ 3½ 3½ 3½	23½ 23¼ 3 3½ 3½ 3½ 22¾ 3 33½ 35½ 37½ 20  063 .056 .071 .082 .075  0F PULLEYS  14  2 3 4 5 6 2 3  3½ 5½ 5½ 5½ 5½ 5½ 5½ 3½ 5½ 5½ 5½ 5½ 3½ 5½ 5½ 5½ 5½ 5½ 3½ 5½ 1½ 3½ 1½ 1 1  12% 3% 1½ 3½ 3½ 1½ 1½ 1 1  12% 3% 1½ 3½ 3½ 1½ 1½ 1½ 2% 2½ 2¾ 3½ 4½ 1½ 1½ 1½ 2% 2½ 2¾ 3½ 4½ 1½ 1½ 1½ 2% 1½ 1½ 1½ 1½ 1½ 1½ 1½ 2% 1½ 1½ 1½ 1½ 1½ 1½ 1½ 2% 1½ 1½ 1½ 1½ 1½ 1½ 1½ 2% 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 2% 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 2% 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 2% 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 2% 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 2% 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 2% 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 2% 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 2% 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 2% 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 2% 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 2% 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 2% 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 2% 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 2% 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 2% 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½ 1½	23½ 23¼ 3 31¼ 31½ 3 22¾ 3 33½ 35½ 33¼ 4 20  063 .056 .071 .082 .075 .0  063 .056 .071 .082 .075 .0  063 .056 .071 .082 .075 .0  063 .056 .071 .082 .075 .0  064 .056 .071 .082 .075 .0  065 .056 .071 .082 .075 .0  067 PULLEYS  14	23½ 23¼ 3 33¼ 33¼ 33¼ 33¼ 22¾ 3 33% 33% 35% 35% 37% 41% 20 25 25 25 20 25 25 20 20 25 25 20 20 25 20 20 20 25 20 20 20 20 20 20 20 20 20 20 20 20 20	23½ 23¼ 3 33¼ 33¼ 33¼ 43 4 4 22¾ 3 33¼ 33½ 35½ 35½ 33¼ 43½ 43½ 43½ 35½ 35½ 35½ 35½ 35½ 35½ 35½ 35½ 35½ 3	23½ 23¼ 3 33¼ 31¼ 33¼ 4 4 22¾ 3 33½ 33½ 33½ 4 4 5 6 7 8 9 3 4 5 6 7 8 9	23½ 23¼ 3 33¼ 33½ 33¼ 4 4 4½ 23¾ 3 33½ 35½ 35½ 4½ 4½ 45½ 5  20 25  063 .056 .071 .082 .075 .085 .097 .095  FPULLEYS  14 16  2 3 4 5 6 2 3 4 5 6 7 2  1½ 5½ 5½ 5½ 5½ 5½ 5½ 5½ 5½ 5½ 5½ 5½ 5½ 5½	23½ 2¾ 3 3¾ 3½ 3¾ 4 4 4½ 5 23¼ 3 3¾ 3½ 3¾ 4 4 4½ 5 33 20 25 3  063 .056 .071 .082 .075 .085 .097 .095 .11  PPULLEYS  14 16  2 3 4 5 6 2 3 4 5 6 7 2 3  ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½	23½ 2¾ 3 3¾ 3½ 3¾ 4 4 4½ 5 22¾ 3 3¾ 3¾ 4 4 4½ 5 22¾ 3 3¾ 3¾ 3¾ 3¾ 4¼ 4¾ 4¾ 5 5 5⅓ 3 20 25 33 3 2063 .056 .071 .082 .075 .085 .097 .095 .115 .097 PULLEYS  14 16  2 3 4 5 6 2 3 4 5 6 7 2 3 4	23½ 2¾ 3 3¾ 3½ 3¾ 4 4 4½ 5 5½ 23¼ 3 3¾ 3½ 3½ 4½ 4½ 4½ 5 5 5½ 6  20 25 33  063 .056 .071 .082 .075 .085 .097 .095 .115 .133  DF PULLEYS  14 16 18  2 3 4 5 6 2 3 4 5 6 7 2 3 4 5 2½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½	23\frac{2}{2}\frac{1}{	23\frac{2}{2}\frac{1}{	23\frac{1}{2}\frac{1}{	23/4 23/4 3 33/4 33/4 33/4 4 41/4 5 53/4 6 61/4 7 7  22/4 3 33/4 33/4 33/4 41/4 43/6 5 53/4 6 61/4 7 7  20 25 33 42  063 .056 .071 .082 .075 .085 .097 .095 .115 .133 .126 .146 .13  38F PULLEYS  14 16 18  2 3 4 5 6 2 3 4 5 6 7 2 3 4 5 6 7 8 2  14 3 5/6 1/4 3/6 1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4	234 234 3 334 334 334 434 4 434 5 534 6 652 7 7 224 3 4 5 6 7 8 2 3 4 5 6 7 8 7 8 2 8 3 4 8 34 34 34 34 34 34 34 34 34 34 34 34 34	234 234 3 334 334 334 334 44 434 5 534 6 64 7 8 84  224 3 334 356 374 444 434 5 534 6 664 7 734 834  20 25 33 42 5  063 .056 .071 .082 .075 .085 .097 .085 .115 .133 .126 .146 .179 .170  IF PULLEYS  14 16 18  2 3 4 5 6 2 3 4 5 6 7 2 3 4 5 6 7 8 2 3 4 5 6 7 8 2 3 4 5 6 7 8 2 3 4 5 6 7 8 2 3 4 5 6 7 8 2 3 4 5 6 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7	234 234 3 334 334 334 434 435 5 534 6 654 7 8 2 3 4 5 6 7 8 2 3 4 5 6 7 8 2 3 4 5 6 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7	234	224	



Steel pulleys can be run at higher speeds than cast iron as they are stronger and lighter. Furthermore, tests have shown that belts slip less on steel than on cast iron or wood.

Steel pulleys are of split construction, no keys being required, the pulleys being held to the shaft by compression of hub by bolts. Data on steel pulleys as manufactured by the American Steel Pulley Co., Philadelphia, Pa., are given on pages 122 and 123.

Wood pulleys are cheaper and lighter than cast iron, and under certain conditions give excellent service. They should not be run in damp places nor at high speeds. A wood rim of hard maple segments, properly laid up in glue, has nearly three times the strength of good cast iron for resisting the stresses set up by its own rotation.

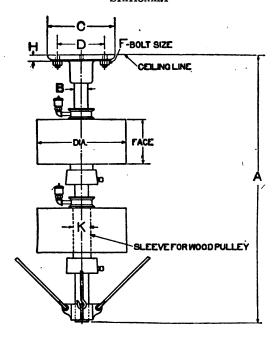
The tractive pull of a leather belt upon a wood rim is greater than upon any metallic rim. With wood pulleys looser belts can be run, and belt slippage can be reduced to a minimum.

There are no standard dimensions as manufacturers have developed their own designs. Below are sizes manufactured by the Dodge Mfg. Co., Mishawaka, Ind.

May be obtained in a variety of face widths—widths above 6 ins. advancing by two, as 6, 8, 10, 12, etc.

# MULE STANDS

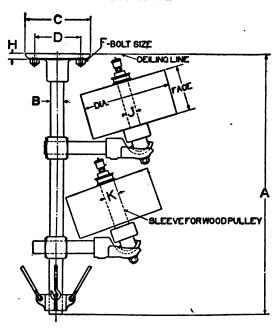
# STATIONARY



Pulley Dia .x Face	A	В	С	D	F	н	К	Rods Dia. x Lth.
10 x 3 10 x 4 12 x 5 12 x 6 12 x 7 16 x 8 24 x 10 24 x 12 30 x 14	4'0" 4'0" 5'0" 5'0" 5'0" 6'0" 6'0"	$1^{15}_{16}$ $1^{15}_{16}$ $1^{15}_{16}$ $2^{7}_{16}$ $2^{7}_{16}$ $2^{15}_{16}$ $2^{15}_{16}$ $2^{15}_{16}$	10 10 10 12 12 12 13 13 13 18 13 18	8 <sup>1</sup> / <sub>16</sub> 8 <sup>1</sup> / <sub>16</sub> 8 <sup>1</sup> / <sub>16</sub> 10 10 10 11 <sup>5</sup> / <sub>8</sub> 11 <sup>5</sup> / <sub>8</sub>	5/5/5/3/3/3/7/7/7/7	1 1 1,1/8 1,1/8 1,1/8 1,1/4 1,1/4	3 3 3 3 1/2 3 1/2 4 4 4	14 x 5'6" 14 x 5'6" 38 x 5'6" 38 x 7'0" 38 x 7'0" 12 x 8'6" 58 x 8'6"

[Dodge Sales & Eng'g Co., Mishawaka, Ind.]





Pulley Dia .x Face	A	В	С	D	F	н	J	ĸ	Rods • Dia. x Lth.
10 x 3 10 x 4 12 x 5 12 x 6 12 x 7 16 x 8 24 x 10 24 x 12 30 x 14	4'0" 4'0" 4'0" 5'0" 5'0" 6'0" 6'0"	$\begin{array}{c} 1^{15} & 6 \\ 1^{16} & 6 \\ 1^{15} & 6 \\ 2^{7} & 6 \\ 2^{7} & 6 \\ 2^{15} & 6 \\ 2^{15} & 6 \\ 2^{15} & 6 \end{array}$	10 12 12 12 13%	8 <sup>1</sup> / <sub>16</sub> 8 <sup>1</sup> / <sub>16</sub> 8 <sup>1</sup> / <sub>16</sub> 10 10 11 <sup>5</sup> / <sub>8</sub> 11 <sup>5</sup> / <sub>8</sub>	5/8/8/8/8/8/8/8/8/8/8/8/8/8/8/8/8/8/8/8	1 1 1 1/8 1/8 1/8 1/4 1/4 1/4	111/6 111/6 111/6 115/6 115/6 115/6 27/6 27/6 27/6	21/16 3 3 3	% x 5' 6" % x 5' 6" 12 x 7' 0" 12 x 7' 0" 5' 6 x 8' 6" % 4 x 8' 6"

[Dodge Sales & Eng'g Co., Mishawaka, Ind.]

#### BELTING

Wide, thin belts are not as satisfactory as narrow thick ones. To get the best results shaft centers should be from 20 to 25 ft. apart. The most economical speeds for belts are from 4,000 to 4,500 ft. per min.

Leather Belts.—For high speeds, the leather should be cut along the spine of the hide, and for low across the shoulder.

Single leather belts are 1/2 to 1/4 inch thick, double 21/4 to 23/4.

Single belts for pulleys up to 11 ins. dia.

Double " " " from 12 ins. and up.
Triple " " " " 20 " " "

U. S. Navy specifications call for oak tanned single leather belts to have a tensile strength of 4,000 lbs. per sq. in., and double 3,600.

Commercial sizes—widths increase by  $\frac{1}{8}$  inch up to 1 inch,  $\frac{1}{4}$  inch up to 4, and  $\frac{1}{2}$  inch to 7. Above 7 ins. depends on the manufacturer.

Rubber belts are made of duck saturated with rubber. They are particularly suited for running in damp places.

Rubber belts are often figured as averaging <sup>1</sup>/<sub>16</sub> inch thickness per ply.

2	ply	rubber	belt	=	$\mathbf{light}$	single	leather	belt.
3	"	"	"	_	medium	"	46	"
4	"	"	u	=	heavy	"	"	"
5	"	"	"	=	light	double	"	"
6	"	"	"	=	medium	"	"	"
7	"	"	"	=	heavy	"	"	"
8	"	"	"	=	triple	"	"	"

#### Commercial sizes

Ply	$\mathbf{Width}$
2, 3 and 4	1 to 60 ins.
5	1½ " " "
6	2 """
7	4 """
8	6 """

Widths from 1 to 2 ins. increase by  $\frac{1}{4}$  in., 2 to 5 by  $\frac{1}{2}$ , 5 to 16 by 1, and 16 to 60 by 2.

Canvas belts have about the same strength as leather.

#### Commercial sizes

Ply	`	1	Wi	dth	l
4		11/2	to	18	ins.
6		3	"	<b>30</b>	"
8		4	"	48	"
10		12	"	60	ţ¢.

Widths from 1½ to 5 ins. increase by ½ in., 5 to 14 by 1, from 14 to 32 by 2. Above 32 ins. special widths can be obtained from manufacturer.

Balata Belts.—These consist of a cotton fabric which is thoroughly impregnated with a solution, the chief ingredient of which is balata. Balata belts should not be installed where the temperature is over 120 degs. F., and they should be kept free from oil. The following table was furnished by R. & J. Dick Co., Passaic, N. J., manufacturers of balata belts.

The following table shows the horse power which each inch of width of belting, from 3 ply to 10 ply, will transmit at the speed given.

Speed of Belt per min.	3 Ply	4 Ply	5 Ply	6 Ply	7 Ply	8 Ply	9 Ply	10 Ply
Ft.	H. P.							
500	0.60	0.90	1.21	1.51	1.81	2.12	2.42	2.71
750	0.90	1.36	1.81	2.27	2.72	3.18	3.63	4.08
1000	1.21	1.81	2.42	3.03	3.63	4.24	4.84	5.44
1250	1.51	2.27	3.03	3.79	4.55	5.30	6.06	6.82
1500	1.81	2.72	3.63	4.55	5.45	6.36	7.27	8.17
1750	2.12	3.18	4.24	5.30	6.36	7.42	8.48	9.54
2000	2.42	3.63	4.85	6.06	7.27	8.48	9.70	10.90
2250	2.72	4.09	5.45	6.82	8.18	9.54	10.90	12.27
2500	3.03	4.54	6.06	7.58	9.10	10.60	12.12	13.64
2750	3.33	4.99	6.66	8.34	10.00	11.66	13.32	14.99
3000	3.63	5.44	7.26	9.10	10.90	12.72	14.52	16.34
3250	3.93	5.90	7.87	9.85	11.81	13.78	15.74	17.71
3500	4.24	6.36	8.48	10.60	12.72	14.84	17.96	19.08
3750	4.54	6.81	9.09	11.36	13.63	15.90	18.18	20.44
4000	4.84	7.27	9.70	12.12	14.54	16.96	19.40	21.81

Horse Power and Widths of Leather Belts.—Speed of belt in ft. per min. = .2618 × dia. of pulley in ins. × rev. per min.

The difference in tension in a belt when running, between the tight and the slack side for a single leather belt may be taken at 40 lbs. per inch of width, for a double belt 65 lbs. and triple 90.

To find H. P. a belt will transmit:

H. P. = 
$$\frac{\text{Speed in ft. per min.} \times \text{width in ins.} \times \text{tension in lbs.}}{33,000}$$

To find width of a belt to transmit a given H. P.:

Width = 
$$\frac{33,000 \times \text{H. P.}}{\text{Speed in ft. per min.} \times \text{tension in lbs.}}$$

# Horse Power Table for Leather Belting single belts

Feet					Wid	th of	Belt in	Inche	9			
in	2	3	4	5	6	8	10	12	14	16	18	20
Speed per M	н,Р.	н.Р.	н.Р.	н.Р,	н.Р.	н.Р.	н,Р,	н.Р.	н,Р	н.Р.	н.Р.	H.P.
400	1	11/2	2	21/2	3	4	5	6	7	8	9	10
600	11/2	214	3	334	41/2	6	71/2	9	1016	12	131/2	15
800	2	3	4	5	6	8	10	12	14	16	18	20
1000	21/2	314	5	61/4	71/2	10	121/2	15	171/2	20	221/2	25
1200	3	41/2	6	71/2	9	12	15	18	21	24	27	30
1500	334	534	71/2	916	111/2	15	1834	221/2	2616	30	3334	371
1800	41/2	634	9	1114	1335	18	221/2	27	311/2	36	401/2	
2000	5	71/2	10	1216	15	20	25	30	35	40	45	50
2400	6	9	12	15	18	24	30	36	42	48	54	60
2800	7	1016		1716	21	28	35	42	49	56	63	70
3000	716	111/4	15	1834	221/2	30	371/2	45	521/2	60	671/2	75
3500	834	13	171/2	22	26	35	44	521/2		70	79	88
1000		15	20	25	30	40	50	60	70	80	90	100
1500	1114	17	221/2	28	34	45	57	69	78	90	102	114
5000	121/2	19	25	31	3716	50	621/2	75	8716	100	112	125

For double belts see page 124.

Table for Calculating Horse Powers Which May Be Transmitted by Steel Pullets Based on 180° Arc of Belt Contact and 125 Lbs. Pull per Inoh Width of Face. This Table Applies to Stock Pulleys. Am. Steel Pulley Co., Phila., Pa.

3         4         5         6         8         10         12           000         016         000	-			acce of a through in access						
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024 025 036 036 036 036 036 036 036 036 036 036	- <u>:</u>		<u>:</u>	<u>:</u> :	<u>:</u> -:	-:	-		:	
0.24 6.00 0.02 0.02 0.02 0.02 0.02 0.02 0.02		:	:	:		:				
0.00			-	-		-				:
0.00   0.45   0.64   0.64   0.69   0.60										
10.0   10.0										
044 055 066 080 1100 044 056 072 080 1100 058 076 073 094 1110 058 076 078 1101 059 076 078 1101 050 077 080 1110 050 077 080 1120 050 077 080 1101 050 077 080 081 077 080 081 078 078 110 120 078 110 120 130 078 110 120 144 078 079 1100 079 110 120 144 079 070 120 070 070 070 070 070 070 070 070 070 07										
0.04 0.65 0.66 0.88 110 0.05 0.06 0.75 0.75 0.75 0.75 0.75 0.75 0.75 0.75	_									
0.066 0.072 0.066 120 0.065 0.073 0.066 120 0.066 0.075 0.066 120 0.066 0.075 0.066 120 0.067 0.075 0.066 120 0.068 0.066 120 0.069 1.06 120 0.060 1.06 126 144 0.060 1.06 126 146 0.060 1.06 126 146 0.060 1.06 126 146 0.060 1.06 126 166 0.060 1.06 126 166 0.060 1.06 146 182 0.060 1.06 146 192 0.060 1.06 144 192 0.060 144 144 144 144 144 144 144 144 144 14			<u>-</u> -	_	<u>.                                    </u>	<u>:</u>				
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0.00 (0.0) (		:	:	<u>:</u> ::	<u>:</u> :	:	:	:	:	:
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111111650 11111111111650 111111111111111	multiply number of revolutions per minute by number in table o width of pulley fac—or Width of pulley fac—or (At 125 lbs. Per Inch Width of Belt) en pulley to transmit a given horse power, divide H. P. by number h width of pulley face—or (At 125 lbs. Per Inch Width of Belt) for Double Belt H. P. + NO (Form Table) — Rev. per Min.
400 6524 6624 6630 6630 6632 6632 6632 6632 6632 6632	umber in  = Horse h Width of H. P. by Rev. per Width of 1
	Wide Wild
3300 4456 456 456 6612 66	y n bble) Incl vide
22.00   2	ions per minute by nn X NO. (From Table) (At 125 liss. Per Inche en horse power, divide NO (Form Table) = (At 125 liss. Per Inch i
	Fron Ibs.
1100 1144 1144 1160 1160 1160 1160 1160	kions per minu X NO. (Froi (At 125 lbs. en horse power NO (Form T (At 125 lbs.)
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44444444444444444444444444444444444444	will transmit, 5 lbs. per inch sesary for a giv 75 lbs. per incl 11 Figures are
83888888888888888888888888888888888888	n pulley will transmit, multiply numbe pull of 75 lbs. per inch width of pulley nute necessary for a given pulley to tra t pull of 75 lbs. per inch width of pulle Note—All Figures are for Double Belt
	belt pull of er minute
<u></u>	Selli et e
	s per last
	pow nort tion
	or a or a volu for a
	d be
<u> </u>	To find horse power a lt by 3.5 for a normal   To find revolutions pe lt by 1.66 for a normal
2245888284888244888884888884888884888884888888	To find horse power a given pulley will transmit, multiply number of revolution result by 3.5 for a normal belt pull of 75 lbs. per inch width of pulley fase—or. R. P. M. X. To find revolutions per minute necessary for a given pulley to transmit a given result by 1.66 for a normal belt pull of 75 lbs. per inch width of pulley face—or Note—All Figures are for Double Belt H. P. + N. (A.

lkiply xr a lbs. face although the lbs. lbs. lbs. lbs. face face

DOUBLE BELTS
(Continued from page 121.)

Feet					Widt	h of Bel	t in Inc	hes			
Speed in Feet per Minute	4	6	8	10	12	14	16	18	20	22	24
~~~	H.P.	н.Р.	н.Р.	Н.Р.	н.Р.	H.P.	H.P.	H.P.	H.P.	н.Р	н.Р.
400	23/4	41/4	53/4	71/4	81/2	10	111/2	13	141/2	16	171/9
600		$6\frac{1}{2}$	834	11	13	15	171/2	191/2	22	24	26
800	534	81/2	111%	141/2	171/2	201/2	23	26	29	32	341/2
1000	71/4	11	14 1/2	1814	21 1/2	251/2	29	321/2	36	40	431/2
1200		13	171/2	22	26	301/2	341/2	39	44	48	$52\frac{1}{2}$
1500	103/4	161/4	$21\frac{37}{4}$	271/4	321/2	38	431/2	49	541/2	60	651/2
1800	13	191/2	26	$32\frac{3}{4}$	39	451/2	52	59	651/2	72	781/2
2000	141/2	$21\frac{3}{4}$	29	361/2	431/2	501/2	58	651/2	721/2	80	87
2400	$17\frac{1}{4}$	26	34 3/4	44	$52\frac{1}{2}$	601/2	$69\frac{1}{2}$	781/2	88	96	105
2800	$20\frac{1}{4}$	301/9			61	71	81	911/2	102	112	122
3000	$21\frac{1}{2}$	$32\frac{1}{2}$	431/2	541/2	651/2	76	871/2	98	108	120	131
	$25\frac{1}{2}$			631/2	76	89	101	114	127	140	153
4000	29 2	$43\frac{1}{2}$			87	101	116	131	145	160	174
	$32\frac{1}{2}$	49 ~		82		114	131	147	163	180	196
5000	$36\frac{1}{2}$	541/2		91	109	127	145	163	182	200	218
	' -	- 1	[ [								ļ

[Foote Bros. Gear & Mach. Co., Chicago]

For single belts see page 121.

# LENGTH OF BELT FOR A GIVEN DRIVE

C = distance between centers of pulleys.

R = radius of large pulley.
r = " " small "

A = arc of contact of large pulley.

B = "" " small

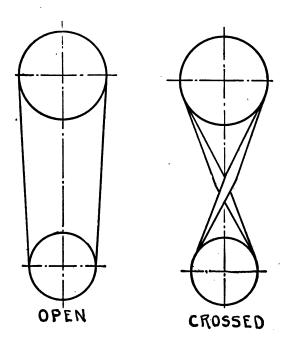
Length of open belt = A + B +  $2\sqrt{C^2 - (R - r)^2}$ 

" crossed belt = A + B +  $2\sqrt{C^2 - (R + r)^2}$ 

# **BELT DRIVES**

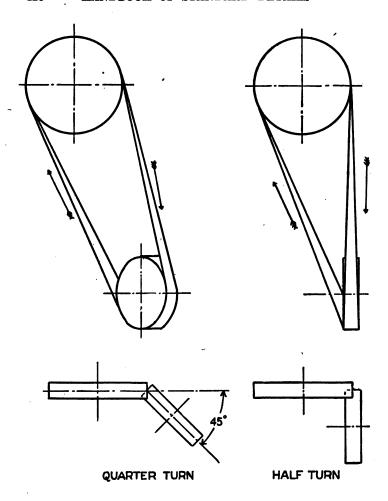
Power may be lost by journal friction and belt slipping. To prevent the former the belt should not be run too tight. As to belt slipping, this may be largely overcome by applying a dressing.

Shafts with Parallel Axes.—Here the center line of the driving and following sides of the belt fall in the middle planes of both pulleys—hence the belt can run in either direction. The arc of contact of crossed belts is equal on both pulleys and is always more than 180 degrees. The gain in contact is lost by the twist in the belt, which causes it to run unevenly on the pulley. However, the arc is generally taken at 180 degrees in making calculations.



Shafts in Parallel Planes but Inclined to Each Other.—The center line of the driving side of the belt is in the middle plane of both pulleys, but the following side is not—thus the belt can run in one direction only.

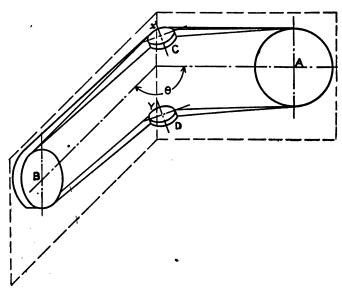
Shafts with Inclined Axes.—A and B (page 127) are the centers of two pulleys,  $\theta$  being the angle between their planes A x y and B x y. Any two points as x and y are taken on the line of inter-



section x y of the planes, and tangents drawn to the pulleys A and B. The center circles of the guide pulleys C and D must be tangent to the tangents drawn from x and y, to the pulleys A and B.

#### BELT DRIVE WITH SHAFTS AT INCLINED AXES

(See page 125.)

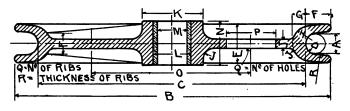


#### ROPE DRIVES

Transmission rope is made from hemp or manila fibres with 3, 4 or 6 strands, the 3 strands for small drives and the 4 and 6 for large drives. A table of 4-strand manila rope is given on page 129.

# WIRE ROPE SHEAVES (Cast Iron)

(See next page for table.)



ROPE SHEAVES AND PULLEYS (See page 127.)

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[Upson-Walton Co., Cleveland, O.]

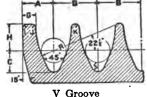
MANILA TRANSMISSION ROPE

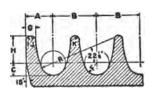
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.90   2	21125   12	60
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[T. B. Wood's Sons Co., Chambersburg, Pa.]

American system of rope transmission has one continuous rope winding from one groove or sheave to another. In this system a uniform tension is kept on the rope, by a traveling tension carriage.

# . . Dodge Standard 60° V and U Grooves FOR AMERICAN SYSTEM ROPE TRANSMISSION



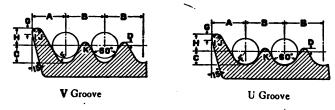


U Groove

Rope Size	A	В		U Gr.	D	ļī	U Gr.	G	н	I	J	к
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 11/8 11/4 13/8 11/2 15/8 13/4 2 21/4	11/4 13/8 11/2 15/8 13/4 17/8 2 21/2 23/4	5/8 11/6 3/4 15/6 7/8 1 11/8	3/8 - 7/66 1/3 9/6 5/8 11/6 8/4 7/8	100000000000000000000000000000000000000	**************************************	3,8 7,66 1,2 9,66 5,8 11,16 3,4 7,8	\$ 15 15 15 15 15 15 15 15 15 15 15 15 15	1 2 9 16 1 18 1 18 1 18 1 18 1 18 1 18 1 18		10000000000000000000000000000000000000	SA S

In the English or separate warp system, a single endless rope is required for each groove or sheave. The English system is now little used except in main drives, as from engine to countershaft.

### Engineers' Standard V and U Grooves For English System Rope Transmission



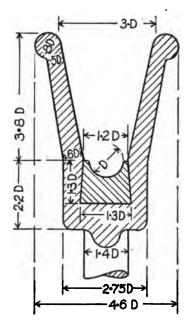
Rope		.*		(	2	]	F	, G	*			
Rope	V Gr.	U Gr.	В	V Gr.	U Gr.	V Gr.	U Gr.	V Gr.	U Gr.	H	I	JК
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<sup>\*</sup> A and G dimensions for ONE V Groove same as for U Grooves.
[Dodge Sales & Eng'g Co., Mishawaka, Ind.]

Wire rope may also be used for drives. The average speed for wire and manila rope is 4500 ft. per min.

The larger the sheaves, the lower is the operating cost as the rope wears longer. A single sheave with a filler is not suitable for transmitting more than 300 H.P., hence it is often necessary to have pulleys with a number of grooves. U grooves are preferable for outdoor service. When the distance between the driving and the driven pulley exceeds 150 ft. an idler should be installed.

### WIRE ROPE PULLEY FOR POWER TRANSMISSION



D = diameter of rope in inches.

Number of arms, 6 for pulleys 2 to 4 ft. dia., 8 from 5 to 8 ft.

Arms have elliptic cross section, short dial given in figure, long  $\sqrt{1.5}$  times short.

Pulley of cast iron, rope runs on a leather filler.

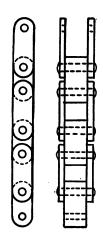
Diameter of pulley not less than 36 D.

Length of hub 2 to 2½ times dia. of shaft.

If a pulley with wider sides is required have the angle between the sides 60 degs. and the grooves for the rubber 30 degs.

## CHAINS FOR TRANSMITTING POWER

Block Chains are for small power drives where the speed is from 600 to 800 ft. per min.



SIZES OF BLOCK CHAIN

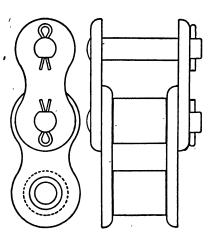
The letters in the table refer to sprocket wheel on page 135.

11_													
Dia. of		Ή	P.	Max.	Pull lbs.	lbs.	Wt. per	<u></u>	Ħ	٦	ß	E	ء
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3		1.4	4.0	2225	<b>%</b>	160	88	.595	3	23	2	ړٍځ	₹∊
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.532		က က	6.6	1213	133	398	83	868	534	781	.00	8	721
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In the column Chain Number—the second number as 14, 1/4, etc. is the width of the chain. [Diamond Chain & Mfg. Co., Indianapolis, Ind.]

### ROLLER CHAINS

Roller Chains are for heavier loads than block and for speeds of 800 to 1,200 ft. per min.



Referring to the figure, a roller and pin are shown in the center, at the left a roller and at right a pin. chain is made up of rollers and pins (as the center in the figure) with alternate in and out links.

# ROLLER CHAINS FOR TRANSMITTING POWER

Sizes Recommended by Soc. of Automotive Engineers and Am. Soc. of Mechanical Engineers

Chain	1772	Dia. of	H.	Н. Р.	Max.	Pull lbs.	lbs.	Wt. per	-	;		F		
Number	rice	roller	Normal	Max.	R. P. M.	Normal	Max.	ft. Ibs.	٦ .	4		<b>a</b>	٠.	뉙
×	122	.306	:	:		:	•			:	i	:	:	:
149 x 3%	100%	.400	2.7	18.1	1993	108	325	.619	.822	.551	%. E	.056	, , , , , , , , , , , , , , , , , , ,	7,5
××	1 4	625	2.0	22.0	926	292	877	8.2	1.45	220		88	%%	2,7 2,7
160 x 34	11%	.75	6.6	29.7	640	396	1189	2.69	1.73	1.18		.113	1. 2./2	;;;
162 x 1	$\frac{11}{2}$	.875	15.7	47.2	200	629	1888	4.15	2.20	1.40		. 135	15,78	13%
164 x 1	13%	1.000	18.0	54.0	888	220	2160	4.96	2.24	1.65		%	, e.	3
168 x 11/4	7	1.125	24.4	73.1	334	975	2925	6.32	2.65	1.90		180	15%	1%
:	272	1.562	:	:	:	:	:	:	:	:		:	:	:
Ē	-   5					,								

[Diamond Chain & Mfg. Co., Indianapolis, Ind.]

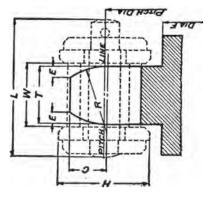
Letters L. H. etc., refer to wheel, page 135.

The normal pull given in the table corresponds to a pressure of 1,000 lbs. per sq. in. of projected rivet area. The maximum pull is about three times the normal pull, but does not exceed one-tenth of the ultimate strength of the chain.

The projected rivet area for any chain may be found by dividing the number representing the normal pull by 1,000. For example, the normal pull for chain 160 x ¾ is 396 lbs., and the projected rivet area is .396 sq. ins. Projected rivet area is the product of the rivet diameter and the length of the bushing in which the rivet turns.

The maximum horse power given is the maximum only when the chain pull does not exceed the limit The normal horse power given in the table corresponds to the normal pull at a chain speed of 800 ft. per given in the sixth column of table on page 134.

Sprocket teeth cross sections are given in columns C, E, T and R. F in the figure is the diameter of the rim or hub. It should not exceed pitch diameter minus  $1.1 \times H$  as clearance must be allowed for the side bars of the chain.



Silent Link.—The Morse Chain, page 137, (Morse Chain Co., Ithaca, N.Y.), is an example of this type. The important feature is the rocker joint, one of the pins being the seat pin and the other the rocker. The manufacturer's claim, 1st, positive speed ratio between driving and driven shafts with the added feature of flexibility, 2nd, 98½ to 99% sustained efficiency, 3rd, quietness at high speeds and 4th, long life.

DATA TO BE USED IN THE DESIGN OF MORSE CHAINS

Pitch, inches	<b>%</b>	Z.	%	%	9/10	12/10	11/2	73	က
Small sprocket driver	85	£1;	13	13	15	15	17	17	17
Small sprocket driven Desirable number of teeth in	51		<u> </u>	77	3	3	 8	31	35
	15-17	15-17	17-21	17-21	17-23	17-23	17-27	17-31	19-31
sprockets. (See Note 3)	75	8	109	115	125	129	129	129	131
driven sprockets	35-45	55-75	55-75	55-85	55-95	55-105	55-115	55-115	55-115
To find pitch diameter of wheel multiply number of teeth by (inches) Addendum. For outside diam-	0.1193	0.159	0.199	0.239	0.2865	0.382	0.477	0.636	0.955
eter of sprockets 33 to 130 1. (See Note 1) inches. Maximum R. P. M.	9,000	0.05	0.00	0.075	0.09	0.12 800	0.15	0.20	0.30 250
readial clearance beyond tooth required for chain, inches	0.375	0.50	0.62	0.75	0.90	1.2	1.5	2.0	3.0
Small sprocket driver	88	88	900	120 95	150	000 1600	270 210	450 350	750
Approximate weight of chain per inch width, I foot long, pounds C for solid pinions	0.75 0.003 0.10	1.00 0.0045 0.16	1.25 0.0063 0.25	1.50 0.009 0.35	1.80 0.013 0.45	2.40 0.023 0.7	3.00 0.035 1.0	4.00 0.058 2.0	6.00 0.145 4.0

Note 1.—Number of teeth = T.

Exact outside diameter = D.

When T has less than 33 teeth, D = pitch diameter.

When T has more than 32 teeth, D = pitch diameter.

when I has more used as occur, D = prom usure eter + (2 x addendum).

Note 2.—Use sprockets having an odd number of teeth whenever

possible.
Note 3.—When specially authorised, a larger number of teeth than shown may be cut in large sprocket.

Note 4.—Thickness of sprocket rim, including teeth should be at least 1.2 times the chain pitch.

Note 5.—The number of grooves in the sprocket, their width and distance apart varies according to pitch and width

of chain. Note 6.—The width of the sprocket should be  $\frac{1}{2}$  to  $\frac{1}{2}$  inch greater than nominal width of the chain.

Note 7.—An even number of links in the chain and an odd number of teeth in the wheels are desirable.

Note 8.—Horisontal drives preferred; tight chain on top desirable for short drives without center adjustment.

able for short drives without center adjustment.

Note 9.—Adjustable wheel centers desirable for horisontal
drives and necessary for vertical drives.

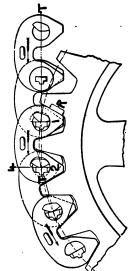
Note 10.—Avoid vertical drives.

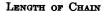
Note 11.—Allow a side clearance for chain (parallel to axis of sprockets and measured from nominal width of

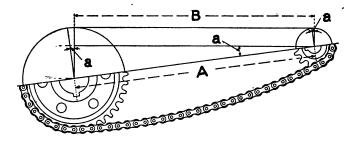
chain) equal to the pitch.

Note 12.—Maximum linear velocity for commercial service 1200
to 1600 feet per minute.

Referring to the figure the link contact with the teeth is resisted at R which is below the line of tension T T, while the resultant force F due to the lever socion tends to maintain the chain link at its true pitch diameter while in contact with the wheel. The rolling action is shown by the two positions of the joint pins at I and 2.







N = number of teeth on large sprocket

n = '" " " small "

R = radius of large sprocket, ins.

r = " "small

P = pitch of chain, ins.

A = distance between centers in pitches.

 $B = A \cos a$ 

Chain lengths in pitches = 
$$2 A + \frac{N+n}{2} + \frac{\left(\frac{N-n}{2 n}\right)^2}{c}$$
  
=  $2 A + \frac{N+n}{2} + \frac{.0257 (N-n)^2}{c}$ 

If the chain length in pitches comes a fractional part of a pitch, use the next whole number. The length of chain in inches is equal to the product of the number of pitches by the pitch.

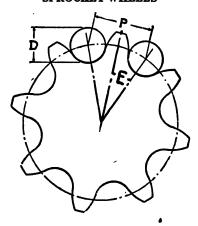
Chain length in inches = 
$$NP\left(\frac{180^{\circ} + 2a}{360^{\circ}}\right) + nP\left(\frac{180^{\circ} - 2a}{360^{\circ}}\right) + 2A \cos a$$

Distance A between centers should not be less than  $1\frac{1}{2}$  times the diameter (2 R) of the larger sprocket nor more than  $60 \times P$ .

In using the above formula for calculating the length of block chains, the length should be a multiple of the pitch. For roller, the length is a multiple of two times the pitch, as the ends have to be joined by an inside and outside link. A sprocket wheel should not have less than 15 teeth. On sprockets of the same diameter a short pitch chain will last longer and run more quietly than a long pitch.

As to tooth forms, the Diamond Chain & Manufacturing Co. has developed a tooth having a constant pressure angle and a variable space angle. A large pressure angle is one of the advantages claimed. Besides, an elongated chain will run as well on a 100 tooth sprocket as on a 20.

### SPROCKET WHEELS



### DIAMETERS OF SPROCKET WHEELS FOR BLOCK CENTER AND TWIN ROLLER CHAINS

P = pitch of chain

N = number of teeth in sprocket

$$E = \frac{180}{N}$$

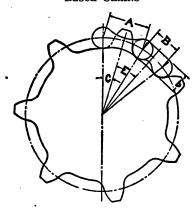
Pitch dia.  $=\frac{P}{\sin E}$ 

D = diameter of roller

Outside diameter of sprocket wheel =  $\frac{P}{\sin E}$  + D

Bottom " " = 
$$\frac{P}{\sin E}$$
 — D

DIAMETERS OF SPROCKET WHEELS FOR ROLLER AND BUILT UP BLOCK CHAINS



$$A = \text{center to center of holes in side links (usually .6)}$$

$$B = " " " " " \text{chain block (usually .4)}$$

$$b = \text{diameter of round part of chain block (usually .325)}$$

$$N = \text{number of teeth}$$

$$E = \frac{180^{\circ}}{N}$$

$$\text{Tan } C = \frac{\sin E}{\frac{B}{A} + \cos E}$$

Pitch dia. = 
$$\frac{A}{\sin C}$$

Outside diameter of sprocket wheel  $=\frac{A}{\sin c} + b$ Bottom " "  $=\frac{A}{\sin c} - b$ 

[Whitney Mfg. Co., Hartford, Conn.]

### **Formulae**

Pitch dia. approx. of sprocket wheel = .318  $\times$  number of teeth  $\times$  pitch ins.

Chain pull in pounds =  $\frac{33,000 \times \text{horse power}}{\text{vel. of chain ft. per min.}}$ 

[Diamond Chain & Mfg. Co., Indianapolis.]

### GEARING

### SPUR GEARS

Circular pitch (P') is the distance measured along the pitch circle from the center of one tooth to the center of the next. Circular 3 1416

$$pitch = \frac{3.1410}{diameter pitch.}$$

Diametral pitch (P) is the number of teeth to each inch of the pitch diameter. Diametral pitch =  $\frac{3.1416}{\text{circular pitch.}}$ 

Addendum is the distance from the pitch circle to the outside diameter.

Dedendum is the distance from the pitch circle to the bottom of the working depth.

Clearance is the distance from the working depth to the bottom of the tooth.

P' = circular pitch.

P = diametral pitch.

D' = diameter of pitch circle.

D = outside diameter.

N = number of teeth.

a = addendum.

c = clearance.

t = thickness of tooth.

Then

$$P' = \frac{3.1416}{P} = \frac{D}{.3183N + 2} = \frac{D'}{.3183N}$$

$$P = \frac{3.1416}{P'}$$

$$D' = .3183 N P' = \frac{N D}{N + 2} = N a$$

$$D = a (N + 2) = .6366 P' + D'$$

$$a = .3183 P'$$

$$c = .05 P = \frac{t}{10}$$

$$t = \frac{P'}{2}$$

Usual width of face of spur gears is 21/2 to 3 times the circular pitch.

Small pinions which run with large diameter gears should be shrouded as the shrouding gives additional strength to the pinion. The shrouding on each side may be taken equal to .4 circular pitch plus 1/8 in.

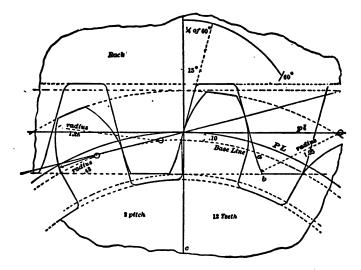
Tooth Forms.—Gear teeth may be constructed with involute, epicycloid or hypocycloid curves (see pages 23-22). The curve generally selected is the involute above the pitch line with radial flanks. The outlines of involute and epicycloidal teeth may be laid out by Grant's odontograph.

Involute gears to be interchangeable must have the same angle of obliquity. Gears with cycloidal tooth outlines to be interchangeable must have the same rolling circle on both flanks and faces.

The addendum line is drawn outside of the pitch line at a distance equal to one divided by the diametral pitch, or to one-third of the circular pitch. The dedendum line is inside of the pitch line by the same distance. The clearance line is inside of the dedendum line by one-eighth of this distance. The base line is inside of the pitch line by one-sixtieth of the pitch diameter.

To Draw a Gear.—Draw the pitch line, addendum, dedendum, clearance and base lines. Space the pitch line for the tooth points, either by dividing the full circle, or by stepping off half the circular pitch.

In the odontograph table at 12 teeth (the number of teeth in the gear to be drawn), is found the face radius 2.51 and this, divided by the diametral pitch 2, gives 1.25. With compass set to this face radius viz. 1.25 draw the faces of the teeth from the addendum



line to the pitch line, from centers on the base line. If the number of teeth is greater than 36, or if the pitch is small, this face radius should be continued to the base line.

At twelve teeth in the table is found the flank radius .96, and this divided by the diametral pitch gives a quotient of .48. With the compass set to .48, and from centers on the base line, draw in all the flanks of the teeth from the pitch line to the base line.

From the base line continue the flanks of the teeth to the dedendum line by straight radial lines, and round them into the clearance line, completing the teeth.

To Draw a Rack.—Draw straight lines at an angle of 15 degs. with the radius line. The point of the tooth, from the halfway point to the point b must be rounded over by an arc drawn from a center on the pitch line, and with the compasses set to 2.10 ins. divided by the diametral pitch, or .67 inch multiplied by the circular pitch.

Grant's Odontograph for Involute Teeth

Pressure angle $= 15$ degs.	Addendum = .3183 × circular pitch =	
1	$\cdot$ Clearance = $\frac{\text{addendum}}{2}$	
diametral pitc	h 8	

No.	.Divide diametr		Multiply circular	by the pitch	Number	Divide diametr		Multipl circula	y by the r pitch
of teeth	Face rad.	Flank rad.	Face rad.	Flank rad.	of Teeth	Face rad.	Flank rad.	Face rad.	Flank rad.
10	2.28	.69	.73	.22	28	3.92	2.59	1.25	.82
11	2.40	.83	.76	.27	29	3.99	2.67	1.27	.85
12	2.51	.96	.80	. 31	30	4.06	2.76	1.29	.88
13	2.62	1.09	.83	.34	31	4.13	2.85	1.31	.91
14	2.72	1.22	.87	.39	32	4.20	2.93	1.34	. 93
15	2.82	1.34	.90	.43	33	4.27	3.01	1.36	.96
16	2.92	1.46	. 93	.47	34	4.33	3.09		.99
17	3.02	1.58	.96	.50	35	4.39	3.16		1.01
18	3.12	1.69	.99	. 54	36	4.45	3.23		1.03
19	3.22	1.79	1.03	. 57	37–40	4.2	4.2	1.34	1.34
20	3.32	1.89	1.06	.60	41–45	4.63	4.63		1.48
21	3.41	1.98	1.09	.63	46-51	5.06	5.06	1.61	1.61
22	3.49	2.06	1.11	.66	52-60	5.74	5.74		1.83
23	3.57	2.15	1.13	.69	61–70	6.52	6.52	2.07	2.07
24	3.64	2.24	1.16	.71	71-90	7.72	7.72		2.46
25	3.71	2.33	1.18	.74	91-120		9.78		3.11
26	3.78	2.42	1.20	.77	121-180		13.38		4.26
27	3.85	2.50	1.23	.80	181–360	21.62	21.62	6.88	6.88

[Phila. Gear Works, Phila., Pa.]

Grant's Odontograph for Epicycloidal Teeth

Addendum = .3183 × circ. pitch =  $\frac{1}{\text{dia'l pitch}}$ . Clearance =  $\frac{\text{addendum}}{8}$ 

	mber of	For any o	one d ther p	iametral p pitch, divid pitch	itch: for le by that	For any	othe	. circular properties of the circular pitch in the circular pitch	pitch, for ltiply by
		Fac	es	Fla	nks	Fa	ces	Fla	nks
Ex- act	Inter- vals	Rad.	Dis- tance	Rad.	Dis- tance	Rad.	Dis- tance	Rad.	Dis- tance
10	10	1.99	.02	- 8.00	4.00	. 62		-2.55	1.27
11	11	2.00		-11.05		.63	.01	-3.34	2.07
12	12	2.01			Straight		.02	Straight	
13⅓	13-14	2.04	.07	15.10	$9.4\bar{3}$	.65	.02	4.80	3.00
$15\frac{1}{2}$	15-16	2.10	.09	7.86	3.46	.67	.03	2.50	1.10
$17\frac{1}{2}$		2.14	.11	6.13	2.20	.68	.04	1.95	.70
20	19–21	2.20	. 13	5.12	1.57	.70	.04	1.63	.50
23	22-24	2.26	. 15	4.50	1.13	.72	. 05	1.43	.36
27	25-29	2.33	.16	4.10	.96	.74	. 05	1.30	.29
33	30-36	2.40	. 19	3.80	.72	.76	.06	1.20	.23
42	37-48	[2.48]	. 22	3.52	.63	.79	.07	1.12	.20
58	49-72	2.60	. 25	3.33	.54	.83	.08	1.06	.17
97	73-144	2.83	.28	3.14	.44	.90	.09	1.00	.14
290	145-300	2.92	.31	3.00	.38	. 93	. 10	. 95	.12
Rack	Rack	2.96	.34	2.96	.34	.94	.11	.94	.11

[Phila. Gear Works, Phila., Pa.]

### Stub Teeth

Stub teeth generally have a pressure angle of 20 degs., and the distance from the pitch diameter to the end of the tooth less than in ordinary teeth. For instance, for a 6 pitch tooth an 8 pitch addendum is used, as per following table which gives dimensions of stub teeth.

Diam- etral pitch	Thick- ness on pitch line	Adden- dum	Deden- dum	Diam- etral pitch	Thick- ness on pitch line	Adden- dum	Deden- dum
4/5	.3927	.2000	.2500	8/10	.1962	.1000	.1250
5/7	.3142	.1429	.1785	9/11	.1744	.0909	.1137
6/8	.2617	.1250	.1562	10/12	.1571	.0833	.1042
7/9	.2243	.1111	.1389	12/14	.1308	.0714	.0893

CIRCULAR PITCH

With its Equivalent in Diametral Pitch, Depth of Space and Thickness of Tooth

Circular	Diametral	Thickness of Tooth	Depth to be	Addendum
Pitch	Pitch	On Pitch Line	Cut in Gear	
6	.5236	3.0000	4.1196	1.9098
5	.6283	2.5000	3.4330	1.5915
4	.7854	2.0000	2.7464	1.2732
3½	.8976	1.7500	2.4031	1.1140
$3 \\ 2\frac{3}{4} \\ 2\frac{1}{2} \\ 2\frac{1}{4}$	1.0472	1.5000	2.0598	.9550
	1.1424	1.3750	1.8882	.8754
	1.2566	1.2500	1.7165	.7958
	1.3963	1.1250	1.5449	.7162
$2 \\ 178 \\ 134 \\ 158$	1.5708	1.0000	1.3732	.6366
	1.6755	.9375	1.2874	.5968
	1.7952	.8750	1.2016	.5570
	1.9333	.8125	1.1158	.5173
$   \begin{array}{c}     1\frac{1}{2} \\     1\frac{3}{8} \\     1\frac{1}{4} \\     1\frac{1}{8}   \end{array} $	2.0944	.7500	1.0299	.4775
	2.2848	.6875	.9441	.4377
	2.5133	.6250	.8583	.3979
	2.7925	.5625	.7724	.3581
1 15 16 7 8 13 16	3.1416 3.3510 3.5904 3.8666	.5000 .4687 .4375 .4062	.6866 .6437 .6007 .5579	.3183 .2984 .2785 .2586
3/4 11/16 5/8	4.1888 4.5696 5.0265 5.5851	.3750 .3437 .3125 .2812	.5150 .4720 .4291 .3862	.2387 .2189 .1989 .1790
1/2	6.2832	.2500	.3433	.1592
7/16	7.1808	.2187	.3003	.1393
3/8	8.3776	.1875	.2575	.1194
6/16	10.0531	.1562	.2146	.0995
14	12.5664	.1250	.1716	.0796
18	25.1327	.0625	.0858	.0398
18	50.2655	.0312	.0429	.0199

DIAMETRAL PITCH
With its Equivalent in Circular Pitch, Depth of Space and Thickness of Tooth

Diametral	Circular	Thickness of Tooth	Depth to be	Addendum
Pitch	Pitch	on Pitch Line	Cut in Gear	
1/2	6.2832	3.1416	4.3142	2.0000
3/4	4.1888	2.0944	2.8761	1.3333
1	3.1416	1.5708	2.1571	1.0000
11/4	2.5133	1.2566	1.7257	.8000
$1\frac{1}{2}$ $1\frac{3}{4}$ $2$ $2\frac{1}{4}$	2.0944	1.0472	1.4381	.6666
	1.7952	.8976	1.2326	.5714
	1.5708	.7854	1.0785	.5000
	1.3963	.6981	.9587	.4444
$2\frac{1}{2}$ $2\frac{3}{4}$ $3$ $3\frac{1}{2}$	1.2566	.6283	.8628	.4000
	1.1424	.5712	.7844	.3636
	1.0472	.5236	.7190	.3333
	.8976	.4488	.6163	.2857
4	.7854	.3927	.5393	.2500
5	.6283	.3142	.4314	.2000
6	.5236	.2618	.3595	.1666
7	.4488	.2244	.3081	.1429
8	.3927	.1963	.2696	.1250
9	.3491	.1745	.2397	.1111
10	.3142	.1571	.2157	.1000
11	.2856	.1428	.1961	.0909
12	.2618	.1309	.1798	.0833
14	.2244	.1122	.1541	.0714
16	.1963	.0982	.1348	.0625
18	.1745	.0873	.1198	.0555
20	.1571	.0785	.1079	.0500
22	.1428	.0714	.0980	.0455
24	.1309	.0654	.0898	.0417
26	.1208	.0604	.0829	.0385
28	.1122	.0561	.0770	.0357
30	.1047	.0524	.0719	.0333
32	.0982	.0491	.0674	.0312
36	.0873	.0436	.0599	.0278
40	. 0785	. 0393	. 0539	.0250
48	. 0654	. 0327	. 0449	.0208

### Horse Power and Working Loads of Cut Cast Iron Spur Gears

Under the heading W L is given the working load or number of pounds of power transmitting strain which can safely be brought on each inch width of tooth of a cut cast iron gear or pinion of the size indicated at left of table, when it is running at the speed listed at top. For horse power and working loads of cut cast steel spur gear multiply the figures in the table by 204.

Under the heading H.P. this is converted into Horse Power transmitted at the speed named.

These figures should be multiplied by the width of working face in inches, for the power of the gear in question.

The feet per minute at pitch line equals pitch diameter in inches multiplied by revolutions per minute and by .2618.

SPEED OF PITCH LINE

Tag	Р	eth					F	eet p	er mi	nute				
Diametral Pitch	Arc Pitch	of Teeth	10	00	20	00	36	00	6	00	9	00	12	500
Ä	Ar	No.	w.l	н.Р.	w.L	H.P.	W.L	H.P.	w.l	н.р.	W.L	H.P.	w.l	н.р.
10	.3142	12 20 40 60 130	90 120 145 152 160	.27 .36 .44 .46 .49	79 105 127 133 140	.47 .63 .76 .80 .84	113 119	.85 1.02 1.07	85 89	.96 1.27 1.55 1.62 1.71	42 56 68 71 74	1.15 1.53 1.86 1.94 2.02	47 56	1.27 1.71 2.04 2.18 2.26
8	.392	12 20 40 60 130	113 150 180 190 200	.34 .45 .55 .58 .61	158 165	.78	116 141 148	.78 1.04 1.27 1.33 1.40	105 110	1.20 1.58 1.91 2.00 2.09	70 84 88	1.42 1.91 2.29 2.40 2.51	58 70 74	1.60 2.11 2.54 2.69 2.80
4	.785	12 20 40 60 130	380	.68 .91 1.09 1.15 1.21	260 315 330	1.17 1.56 1.89 1.98 2.10	230 280 295	1.58 2.08 2.52 2.68 2.79	175 210 220	2.36 3.18 3.82 4.00 4.18	140 170 177	2.86 3.82 4.64 4.83 5.05	116 140 147	3.16 4.22 5.09 5.35 5.64
3	1.047	12 20 40 60 130	300 400 480 503 530	1.45	350 420 440	1.56 2.10 2.52 2.64 2.77	310 373 391	2.08 2.79 3.36 3.52 3.70	232 280 295	3.18 4.22 5.10 5.37 5.64	185	3.82 5.05 6.14 6.42 6.77	155 187	4.22 5.64 6.80 7.13 7.50

(Continued on page 148.)

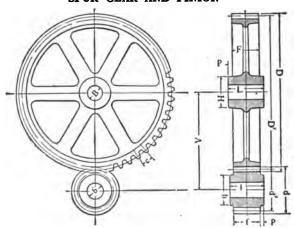
### SPEED OF PITCH LINE—Continued

Ē,	Pitch	seth					F	eet p	er mi	inute				
Diametral Pitch-	Arc. Pi	. of Teeth	10	00	2	00	8	00	6	00	9	00	1:	200
Д	⋖	No.	W.L	H.P.	W.L	н.р.	W.L	H.P.	w.L	H.P.	W.L	H.P.	W.L	H.P.
2	1.57	12 20 40 60 130	600 720 760	1.37 1.82 2.18 2.30 2.40	520 630 663	2.34 3.12 3.78 3.98 4.17	467 560 592	3.15 4.20 5.04 5.33 5.57		4.78 6.37 7.64 8.05 8.40	355	5.71 7.64 9.50 9.70 10.10	280 295	
11/2	2.09	12 20 40 60 130	800 963 1010	1.80 2.42 2.92 3.06 3.21	700 840 880	3.12 4.20 5.04 5.28 5.55	620 750 780	4.16 5.58 6.75 7.03 7.38	466 560 585	6.34 8.47 10.20 10.65 11.22	450 470	7.59 10.15 12.28 12.82 13.44	372 390	8.37 11.28 13.52 14.20 14.90

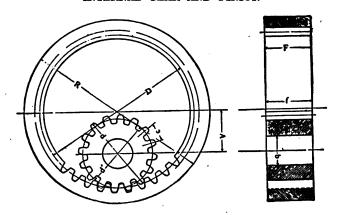
[Link Belt Co., Chicago, Ill.]

### Forms for Ordering

### SPUR GEAR AND PINION



### INTERNAL GEAR AND PINION



Gear			Pinion		
Number of Teeth			Number of Teeth		
Pitch { Circular Diametral	=	C	$\mathbf{Pitch.} \dots \left\{ \begin{matrix} \mathbf{Circular} \\ \mathbf{Diametral} \end{matrix} \right.$	=	c
Diametral	=		Diametral	=	
Face	=	$\mathbf{F}$	Face	=	f
Bore	=	В	Bore	_	b
Pitch Diameter	=	$\mathbf{D'}$	Pitch Diameter	=	d
Outside Diameter	=	D	Outside Diameter	=	d
Diameter of Hub	=	H	Diameter of Hub	_	h
Length of Hub	=	L	Length of Hub	=	l
Projection of Hub	=	$\mathbf{P}$	Projection of Hub	=	р
Keyway			Keyway		-
Material			Material	•	

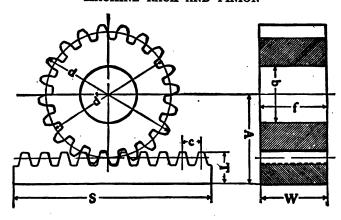
Distance between centers = A

### Materials for Gears

Gears may be of cast iron, cast steel, bronze or rawhide. Cast iron gears can be obtained either with cast (molded) teeth or generated (cut). Cast teeth are for rough drives but for accuracy, cut teeth are preferable; in any case a peripheral speed of 1,100 ft. per min. must not be exceeded as the noise becomes excessive. For working

loads of cast iron gears, see page 147. Rawhide gears run quietly, but the pressure on the teeth should not exceed 240 lbs. per in. of face.

### MACHINE RACK AND PINION



Rack			Pinion		
Pitch $.$ Circular $$ Diametral = 3.14	=	C	Number of Teeth		
Diametral = $3.14$	116-	⊦C	$     Pitch     {Circular \\ Diametral}   $	=	c
Thickness	==	T	Diametral	=	*
Face	=	W	Pitch Diameter	=	d
Length of Rack	=	S	Outside Diameter	==	ď
Material	=		Bore	=	b
			Face	=	f
Center of Pinion to Bot-			Keyway	_	
tom of Rack	=	A	Material	=	

<sup>\*</sup>Number of teeth to inch of Pitch Diameter.

[Foote Bros. Gear & Machine Co., Chicago, Ill.]

### MITER AND BEVEL

Miter gears have their axes meet at 90 degs., both gears being the same size. Bevel gears have their axes meet at other than 90 degs.

Center Angle.—Divide the number of teeth in the pinion by the number of teeth in the gear, the quotient is the tangent of the center angle of the pinion and cotangent of center angle of gear.

Increase Angle.—Divide double the sine of the center angle by the number of teeth in the pinion, the quotient is the tangent of increase angle for pinion or gear.

Face Angle.—Add the increase angle to the center angle of either gear, and the sum is the face angle.

Cut Angle.—Subtract the increase angle from the center angle of either gear, and the remainder is the cut angle.

Back Angle.—Subtract the increase angle from 90 degrees and the r mainder is the back angle for either gear.

Diameter Increase.—Double the cosine of the center angle and divide it by the diametral pitch, the quotient is the diameter increase, which added to the pitch diameter, is the outside diameter. The diameter increase is not the same for pinion and gear. They are calculated separate from center angles as above.

To Find the Length of Face on a Pair of Bevel Gears.—Multiply the secant of center angle of pinion by the radius of gear, and take one-third of product. Example: A gear is 6 ins. dia., and pinion 3 ins., find the fact of the gear.

$$\frac{3''}{6''}$$
 = .5000 = tangent of angle.

Secant of angle =  $1.1174 \times 3$ " (radius gear) = 3.352.

Face of gear = 
$$\frac{3.352}{3}$$
 = 1.11".

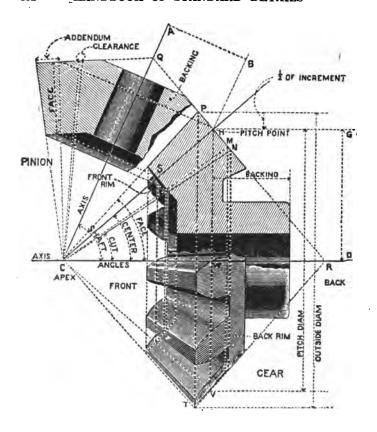
In bevel gears, to find the thickness of tooth at small end, divide the distance from apex to small end of tooth by the distance from apex to pitch diameter, and the quotient is the ratio. Multiply the thickness of tooth at pitch line by the ratio just found, and the product is the thickness of tooth at the pitch line of small end of tooth.

To find the pitch line at the small end of the tooth, multiply the ratio as obtained above by the addendum, the product is the addendum at the small end of the tooth.

[Foote Bros., Gear & Mach. Co., Chicago, Ill.]

To Draw a Pair of Bevel Gears at any Shaft Angle. (See page 152.)

—Draw the given axes A C and D C meeting at the apex C. Lay off the distances A B and D G equal to the pitch radii of the gears. Draw B H and G H parallel to the axes, and from their intersection, the pitch point H, draw the center line H C to the apex. Lay off H S equal to the given face. Draw Q H R at right angles to H C.



Lay off H P and H M each equal to the known addendum and M N equal to the known clearance. Draw P C, M C and N C.

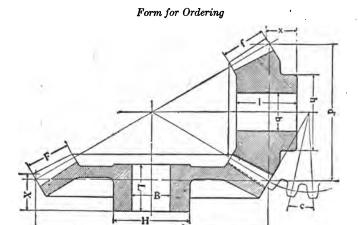
P C H is the increment angle or the addendum angle. P C D is the face angle, N C D is the cut angle.

The "backing" is the distance from the pitch line to the back end of the hub.

The small ends of the teeth are at the "front," and the large ends at the "back" of the gear.

The working pitch diameter of the gear is the diameter H V... The outside diameter is P T. The increment or difference between the pitch and the outside diameters, is variable with the angle of the gear, not being the same for all gears of the same pitch, as with spur gears.

[Phila. Gear Works, Phila., Pa.]

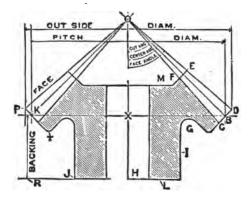


### Gear' Pinion Number of Teeth... Number of Teeth.... Circular.. Circular.. Face..... Face....... Bore..... Bore..... Pitch Diameter..... $\mathbf{D'}$ Pitch Diameter..... ď Backing..... $\mathbf{x}$ Backing..... x Length Through Hub. Length Through Hub. 1 Diameter of Hub..... н Diameter of Hub.... Keyway..... Keyway..... Material..... Material.....

When ordering either gear or pinion, always give number of teeth of mate. Distance x is sometimes taken to the pitch diameter—always state how it is taken.

<sup>\*</sup>Number of teeth to inch of pitch diameter.

### Mitre Gear Angles and Outside Diameter of One Diametral Pitch



NOTE—To obtain outside diameter, divide diameter given in table by the required diametral pitch. Angles given are fixed for the number of teeth as listed.

Number of teeth	Face Angle	Back Angle	O.D. for one Dia. Pitch	Number of teeth	Face Angle	Back Angle	O.D. for one Dia. Pitch
8	55.12	10.12	9.41	76	46.06	1.06	77.41
9	54.00	9.00	10.41	77	46.05	1.05	78.40
10	53.10	8.10	11.41	78	46.03	1.03	79.41
11	52, 36	7.36	12.41	79	46.02	1.02	80.41
12	51.75	6.75	13.41	80	46.00	1.00	81.41
13	51.23	6.23	14.41	81	46.00	1.00	82.41
14	50.79	5.79	15.41	82	45.98	.98	83.41
15	50.40	5.40	16.41	83	45.97	. 97	84.41
16	50.06	5.06	17.41	84	45.96	.96	85.41
17	49.80	4.80	18.41	85	45.95	. 95	86.41
18	49.50	4.50	19.41	86	45.94	.94	87.41
19	49.30	4.30	20.41	87	45.93	. 93	88.41
20	49.05	4.05	21.41	88	45.92	.92	89.41
21	48.86	3.86	22.41	89	45.91	.91	90.41
22	48.68	3.68	23.41	90	45.90	.90	91.41
23	48.52	3.52	24.41	91	45.89	.89	92.41
24	48.37	3.37	25.41	92	45.88	.88	93.41
25	48.24	3.24	26.41	93	45.88	.88	94.41
26	48.11	3.11	27.41	94	45.87	.87	95.41
27	48.00	3.00	28.41	95	45.87	.86	96.41
28	47.89	2.89	29.41	96	45.86	.85	97.41
29	47.79	2.79	30.41	97	45.86	.84	98.41
30	47.67	2.67	31.41	98	45.85	.83	99.41

Number of teeth	Face Angle	Back Angle	O.D. for one Dia. Pitch	Number of teeth	Face Angle	Back Angle	O.D. for one Dia. Pitch
31	47.61	2.61	32.41	99	45.85	.83	100.41
32	47.53	2.53	33.41	100	45.84	.82	101.41
33	47.45	2.45	34.41	102	45.79	.79	103.41
34	47.39	2.39	35.41	104	45.78	.78	105.41
35	47.31	2.31	36.41	105	45.77	.77	106.41
36	47.24	2.24	37.41	106	45.76	.76	107.41
37	47.19	2.19	38.41	108	45.75	.75	109.41
<b>3</b> 8	47.13	2.13	39.41	110	45.73	.73	111.41
39	47.08	2.08	40.41	112	45.72	.72	113.41
40	47.00	2.00	41.41	114	45.71	.71	115.41
41	46.97	1.97	42.41	116	45.70	.70	117.41
42	46.93	1.93	43.41	118	45.69	.69	119.41
43	46.88	1.88	44.41	120	45.68	. <b>6</b> 8	121.41
44	46.84	1.84	45.41	122	45.66	.66	123.41
45	46.80	1.80	46.41	124	45.65	.65	125.41
46	46.76	1.76	47.41	126	45.64	.64	127.41
47	46.72	1.72	48.41	128	45.63	.63	129.41
48	<b>46</b> .68	1.68	49.41	130	45.62	.62	131.41
49	46.65	1.65	50.41	132	45.61	.61	133.41
50	46.62	1.62	51.41	134	45.60	.60	135.41
51	<b>46.5</b> 8	1.58	52.41	136	45.59	.59	137.41
52	46.55	1.55	53.41	138	45.58	.58	139.41
53	46.52	1.52	54.41	140	45.57	.57	141.41
54	46.50	1.50	55.41	142	45.56	.56	143.41
55	46.47	1.49	56.41	144	45.55	. 55	145.41
56	46.44	1.44	57.41	146	45.55	55	147.41
57	46.41	1.41	58.41	148	45.55	.55	149.41
<b>5</b> 8	46.38	1.38	59.41	150	45.54	.54	151.41
<b>5</b> 9	46.35	1.35	60.41	152	45.54	.54	153.41
60	46.33	1.34	61.41	154	45.53	.53	155.41
61	46.32	1.32	62.41	156	45.52	.52	157.41
62	46.30	1.30	63.41	158	45.51	.51	159.41
63	46.28	1.28	64.41	160	45.50	.50	161.41
64	46.26	1.26	65.41				
65	46.24	1.24	66.41				
66	46.22	1.22	67.41			l	
67	46.20	1.20	68.41	1			
68	46.19	1.19	69.41			١	
69	46.18	1.18	70.41			١	
70	46.16	1.16	71.41			١	1
71	46.15	1.15	72.41				
72	46.11	1.11	73.41			١	
73	46.09	1.09	74.41			١	
74	46.08	1.08	75.41			١	
75	46.06	1.06	76.41				
		Ī		N.		1	1

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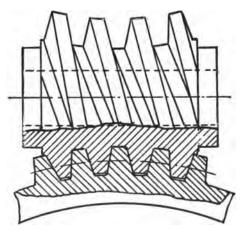
### WORM GEARING

Terms—pitch and diametral pitch are same as for spur gears. Lead = number of threads  $\times$  linear pitch. Linear pitch of worm = circular pitch of wheel. Normal pitch = cosine of lead angle  $\times$  linear pitch. Pitch dia. of wheel =  $\frac{\text{number of teeth} \times \text{cir. pitch.}}{\text{or of teeth}}$ 

Cotangent of lead angle =  $\frac{\text{pitch dia. of worm} \times \pi}{\text{lead}}$ . In gear table on pages 158 and 159, axial tooth angle = 60 degs., pressure angle = 30 degs.

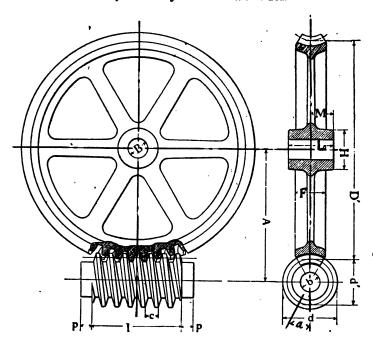
Worm wheels have straight or concave faces, an illustration of the latter is shown on page 157. Angle A is preferably 30 degs., although it may be between 30 and 35. Wheels may have the following proportions in terms of circular pitch P. Width of face = 2 P. Dimensions of tooth on pitch line, thickness = .49 P, height = .35 P, depth = .45 P.

### CURVED WORM



Worms are either straight or curved. The straight has a constant pitch diameter over its entire surface. In the curved, the worm has the form of an hour glass, the object being to get a greater surface contact than can be obtained with a straight worm. The Hindley worm is of the curved type. To get the maximum efficiency the worm should be as small in diameter as practical. Length generally six times the pitch.

### Form for Ordering Worm and Worm Gear



Worm Gear			Worm		
Number of Teeth Pitch (Circular) Face Bore Pitch Diameter Length Through Hub Projection from Center Keyway Material Right or Left Hand	= = =	C F B D' L M	Pitch (Distance from center to center of teeth.) Lead (Advance in one revolution) Pitch Diameter Outside Diameter Bore Length Projection of Hub Keyway Material. Right or Left Hand	<u> </u>	b
Distance between	een	Center	rs = A		

### WORMS AND GEARS

H. P. at 1000 R. P. M.	72	**	<b>ደ</b> ደ			22:	325	32	S	· •	'జ్లో	• •			ឌន
Used For	Engine Timing Gears Refrigerating Mach. Self Starter	Engine Timing Gears Refrigerating Mach. Refrigerating Mach.	Refrigerating Mach. Steering	Engine Timing Gears Small Tractor	Steering Small Pleasure Car	72 Ton Truck	72 Ton Truck	Industrial Truck	Industrial Truck Med. Size Touring	Industrial Truck	Med. Size Touring	Elec. Pleasure Car	Industrial Truck Industrial Truck	Utility Tractor	1 Ton Truck
Hand		LE HE													iHH iHi
Ctr's, Change Per Wheel Tooth	.1008	0593	0796	.1193	.1145	.1193	.1762	.0869	.13285	10796	1509	1112	1321	.1416	1691
Lead	1.90625	1.848	2.415	3.000	6.388	3.3211	5.5353	1.6386	2.5043	2.0349	5.6874	3.500	1.660	3.560	4.250 4.250 5.200
Lead	45° 25°-56′ 10°-49′	272 272 286 296 237 297 297 297 297 297 297 297 297 297 29	28.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55 56.55	32°-29′	8 -37 47°-15′	30°-49′ 27°-51′	41°-22′ 22′ 22′ 22′	16,135,55	25°-7'	23°-21′ 35°-26′	38,49	37°-28	16°-34 20°-15'	29°-1′	32°-16' 30°-38'
Pitch Dia of Worm	2.22 1.2474 1.2496	2.0202 1.115 1.123	1.167 2.2486	2.160 1.500	3.021 1.8791	888	805	1.75	2.700	1.500	2.250	1.4415	1.775	2.043	2.002 2.142 2.2575
Lineal Pitch	. 6335 . 47656 . 2455	345 345 345	2.88.2	9878	7885	. 83028	1.10704	. 54621	.83476	.6783	9479	200	88.89	98. 1	1.0625 1.050
Normal Pitch	448 4286 2445	2724	2.04. 2.05.24	523 6326	225	. 734	838	.5234	74192	.6227	7385	.55385	. 7954	.778	88.8. 208.
Reduction	.909 5.25 17	2.8-11 7.66 6.833		14-11	3.625	2.2	4 4 5 2 2 5	24.25 26.25 26.25 26.25	3.857	14.66 8.8	883	8.65	17.5	الا	7.35
Ratio	11-10 4-21 3-51	897	주 <del>7</del> 왕왕왕	11-15 4-23	4 % 8 %	7-4-2 12-8 12-8	2-21	745	3-32 7-27	44	88	Į	4 4 8 8	# #	111 388
Centers	2.120 2.2165 2.650	2.8125	2.8125 2.8125 2.875	3.440	4.625	82. 82.	444 888	92.2	5000	5.500	500	5.511	5.511	5.696	5.975

នននន	888	*****	82888	98 98 98 98	833	288	52 52 53 53 53 53 53 53 53 53 53 53 53 53 53
1 Ton Truck 1 Ton Truck 1 Ton Truck 1 Ton Truck Motor Bus	15 Ton Truck 15 Ton Truck 15 Ton Truck 15 Ton Truck	173 1 on 1 rock 174 Ton Truck 175 Ton Truck Motor Bus 2 Ton Truck	2 Ton Truck 2 Ton Truck 2 Ton Truck 2 Ton Truck 5 Ton Truck 6 Ton Truck	2 Ion Elec. Iruck 3 Ton Truck 3 Ton Truck 3 Ton Truck	2 Ton Truck 2 Ton Truck 2 Ton Truck 2 Ton Truck	4 Ton Truck 3 and 5 Ton Truck 3 and 5 Ton Truck 3 and 5 Ton Truck	2547 3 and 5 Ton Truck 5 and 6 Ton Truck 7 Ton Truck 5 and 6 Ton Truck 5 and 6 Ton Truck
<b>ਜ਼ਜ਼ਜ਼ਜ਼</b> ਫ਼ਫ਼ਫ਼ਫ਼ਫ਼	HHHH HHH	वंस्रसंस्र वंद्रदेद्धदेव	###### ######	वंद्यंद्रवंद्यं वंद्यंद्रवंद्यं	वंष्ट्रंष्ट्रं यंष्ट्रंष्ट्रं	i 年 年 年 1	ं संसंसंसंसं संसंसंसंसं
. 1567 . 1562 . 1355 . 1528	2012	1427 1428 2189 2064	285 286 286 286 286 286 286 286 286 286 286	2337	. 1928 . 1321 . 1321	2189 2189 2253	2437 2437 2189 1771 2586
5.90625 4.9075 4.250 3.840 5.000	5.9375 6.32185 5.24972	5.3823 5.1873	2. 4. 4. 3.7.30 2. 750 3. 826 2. 826	14.4.6 16.4.6 16.2.2 16.2.2 16.2.2 16.2.2 16.2.2 16.2.2 16.2.2 16.2.2 16.2 16	4 4. 2. 4 4. 4. 2. 4 7. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2.	4.125 5.500 7.0778	4. 59375 4. 59375 4. 125 3. 339 5. 500
85.55 88.35 8.48 8.48 8.48	35°-23′ 20°-54′ 20°-49′ 20°-49′ 20°-49′	23. 25. 3118. 3118.	288 <b>25</b> 5,45,15,55,55	26°-27 31°-45′	27, 28, 13, 28, 28, 28, 28, 28, 28, 28, 28, 28, 28	82°-10° 28°-10° 28°-11°	26°-2' 26°-2' 25°-31' 21°-16' 27°-53' 20°-1'-25
2.2366 2.265 2.210 2.527 2.751	88.88 88.88 88.88 88.88	2.308 2.308 2.718 2.719	2.9135 3.2623 3.211 2.211	2.819 2.819 2.8141	2.2.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3	2.749 2.7813 2.7813	2.983 2.749 2.729 4.3308 4.258
.984375 .9815 .850 .960 1.250	1.1875 1.2643 1.3124 1.0234	.89696 .89706 1.375	1.4579 1.1875 1.275 1.275	1.3437 1.368 1.368	1.3681 1.3681 1.444	1.375 1.03125 1.375 1.41557	1.53125 1.53125 1.376 1.113 1.375 1.625
.7535 .80798 .72496 .8642 1.082	1.0242 1.12698 90753	. 7879 . 75105 1. 215 1. 10801	1.3155 1.0774 1.236 1.192 84629	1.31498 1.2059 1.1632 1.1556	1.0776 1.1831 .79113	1.241 .925 1.1636 1.0997	1.3758 1.3758 1.241 1.037 1.215 1.52676
5.16 7.22 6.73 6.55		8.59.5	8.68 6.5 8.68 8.68 8.68	17.25 17.25	8.75 17.66 10.33	11.33 11.75 8.75 6.8	10.33 10.66 15.66 14.33
67744 E <b>28</b> 23	7711 8888	7744 8888	24444 22234	7 7 8 8	442 322	¥2¥¥	222444
5.975 5.975 6.000 6.548		6.880 6.880 7.125 7.343	2.7.7.7.7. 2.6.6.6.6.6.6.6.6.6.6.6.6.6.6.6.6.6.6.	7.7.2 2.7.21 8.721 8.66	8.250 8.250 8.250 625	8.815 9.050 9.050 9.050	9.05 9.295 9.690 9.690 13.250

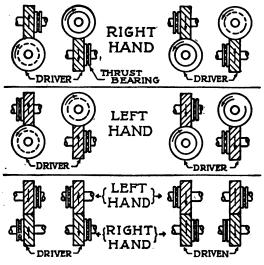
[Baush Machine Tool Co., Springfield, Mass.]

### HELICAL GEARS

Helical gears (often miscalled spiral gears) have angular teeth, and can be used when the shafts to be connected are not parallel.

The tooth dimensions are obtained from the normal pitch (determined by the cutter used) which is the same as the circular pitch of spur gears. The circumferential pitch depends on the tooth angle, and when this is 45 degs., the velocity at the pitch line is the same for both gears, but at angles other than 45 the velocity is different. With helical gears the velocity ratio depends on the tooth angles and the diameters of the pitch surfaces.

### DIRECTION OF ROTATION AND THRUST OF HELICAL GEARS



[Boston Gear Works, Norfolk Downs, Mass.]

The driving gear is the one having the greatest tooth angle, the velocity being independent of the pitch diameters. Gears of the same hand will run together on shafts set at 90 degs., and those of opposite hand on parallel shafts. Helical gears are preferable to bevel when smooth running is required—furthermore greater speed reductions can be obtained with helical.

### Formulæ

Driver	Follower
Pitch dia. = number of teeth × cir. pitch	Pitch dia. = number of teeth × cir. pitch
Circular pitch = $\frac{\pi}{\pi \times \text{pitch dia.}}$ number of teeth	Circular pitch = $\frac{\pi}{\text{number of teeth}}$
$\frac{\text{Cosine tooth pitch angle of driver}}{\text{eircular pitch}} = \frac{\text{normal circular pitch}}{\text{circular pitch}}$	Tooth angle of follower = angle between shafts — tooth angle of driver

When the axes of the gears are at right angles, the number of teeth either in the driver or the follower = pitch dia.  $\times$  normal pitch  $\times$  cosine of tooth angle.

### HERRINGBONE GEARS

Herringbone or double helical gears consist of two single helical gears reversed, that is, one right hand helix and one left hand. The teeth may meet at the center of the gear face, or the teeth may be staggered one half pitch apart as in the Wuest gear with a groove cut of one half the pitch on each side of the center of the gear face. In Wuest gears the teeth have a pitch angle of 23 degs., and are of involute form with a 20 deg. angle of obliquity.

P' = circular pitch	N = number of teeth in a gear
P = diametral pitch	W = width of face
Pitch dia. (20 teeth and over)	Pitch dia. (under 20 teeth)
N	$=\frac{.95 \text{ N} + 1}{P}$
= <u>P</u>	= <u>P</u>
$Addendum = \frac{.8}{P}$	$Dedendum = \frac{1}{P}$
Full depth $=\frac{1.8}{P}$	Working depth = $\frac{1.6}{P}$

Standard face width for gears with pinions of not less than 25 teeth is equal to 6 P', and for face widths for high ratio gears with small pinions 6 P' to 12 P'.

### SECTION IV

### PIPE, TUBES AND FITTINGS

TRADE CUSTOMS—STANDARD WROUGHT IRON PIPE—EXTRA STRONG
WROUGHT IRON PIPE—DOUBLE EXTRA STRONG WROUGHT IRON
PIPE—COUPLINGS—NIPPLES—BOILER TUBES—STEEL
TUBES—BRASS AND COPPER TUBES—PIPE BENDS
—FLANGES—FITTINGS—VALVES—COCKS—
EXPANSION JOINTS

Trade Customs Pertaining to Wrought Iron and Steel Pipe for Steam, Water and Gas.

Specify whether wrought iron or steel pipe is required.

Pipe is designated by its nominal inside diameter from  $\frac{1}{8}$  to 15 ins.; above 15 ins. by the outside diameter, the thickness being specified.

The outside diameter of pipe heavier than standard has the same diameter as standard, the extra thickness being on the inside.

The inside diameter of casings is always given.

The sizes of boiler tubes are indicated by their outside diameter. Pipe is shipped in random lengths 18 to 21 ft. with threads and couplings, except extra and double extra strong which are shipped with plain ends. There is an extra charge for pipe cut to specified lengths—couplings not being furnished unless specified—pipe so cut is always measured to include the couplings.

Standard pipe cut to given lengths is always furnished with threaded ends. Extra strong and double extra strong have plain ends.

Pipe is furnished either butt or lap welded. Butt welded pipe may be obtained up to 3 ins. diameter, and lap welded from 1½ in. up.

Pipe threads—see chapter on Threads.

In cutting pipe to order all dimensions should be given from center to center of valves and fittings.

STANDARD WROUGHT IRON AND STEEL PIPE

	of Threads per Inch of Screw	1	2444 4444
Nominal Weight per Foot	Thread- ed and Coupled		2.25 2.25 2.25 2.25 2.25 2.25 2.25 2.25
Nomin	Plain Ends		244 - 24
Length	Con- taining One Cubic	Feet	2533.775 744.360 745.360 745.360 86.713.960 106.718 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375 11.375
Length of Pipe per Square Foot of	Exter Internal	Feet	14.199 10.4638 17.174 17.174 17.174 18.355 18.355 18.375 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.376 19.37
Length per S Foc	Exter- nal Surface	Feet	9 4 4 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
reas	Metal	Sq. Ins.	. 072 . 157 . 157 . 250 . 250
Transverse Areas	Inter- nal	Sq. Ins.	. 067 . 194 . 304 . 304 . 304 . 304 . 305 . 305
Tra	Exter- nal	Sq. Ins.	1288 1288 1288 1288 1288 1288 1288 1288
Circumference	Inter- nal	Inches	28.289 2.289 2.289 2.289 2.289 2.289 2.289 2.289 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280 2.280
Circun	Exter- nal	Inches	1.272 1.666 2.632 3.299 3.299 3.299 5.215 10.996 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27.096 27
	Nominal Thick- ness	Inches	0.068 0.088 0.088 0.1133 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.1145 0.114
Diameter	Approx- imate Inter- nal	Inches	286 682 682 682 682 682 682 682 682 682
Diaz	Exter- nal	Inches	.405 .540 .540 .540 .540 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080 .1080
	Sign	Inches	****** *** * * * * ***

EXTRA STRONG WROUGHT IRON AND STEEL PIPE

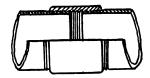
	<i>;</i>	
		28. 1. 1. 1. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2.
Length of	Pipe Containing One Cubic Foot	3966 392 2010 290 1024 689 1024 689 1102 016 333 016 200 1193 112 256 21 801 116 202 116 202 116 202 1174 4 1177 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
	Internal Surface Feet	17.766 6.966 6.966 6.966 6.966 1.966 1.966 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136 1.136
Length of Pipe per Square Foot of	External Surface Feet	2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.
68.6	Metal Sq. Inches	093 157 227 227 227 239 639 639 147 3 016 8 407 6 112 8 405 111 1119 8 405 112 113 8 405 114 117 117 117 117 117 117 117 117 117
Transverse Areas	External Internal Metal Sq. Inches Sq. Inches	. 036 . 072 . 234 . 238 . 238
Tra	External Sq. Inches	22.22 22.23 22.23 22.23 22.23 22.23 23.23 24.23 25.23 26.43 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23 27.23
Circumference	External Internal Inches	. 675 1.329 1.715 2.331 2.331 3.007 4.015 6.092 1.12,020 11.202 11.202 11.202 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 11.203 1
Circum		1.22 2.21 2.22 2.22 2.23 2.23 2.23 2.23
	Nominal Thickness Inches	900 1119 1119 1119 1119 1119 1119 1119
ter	Approximate Internal Diameter Inches	215 2302 2302 2423 2423 2423 2500 11.939 2500 2500 2500 2500 2600 2600 2600 2600
Diameter	Exter- nal Inches	406 406 406 406 406 406 406 406
	Nomi- nal- Inter- nal Inches	****** ** * * * * *

DOUBLE EXTRA STRONG WROUGHT IRON AND STEEL PIPE

Nomi-	, H	Pounds	1. 714 2. 440 3. 659 5. 214 6. 408 9. 028 9. 028 13. 695 118. 683 22. 581 22. 581 23. 530 38. 533 53. 150 63. 079 72. 424
1	Pipe Contains Concording Concording Foot	Feet	2887 164 973 404 210 998 228 379 151 526 81 162 58 465 34 659 18 454 14 306 11 107 7 107 7 6 312 3 379
Length of Pipe per Square Foot of	Internal Surface	Feet	15.157 8.801 6.376 4.263 2.541 2.541 2.541 1.660 1.1400 1.211 1.211 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.210 1.21
Length o	External Surface	Feet	4 547 3 637 2 994 2 994 2 904 2 301 1 328 1 1 994 8 548 6 686 5 76 5 76 5 76 5 76 5 76 5 76
9.B.8	Metal	Sq. Inches	. 504 1.076 1.076 1.534 1.885 2.656 4.068 6.721 8.101 11.340 11.340 11.340 11.340 11.340
Transverse Areas	Internal	Sq. Inches Sq. Inches	.050 .148 .282 .630 .950 .1774 2.464 4.155 5.845 7.803 10.066 11.966 11.966 12.966 13.835 27.109
Tr	External	Sq. Inches	. 554 
Circumference	Internal	Inches	792 1.363 1.882 2.815 3.456 4.722 4.722 6.564 7.226 8.570 11.247 12.764 15.384 11.384 11.384 11.384 11.384
Circum	External Internal	Inches	2. 639 3. 299 4. 131 5. 215 5. 969 7. 461 10. 996 12. 566 14. 137 15. 708 17. 477 20. 813 23. 955 27. 096
	Nominal Thickness Inches		294 308 308 382 382 400 552 600 674 7710 775 864 875
ær	Approxi- mate Internal Diameter	Inches	252 434 634 686 11.100 1.771 2.300 2.300 2.300 4.063 4.897 6.877
Diameter	Exter- nal	Inches	
	Nomi- nal Inter- nal	Inches	7,4 4, 6 4 4 70 70 70 70 70 70 70 70 70 70 70 70 70

Standard, extra strong and double extra strong pipe for a given size have the same outside diameters. strength of extra strong and double extra strong is secured by decreasing the inside diameter.

#### PIPE COUPLINGS FOR STANDARD WROUGHT IRON PIPE



Size of Pipe	Dia. of Coupling	Length	Weight lbs.	Size of Pipe	Dia. of Coupling	Length	Weight lbs.
1/8 1/4 3/8 1/2 3/4 1 1 1/4 1 1/2 2 2/2 3	.562 .685 .848 1.024 1.281 1.576 1.950 2.218 2.760 3.276 3.948	7/8 1 11/8 13/8 15/8 17/8 22/5/8 22/5/8 23/5/8 31/8	.029 .043 .070 .116 .209 .343 .535 .743 1.208 1.720 2.498	4½ 5 6 7 8 9 10 11 12 13 14	5.591 6.296 7.358 8.358 9.358 10.358 11.721 12.721 13.958 15.208 16.446	35/8 41/8 41/8 41/8 45/8 51/8 61/8 61/8	5.241 8.091 9.554 10.932 13.908 17.236 29.877 32.556 43.098 47.152 59.493
3½ 4	4.591 5.091	35/8 35/8	4.241 4.741	15	17.446	61/8	63.29

For threads per inch see table of Standard Wrought Iron Pipe. [National Tube Co., Pittsburgh, Pa.]

## NIPPLES FOR STANDARD WROUGHT IRON PIPE (Right and left hand threads)



Short and long nipples have an unthreaded portion or shoulder as shown in figure. Close nipples have no shoulder. See table page 167.

## NIPPLES (Continued)

Size, Inches			Length	n, Inches		
Inches	*Close	*Short	1	Lo	ong	
1 1 1 1 2 2 1 2 2 1 2 3 3 1 2 4 1 2 5 6 7 8 9 10 12	34 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 2 2 1 1 2 2 2 1 1 2 2 2 2 1 2 2 2 3 3 4 4 4 4 4 1 5 5 5 5 5 5 6	2 2 2 2 2 2 2 2 2 2 2 3 3 3 3 4 1,2 4 4 1,2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	21/2/2 21/2/2 21/2/2 3 1/2/2 3 3 1/2/2 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	3\\\2\\3\\2\\3\\2\\4\\4\\2\\4\\2\\5\\5\\6\\6\\6\\6\\6\\6\\6\\6\\6\\6\\6\

<sup>\*</sup> These lengths conform to the Manufacturers' Standard.

#### STANDARD BOILER TUBES

			٥	IAND	AKD	DOILE	K IUI	DEO			
Dia	meter	Thick-	auge	Circum	ference	Tran	sverse A	rea.	tube	th of per t. of	Nom-
Ex- ter- nal	In- ternal	Nominal T	Nearest B. W. G	Ex- ternal	In- ternal	Ex- ternal	In- ternal	Metal	Ex- ternal Sur- face	In- ternal Sur- face	Weight Per Foot
Ins.	Ins.	Ins.	No.	Ins.	Ins.	Sq. ins.	Sq. ins.	Sq.	Feet	Feet	Lbs.
134 214 214 225 314 314 314 56 78 9	1.560 1.810 2.060 2.282 2.532 2.782 3.010 3.510 3.510 3.510 6.670 7.670 8.640 9.594	.095 .095 .109 .109 .120 .120 .124 .134 .134 .165 .165 .180	13 13 13 12 12 12 12 11 11 11 10 9 8 8 8 7	11.781 12.566 14.137 15.708 18.850 21.991 25.133	5.686 6.472 7.169 7.955 8.740 9.456 10.242 11.027 11.724 13.295 14.778 17.813 20.954 24.096 27.143	3.976 4.909 5.940 7.069 8.296 9.621 11.045 12.566 15.904 19.635 28.274 38.485 50.265 63.617	2.573 3.333 4.090 5.036 6.079 7.116 8.347 9.677 10.939 14.066 17.379 25.249 34.942 46.204 58.629	.569 .643 .819 .904 .990 1.180 1.274 1.368 1.627 1.838 2.256 3.025 3.025 3.434 4.061 4.988	1.091 1.018 .954 .848 .763 .636 .545 .477	2.110 1.854 1.673 1.508 1.373 1.269 1.171 1.088 1.023 902 .812 .673 .572 .498	1.932 2.186 2.783 3.074 3.365 4.011 4.331 4.652 5.532 6.248 7.669
11 12 13	10,560 11,542 12,524	.220	5	34.558	33,175	95.033	87.582 104.629	7.451	.347	.361	25.329 28.788 32.439

Lap welded boiler tubes, as manufactured by the National Tube Co., are of open hearth steel. Sizes including 4 in. dia. are tested to 750 lbs. per sq. in. and above this size to 500.

#### STEEL TUBES

Cold drawn Shelby seamless steel tubes can be obtained from  $\frac{3}{16}$  in, to 9 ins. O. D.

Hot rolled can be rolled from 2 to 9 ins. They cannot be rolled smaller than 2 ins. O. D. nor with a wall thickness less than 3% of the outside diameter, provided further that the wall is not thinner than 11 gauge. Hot rolled tubes are desirable when it is necessary to machine the outside or inside to finished dimensions.

Comparison of Standard Wrought Iron Pipe and Shelby Seamless Steel Tubing

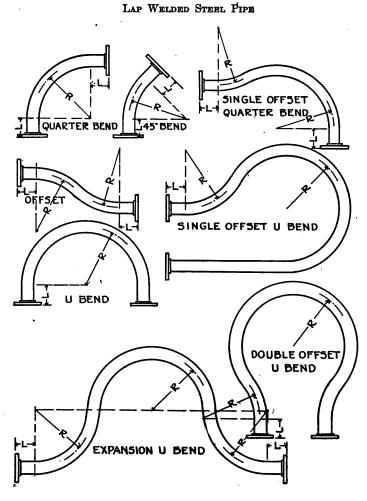
Inside	inal Size Diameter t Iron Pipe	Nominal Weight	Nominal Thickness	of Se	actional Size amless Tubing
Size	O. D.	per Foot	of Wall	O. <b>D</b> .	Thickness B. W. G.
1/6	.405	.244	.068	13/32	16 Ga.
1%	.540	.424	.088	1/32	14 Ga.
3/8	.675	. 567	.091	217	13 Ga.
1/8 1/4 3/8 1/2 3/4	.840	.850	.109	21/32 27/32	12 Ga.
$\frac{3}{4}$	1.050	1.130	.113	11/16	12 Ga.
1	1.315	1.678	.133	15/16	10 Ga.
$1\frac{1}{4}$	1.660	2.272	.140	15/8	9 Ga.
11/2	1.900	2.717	.145	1 1 1/8	9 Ga.
$2^{1/2}$ $2^{1/2}$ $3$ $3^{1/2}$	2.375	3.652	.154	23/8	5€2 6 Ga.
$2\frac{1}{2}$	2.875	5.793	.203	$\frac{278}{312}$	6 Ga.
3	3.500	7.575	.216		4 Ga.
31/2	4.000	9.109	.226	4	4 Ga.
4	4.500	10.790	.237	4½ 5	4 Ga.
$\frac{4}{5}$ /2	5.000 5.563	12.538 14.617	.247	5 5 6	1 /4
O R	6.625	18.974	.280	55/8 65/8	32
7	7.625	23.544	.301	75/8	732 5/
5 6 7 8 9	8.625	28.554	.322	85%	114
9	9.625	33.907	.342	95%	112
10	10.750	40.483	.365	1034	3/32
îĭ	11.750	45.557	.375	1134	3%
$\tilde{1}\tilde{2}$	12.750	49.562	.375	1234	1/4 9/32 9/32 5/16 11/52 11/52 8/8 8/8

TENSILE AND PHYSICAL PROPERTIES OF SHELBY COLD DRAWN STEEL TUBES

			M	Minima			
Grade	Treatment	Yield Point	Tensile Strength	Eloi	Elonga- tion	Reduc-	Appearance and Condition
19910			Lbs. per Sq. In.	%2*	.8%	Area %	
.17 Carbon	Temper "T" Finish Anneal	45000	28000	17	10	30	Surface dull and fairly scale free. Unless otherwise speci- fied, material is always furnished to this temper.
.17 Carbon	Temper "U" Special Anneal	38000	23000	33	15	35	Surface dull and very slightly scaled. Material of this temper will stand a moderate amount of cold forming.
.17 Carbon	Temper "V" Medium Anneal	35000	20000	45	22	45	forming and is in excellent shape for machining. However, the tool should have a 30 deg, top rake, as the chips
.17 Carbon	Unannealed	22000	63000	10	es	18	are long and tough. Surface bright and scale free, Material of maximum strength with but slight ducility.
Boiler Tube	Temper "W"	27000	47000	25	27	20	Surface slightly scaled. This temper is suitable for all purposes: it stands cold forming and manipulation.
Boiler Tube	Temper "X"	28000	20000	22	88	52	Surface considerably scaled. Especially suitable for stay- bolts.
.35 Carbon	Temper "T" Finish Anneal	65000	80000	18	91	8	Surface dull and fairly scale free. These otherwise speci- fod material is always furnished to this temper. It is used for mechanical purposes on parts requiring medium high for mechanical purposes.
35 Carbon	Temper "U" Medium Anneal	48000	65000	32	18	33	constant properties our nine auctions.  Surface dull and slightly scaled. This temper is suitable for purposes requiring medium tensile strength and ductifive resisting power. This temper will stand research to cold forming.
.35 Carbon	Unannealed	20000	85000	01	•	12	Surface bright and scale free. This material has maximum strength but hardly any durelity, and should not be used where subjected to shock. Material, provided it is not subjected to cold working or manipulation, and is to be heaved above 500°C during subsequent manufacture, about 6 transhed to this temper.

[Tubes made by the Shelby process are manufactured by National Tube Co., Pittsburgh, Pa.]

PIPE BENDS



' Minimum radius of pipe bend, 5 times the outside diameter of the pipe. Bends with shorter radii have practically no expansion value as they buckle in bending. All radii taken to center line of pipe.

Size of pipe, ins.	21/2	3	31/2	4	41	5	6	7	8	9	10	12	14	15	16	18	20	22	24
R = minimum advisable ra- dius, ins	121	15	17}	20	221	25	30	35	40	45	50	60	70	75	80	108	120	132	144
I. = minimum tangent length ins	4	4	5	5	6	6	7	8	9	11	12	14	16	16	18	18	18	18	18

#### COPPER AND STEEL PIPE

Minimum radius should be at least 5 times the outside diameter of the pipe.

# THICKNESS OF STEEL PIPE FOR BENDS Up to 125 Pounds Working Pressure

Radius	Pipe Size	Pipe
4 to 5 diameters	. 7 inches and smaller	.Extra strong
	8 inches and larger	.1/2 inch thick
Over 5 diameters	7 inches and larger	. Full weight
	8 inches	
	10 inches	.40.48 pounds per foot
	12 inches	
	14 inches to 16 inches, inclusive	
	18 inches to 22 inches, inclusive	
•	24 inches to 30 inches, inclusive	. 7 inch thick
	to 250 Pounds Working I	
4 to 5 and 6 diameters	. 7 inches and smaller	
	8 inches and larger	
Over 6 diameters	7 inches and smaller	
	8 inches	
	10 inches	
	12 inches	
	14 inches to 16 inches, inclusive	
	18 inches to 22 inches, inclusive	e. 1/16 inch thick
	24 inches to 30 inches, inclusive	. ½ inch thick
250 Pounds	s to 350 Pounds Working I	Pressure
4 diameters and over	7 inches and smaller	.Extra strong

8 inches and larger ...... 1/2 inch thick

**FLANGES** 

STANDARD AND LOW PRESSURE FLANGES (For pressures up to 125 lbs.)



Size	Diameter of Flanges	Thickness of Flanges	Bolt Circle	Number of Bolts	Size of Bolts	Length of Bolts
Inches	Inches	Inches	Inches		Inches	Inches
1	4	7/16	3	4	7 1 2 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	11/2
$\frac{114}{112}$	41/2	1/2	33/8 37/8	4	7/16	11/2
$1\frac{1}{2}$	5 6	16		4	1/2	13/4
2 <sup>1</sup> / <sub>2</sub> 2 <sup>1</sup> / <sub>2</sub> 3 3 <sup>1</sup> / <sub>2</sub>	6	5.78 11.16 3.4 13.16	43/4 51/2 6	4	5/8	2
$2\frac{1}{2}$	7	11/16	$5\frac{1}{2}$	4	5∕8	21/4
3	71/2	34	6	4	<b>5</b> ∕8	21/4
$3\frac{1}{2}$	8½	13/16	7	4	5∕8	21/2
4	9	1 10/-	$7\frac{1}{2}$	8	5/8	23/4
4 1/2 5 6 7 8 9	91/4	1 20/00	73/4	4 4 4 8 8 8 8 8 8 8 12	3/4	23/4
5	10	15 16	81/2	8	3/4	23/4 3 31/4 31/4 31/2
6	11	1	91/2	8	3/4	3
7	$12\frac{1}{2}$	1116	1034	8	3/4	3
8	$13\frac{1}{2}$	11/8	$11\frac{3}{4}$	8	3/4	31/4
	15	11/8	131/4	12	3/4	31/4
10	16	13/16	141/4	12	7/8 7/8	31/2
12	19	11/4	17	12	1/8	31/2
14	21	13/8	183/4	12	1	4
15	221/4	13/8	20	16	1	4
16	$23\frac{1}{2}$	17/16	$21\frac{1}{4}$ $22\frac{3}{4}$	16	1	4
18	25	1916	223/4	16	11/8	41/2
20	271/2	11116	25	20,	11/8	43/4
22	291/2	113/16	271/4	20	11/4	5 5½
24	32	172	291/2	20	11/4	51/4
26	341/4	2	3134	24	11/4	51/2
28	361/2	21/16	34	28	11/4	51/2
30	38¾	21/8	36	28	13/8	534
32	4134	21/4	381/2	28	11/2	61/4
34	4334	25/6	401/2	32	11/2	61/2
36	46	23/8	4234	32 32	11/2	$6\frac{1}{2}$
<b>3</b> 8	483/4	23/8	451/4	32	15/8	634
40	5034	21/2	4714	36	15%	7

American standard in effect January 1, 1915. Flanges can be obtained in cast iron, malleable iron and cast steel. The drilling

templates are in multiples of four, so that fittings may be made to face in any quarter and bolt holes straddle the center line. Bolt holes are drilled  $\frac{1}{8}$  inch larger than nominal diameter of bolts.

TEMPLATES FOR DRILLING

Extra Heavy and Medium Flanged Valves and Extra Heavy
Flanged Fittings—American Standard—Effective January 1, 1915.

Size in inches	Diameter in inches of Flanges	Thickness of Flanges in inches	Bolt Circle in inches	Number of Bolts	Sise in inches of Bolts	Length in inches of Bolts	Length in inches of Studs with 2 Nuts
1	41/2	11/16	31/4	4	1/2	2	
$\frac{1\frac{1}{4}}{1\frac{1}{2}}$	5 6	3/4 13/16 7/8	3 1/4 3 3/4	4	1/2	21/4	
11/2	6	13/16	41/2	4	5/8	2½ 2½ 3 3¼	
$2^{1}/2$ $2^{1}/2$ $3^{1}/2$	61/2	1/8	5	4	5/8	21/2	
$2\frac{1}{2}$	71/2	1	51/8	4 8 8 8 8 12 12 12 12 16	8/4	3	
3	81/4	1 1/8 13/16	65/8	8	<b>8</b> ∕₄	31/4	• • • •
31/2	9	13/16	71/4	8	3/4	1 31/4	
4	10	11/4	71/8	8	8/4/4/4/3/4/8/8 3/4/4/4/8/8	31/2 31/2 33/4 33/4	• • • •
4½ 5 6 7 8	101/2	16/16	81/2	8	34	3½ 3¾	• • • •
5	11	13/8 17/16	914	8	<b>1</b> %	33/4	
6	121/2	17/6	105/8 117/8	12	74	33/4	• • • •
7	14	$\frac{112}{158}$	11 /8	12	<b>48</b>	4	• • • •
ð.	15	1%	13 14	12	1/8	41/4 43/4	• • • •
10	1614	184 178	151/	12	1	5	••••
12	$17\frac{1}{2}$ $20\frac{1}{2}$	2 2	15¼ 17¾	16	11/8	5½	••••
14	23	21/8	2014	20	116	51/2	• • • •
15	2416	02 7	$\frac{2074}{21\frac{1}{2}}$	20	11/	53/4	• • • •
16	$24\frac{1}{2}$ $25\frac{1}{2}$	2016	$22\frac{1}{2}$	20	114	6	• • • •
18	28	236	2434	24	11/	61/	••••
20	301/2	216	27	24	13%	$\frac{6\frac{1}{4}}{6\frac{1}{2}}$	• • • •
22	33 2	25%	$29\frac{1}{4}$	24	11%	7	••••
24	36	23/4	32	24	15%		91/2
26	$38\frac{1}{4}$ $40\frac{3}{4}$	213/16	341/2	28	15/8	$7\frac{1}{2}$ $7\frac{3}{4}$	10
28	4034	215/16	37	28	15/8	8	10
26 28 30 32	43	3	391/4	28 28 28 28 28 28 32	134	8 81/4 81/2	101/2
32	451/4 471/2	31/8	411/6	28	17/8	81/2	11
34	471/2	31/4	431/2	28	17/8	9	111/2
36	50	33/8	46	32	17/8	91/4	111/2
38	$52\frac{1}{4}$ $54\frac{1}{2}$	37/m	48	32	17/8	91/4	111/6
40 l	541/2	39/16	501/4	36	17/8	91/2	12 1 12
42	57	311/4	$52\frac{3}{4}$	36	17/8	934	12
44 .	591/4	33/4	55	36	2	10	121/6
46	611/2	33/4 37/8	571/4	40	2 2	101/4	13 13 13
48	65	4	603/4	40	2	101/2	13

Extra Heavy Companion Flanges (For pressures up to 250 lbs.)



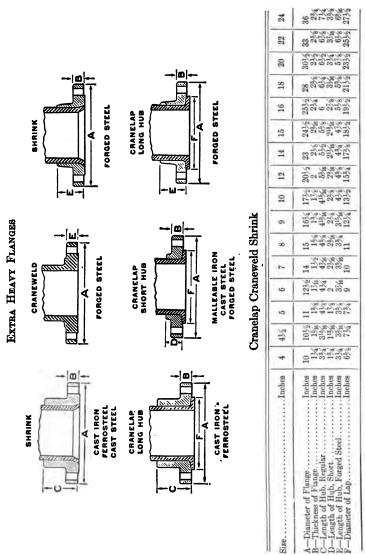
Cast iron, malleable iron, ferrosteel, cast steel, forged steel

SiseInches 1 11% 11%	-	17.	11/2	2	27.2	8	37%	4	2 23/2 3 33/5 4 13/2 5 6 7 8	10	9	7	8	-	0	10 12 14	14 15	35	16	18	20 23	2 24
A—Diameter of Flange . Inches B—Thickness of Flange . Inches C—Length of HubInches		2,4,7	435 5 6 635 735 136 136 138 13 1 138 134 138 136	25/2/8%	2-3	%%%	822	577	10 10½ 11 12½ 14 1½ 1½ 1½ 1½ 1½ 1 1½ 1½ 1½ 1½ 2	13%	27.2	72.2	15 15% 15% 29%	16% 17 2% 2 2% 2	<u> </u>	1715 2015 23 176 2 236 178 2 236 1 236 296 295	23 23/2 23/2 21/2 21/2 21/2	722	25.52 27.72 27.83 27.83 34.33	ı ∖∞o√a I	3014 33 214 256 314 376	32,38

For drilling see page 173.

These flanges have a 1/6 in. raised face, the face having sufficient height to hold a copper gasket in place. Sizes in effect Jan. 1, 1915, recommended by American Society of Mechanical Engineers.

Other types of extra heavy flanges are shown on page 175.



For drilling see page 173.

#### **BRASS AND COPPER TUBES**

When ordering seamless brass and copper tubes state whether inside or outside diameter is required, otherwise outside diameter is shipped. In designating thickness, Stubs' (Birmingham Wire Gauge) or Brown and Sharpe is given. Tubes can be obtained with hard or soft temper, the latter should be specified if they are to be bent or flanged. They can be obtained in a variety of dimensions, the following table gives common sizes.

SEAMLESS BRASS\* TUBES

Outside dia., ins.	Stubs'	Weight per	Outside	Stubs'	Weight per
	gau <del>ge e</del> xact	foot, lbs.	dia., ins.	gauge—exact	foot, lbs.
1/8	21	.034	15/8	14	1.48
3/16	21	.057	18/4	13	1.82
1/4	20	.087	2	13	2.09
5 16	20	.112	$egin{array}{c} 2 \\ 2 \frac{1}{4} \\ 2 \frac{1}{4} \end{array}$	16	1.45
8 8	19	.161		12	2.69
7 16	19	.192		16	1.64
5 (6) 8 (6) 2 (6) 8 (6) 8 (6) 8 (7) 16 (8) 8 (7) 8 (7) 8 (7) 8	18	.255	2½	12	3.01
	18	.290	2½	16	1.83
	18	.326	2¾	12	3.32
	17	.463	3	11	3.99
1 1½	17 16 16	.547 .700 .790	3 3 3 <sup>1</sup> ⁄ <sub>2</sub>	16 10 10	2.20 4.82 5.21
$1\frac{1}{4}$ $1\frac{3}{8}$ $1\frac{1}{2}$	15 14 14	.98) 1.24 1.36	4	10	5.98

<sup>\*</sup>For weight of copper tubes multiply by 1.051.

Seamless brass and copper tubes are also rolled in standard iron pipe sizes  $\frac{1}{2}$ ,  $\frac{1}{2}$ ,  $\frac{3}{2}$ ,  $\frac{3}{2}$ ,  $\frac{3}{2}$ ,  $\frac{3}{2}$ ,  $\frac{3}{2}$ ,  $\frac{3}{2}$ ,  $\frac{4}{2}$ ,  $\frac{4}{2}$ ,  $\frac{5}{2}$ ,  $\frac{6}{2}$ ,  $\frac{7}{2}$ ,  $\frac{7}{2}$ ,  $\frac{3}{2}$ ,

#### FITTINGS

Standard fittings are guaranteed to 125 lbs. working pressure and extra heavy to 250 lbs.

Standard fittings and flanges are plain faced, while extra heavy inside of the bolt holes have a raised surface 1/16" high.

In describing fittings the run is first named, then the outlet.

LENGTH OF THREAD ON PIPE THAT IS SCREWED INTO VALVES OR FITTINGS TO MAKE A TIGHT JOINT

Dia. of pipe	Length of thread on pipe	Dia. of pipe	Length of thread on pipe
1/8 1/4 3/8 1/2 3/4 1 1/4 11/2 2 2/2 3	8/4/0/08/08/19/19/19/09/08/19/19/09/09/09/09/09/09/09/09/09/09/09/09/09	3½ 4 4½ 5 6 7 8 9 10 12	1 1 1 1 1 1 1 1/4 1/4 1/4 1/4

# EXTRA HEAVY CAST IRON SCREW FITTINGS (For steam pressures up to 250 lbs.)

(See figures, page 178)

15/2 15/2 25/16	13/8 23/4 7/8	1 119/2 33/16	114 115/8 37/8 13/8	11/2 21/4 41/8 11/4	2 2½ 5 1½	2½ 3 6 1¾
1 <sup>21</sup> / <sub>16</sub> <sup>7</sup> / <sub>16</sub> <sup>9</sup> / <sub>16</sub>	129.65 1/2 5/8	25/16	234 11/16 13/16	31/16	334	4%6 1 11%
2 311/16	31/2	4 415/2	41/2	5 51/42	6 513/16	8 73/6
73/8 21/4	81/16 27/16	211/16	27/8	107/6 31/8	35/16	14 9 8 316 %
5% 114	6 15/6	613/6	73/6 19/6 111/6	715/6 111/6	95/16 13/4 17/8	11% 178 11%
	25/6 3/4 121/2 7/6 9/6 2 311/2 73/8 21/4	121/4 129/4 7/6 1/4 9/6 5/8 2 2 31/4 41/4 73/6 81/6 21/4 27/6	131/4 139/4 25/6 1/6 1/2 1/8 1/6 1/2 1/8 1/4 2 311/4 41/4 41/4 311/4 41/4 41/4 7 3/6 81/4 21/4 2 21/4 21/4	111/4 119/4 25/6 28/4 28/4 1/4 1/4 11/4 11/4 11/4 11/4 11/4 11/	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$

## STANDARD CAST IRON SCREW FITTINGS (For steam pressures up to 125 lbs.)











Sise Inches A-Center to Face Inches AA-Face to Face Inches B-Center to Face Inches C-Center to Face Inches D-Face to Face Inches D-Face to Face Inches E-O.D. of Bead Inches F-Width of Bead Inches G-Thread Length Inches	1 1/2 7/16 1 1/4 3/8	3/8 7/8 13/4 9/16 17/16 21/16 11/8 7/16	11/6 21/8 11/8 17/8 17/8 17/8 17/8 17/8	25/8 13/16 21/16 21/16 21/16 23/4 13/4 18/16	1 11/2 3 15/6 21/2 31/4 21/6 5/8	114 118 is 358 11 is 384 212 9 is	11/2 2 4 11/6 31/4 43/4 23/4 5/8 11/6	2 2 3 8 4 3 4 1 3 8 4 5 1 2 3 3 8 1 1 16 7 8	21/2 27/8 53/4 15/8 618/6 41/8 18/8	3 3 5 1 6 5 1 7 5 5 1 1 5 5 1 1 1 1 1 1 1 1 1 1 1
Size	31/2 311/6 78/8 21/6 63/8 88/4 51/4 1	4 4 8 214 718 934 6 116 118	41/4 47/8 87/8 77/8 10/4 11/4	5 411/6 93/8 29/6 81/2 11/6 11/6 11/4	6 55% 105% 211% 915% 133% 11% 13%	7 61/6 121/8 31/8 111/4 145/8 93/4 11/2	8 613 16 1358 39 6 12 16 16 13 16 1078 138 158	31/8 141/2 19	45/6 16 20%	12 9% 1918 478  1556 134 178

The Center to Face and Face to Face dimensions of Reducing Tees and Crosses are determined as follows: For AA-Face to Face, add to the outside diameter E of outlet bead, twice the width F of the run bead.

For A-Center to Face, add to the width F of outlet bead, one-half the diameter E of the run-bead.



$$X = A - G$$

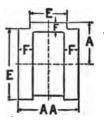
$$Y = B - G$$

$$Z = C - G$$
For Example AA of a 2 x %

equals 
$$1\frac{8}{4} + \frac{11}{16} + \frac{11}{16} = 3\frac{1}{8}$$
 Inches.

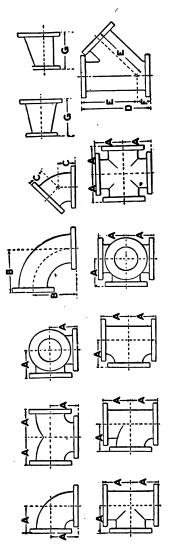
$$A = \frac{1}{16} + 1^{11} \frac{1}{16} = \frac{2}{16}$$
 Inches.

[Walworth Mfg. Co., Boston, Mass.]



The sizes of fittings are determined by the largest opening whether in run or branch.

STANDARD AND LOW PRESSURE FLANGED FITTINGS



$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
114 115 2 2 2 2 2 1 1 1 1 2 1 4 1 5 6 7 7 8 9 9 1 0 1 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
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Standard and Low Pressure Flanged Fittings are furnished plain faced unless otherwise ordered. All reducing fittings 1 to 16" inc. have the same face to face dimensions as straight size fittings.

EXTRA HEAVY FLANGED FITTINGS
Cast Iron, Ferrosteel and Cast Steel

(See figures, page 179)

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All extra heavy flanges have a 1/6 inch raised face inside of bolt holes. This raised face is included in face to face, center to face and thickness of flange dimensions.

#### VALVES

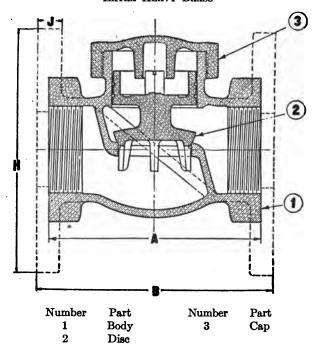
Check valves are only for use when the flow of steam or water is always in one direction. Globe and angle valves should be installed to close against pressure, for if installed the opposite way they could not be opened if the valve disc became detached from the stem. Gate valves should always have their spindles vertical.

Standard valves are for pressures up to 125 lbs., extra heavy for pressures up to 250.

Valves under 6 ins. have screwed ends, over this size the valves are generally flanged.

The following data on check, globe, angle and gate valves was supplied by Crane Co., Chicago, Ill.

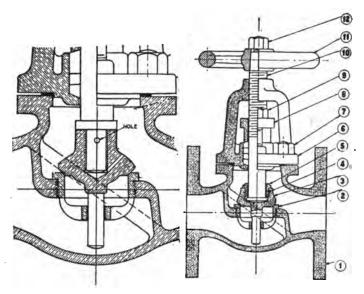
HORIZONTAL PATTERN, CUSHIONED—CHECK VALVE
EXTRA HEAVY BRASS



DIMENSIONS

Size Ins.	A	В	н	J
3/4	2 <sup>15</sup> 16	334	4	7/16
1	3 <sup>1</sup> / <sub>2</sub>	438	4½	1/2
11/4	4 <sup>1</sup> / <sub>16</sub>	4136	5	17/22
11/2	4 <sup>5</sup> / <sub>8</sub>	512	6	9/16
2	5 <sup>3</sup> / <sub>4</sub>	612	6½	5/8

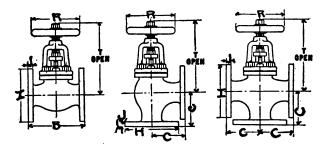
GLOBE, ANGLE AND CROSS VALVES—STOP AND SCREW DOWN CHECK



- 1 Body
- 2 Seat
- 3 Disc (stop)
- 4 Cotter pin
- 5 Disc nut
- 6 Bonnet
- 7 Bonnet studs
- . Donner sou
- 8 Gland
- 9 Gland studs
- 10 Stem stop
- 11 Wheel
- 12 Wheel nut

(Continued on page 184)

## STOP AND SCREW DOWN CHECK VALVES-Continued



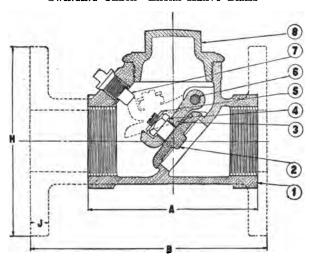
#### DIMENSIONS—STANDARD IRON BODY

Size Ins.	В	С	н	J	R	T
2 2)/2 3 3/2 4 4/2 5 6 7 8 10	8 8½ 9½ 10½ 11½ 12 13 14 16 17 20 24	4 4 <sup>1</sup> / <sub>4</sub> 4 <sup>3</sup> / <sub>4</sub> 5 <sup>3</sup> / <sub>4</sub> 5 <sup>3</sup> / <sub>4</sub> 6 6 <sup>1</sup> / <sub>2</sub> 7 8 8 <sup>1</sup> / <sub>2</sub> 10 12	6 7 71/2 81/2 9 91/4 10 11 121/2 131/2 16	5 8 11, 16 3, 4 13, 16 15, 16 15, 16 11, 18 13, 16 11, 14	61/2 61/2 71/2 71/2 9 9 10 12 14 16 18 20	11½8 11¾4 13½8 13½8 15¾2 17¼ 19 21¼4 23¾4 27¾4 32½

## DIMENSIONS-EXTRA HEAVY BRASS

Size Ins.	В	C	н	J	R	Т
1½ 2 2½ 3 3½ 4 4½ 5	63/8 73/8 83/4 10 107/8 111/2 121/4 13	334 41/8 45/8 51/4 53/4 61/8 63/8 73/4	6 6½ 7½ 8¼ 9 10 10½ 11 12½	916 58 11,66 34 13,16 7,8 15,16	5½ 6½ 7½ 9 9 10 10 12 14	9 10½ 11½ 12½ 12½ 14½ 15¾ 16½ 18

SWINGING CHECK—EXTRA HEAVY BRASS



Number	Part	Number	Part
1	Body	•5	Cotter pin
2	Disc	6	Hinge pin
3	Hinge	· 7	Stop plug
4	Disc nut	8	Cap

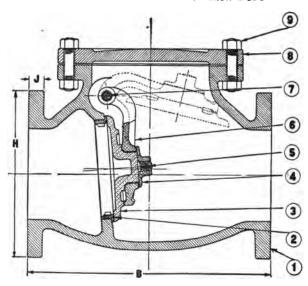
#### DIMENSIONS

Size Ins.	A	В	Н	Ј
$1 \\ 1\frac{1}{4} \\ 1\frac{1}{2} \\ 2$	3 <sup>5</sup> / <sub>8</sub> 4 <sup>1</sup> / <sub>8</sub> 4 <sup>13</sup> / <sub>16</sub> 5 <sup>13</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>8</sub> 6 <sup>1</sup> / <sub>4</sub> 7 <sup>3</sup> / <sub>16</sub> 8 <sup>1</sup> / <sub>8</sub>	4½ 5 6 6½	1/2 17/32 9/16 5/8

In the valve shown, the swing of the disc can be controlled by the plug stop.

## 186 HANDBOOK OF STANDARD DETAILS

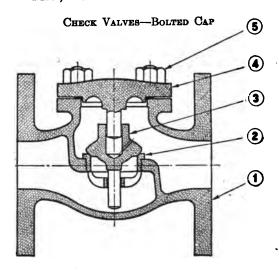
## SWINGING CHECK—STANDARD IRON BODY

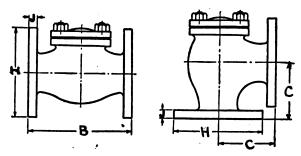


Number	Part ·	Number	Part
1	Body	6	Hinge
2	Seat	7	Hinge pin
3	Disc	8	Cap
4	Disc nut	9	Cap bolts
5	Disc pin		-

#### DIMENSIONS

Sin		н	J	Size Ins.	В	н	J
21 3 4 5	10 11 13 15	7 7½ 9 10	11 <sub>16</sub> 3/4 15/16 15/16	6 8 10 12	16 18 22 26	11 13½ 16 19	1 1½ 1¾ 1¾ 1¼



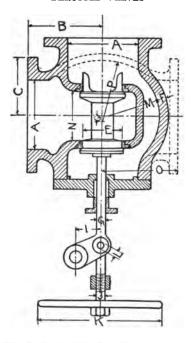


Horizontal and angle pattern, bolted bonnet, extra heavy brass

Number	1	2	3	4	5
Part	Body	Seat	Disc	Cap	Cap Studs
		Dim	ENSIONS		
Size, Inches.	B		C	Н	J
1½	63/8		3 <sup>8</sup> / <sub>4</sub>	6	9/16
2	73/8		4 <sup>1</sup> / <sub>8</sub>	6½	5/8
2½	83/4		4 <sup>5</sup> / <sub>8</sub>	7½	11/16
3	10		5 <sup>1</sup> / <sub>4</sub>	8¼	8/4

4

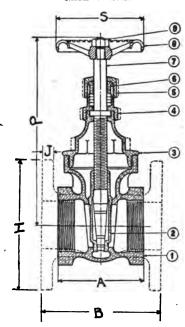
THROTTLE VALVES



A	В	C	Ε.	F	G	1	J	К	L	М	N	Lift of valve
4 5 5 <sup>1</sup> / <sub>2</sub> 6 <sup>1</sup> / <sub>2</sub> 8 <sup>1</sup> / <sub>2</sub> 9 11 12 13	6½ 7¼ 7¼ 8½ 9¾ 11 11½ 14	61/4  81/2 93/4 11 111/2 161/2 125/8	35/8 43/16 43/16 51/2 7 71/4 81/4 91/16 93/4	5/8 7/16 7/16 · 3/4 7/8 7/8 1 1 1/4 11/16	1 11/8 11/8 11/4 15/8 11/2 15/8 15/8	2 ½ 231/32 231/32 3 5/8 4 4 2 ½ 3	7/8 7/8 7/8 11/8 11/8 11/4 11/4	 8 8  9  9	78 78 118 112 112 112	61/4 73/4 83/4 91/2 111/2	2½ 3 3½ 4½ 6 6½ 7	1 1/4 1 1 1 1/4 2 2 1/2 2 1/4 2 1/3/2

All dimensions in inches. Valve shown operated either by wheel  $\kappa$  or by lever I.

GATE VALVES



## STANDARD BRASS-Non-RISING STEM

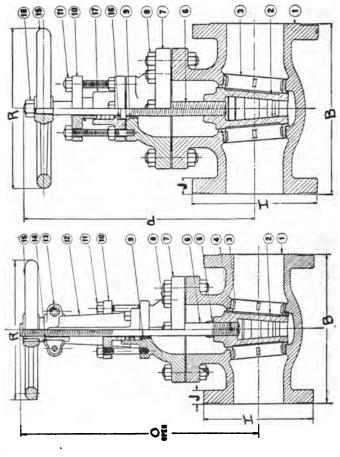
Number	Part	Number	Part
1	Body	6	Gland
2	Disc	7	Stem
3	Bonnet	8	Wheel
4	Stuffing box	x 9	Wheel nut
5	Stuffing nu	+	

#### DIMENSIONS .

Size Ins.	A	В	н	J	P	s
1 1½ 1½ 2	$2^{5/8}$ $2^{15}/6$ $3^{1/4}$ $3^{29}$ $3^{29}$	$3\frac{3}{8}$ $3\frac{7}{8}$ $4\frac{3}{8}$ $5\frac{1}{2}$	4 4½ 5 6	3/8 13/32 7/16 1/2	5 <sup>7</sup> / <sub>16</sub> 6 <sup>7</sup> / <sub>16</sub> 7 <sup>1</sup> / <sub>4</sub> 8 <sup>3</sup> / <sub>4</sub>	$2\frac{3}{4}$ $3\frac{1}{16}$ $3\frac{5}{8}$ $4\frac{1}{16}$

## 190 HANDBOOK OF STANDARD DETAILS

## IRON BODY-RISING AND NON-RISING STEM



Number	Part	Number	Part
1	Body	5	Stem ring
<b>2</b>	Disc	6	Stem
3	Body ring	7	Bonnet
4	Pin	8	Bonnet bolts

Number	Part	Number	Part
9	Bonnet bushing	14	Yoke sleeve
10	Gland	15	Wheel
11	Gland studs	16	Stuffing box bushing
12	Yoke	17	Stuffing box
13	Yoke bolts	18	Wheel nut

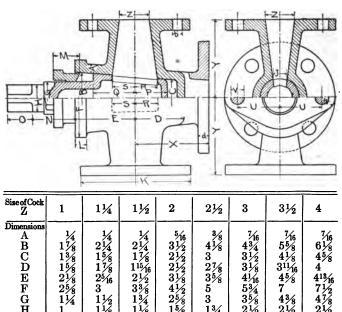
#### STANDARD DIMENSIONS

Sise Ins.	В	н	J	О	P	R
	7	6	5,6	141/2	118/	616
2 2½ 3 3½	7½ 8 8½	7	5 8 11 16 3 4 13 16 15 16 15 16 15 16	16	11¾ 12¾ 14¼ 15¼ 16¼ 17% 19 20¾ 23 26 28 30¼ 35¼	6½ 6½ 7½ 7½
31/2	1 0	7½ 8½ 9	13 16 15 2	16 19 21¼ 24 25½ 28½ 31¾ 37¼	1514	712
41/2	91/2	91/4	15 16 15 16	251/2	175/8	9
6	101/2	11	1	3134	2034	12
4 4 <sup>1</sup> / <sub>2</sub> 5 6 7 8 9	9½ 10 10½ 11 11½ 12	10 11 12½ 13½ 15 16 19	1 <sup>1</sup> / <sub>6</sub> 1 <sup>1</sup> / <sub>8</sub>	41	23 26	10 12 12 14 14 14 16
10	13	15 16	11/8 11/8 13/6 11/4	41 44 <sup>3</sup> ⁄ <sub>4</sub> 50	28 30¼	16
12	14	19	11/4	571/4	351/4	18

## EXTRA HEAVY DIMENSIONS

Size Ins.	В	Н	J	· o	P	R
1 1/4 1 1/2 2 2 1/2 3 3 1/2 4 4 1/2 5 6 7 8 9 10 12	61/2 71/2 81/2 91/2 111/8 117/8 115/8 161/4 161/2 17 18	5 6 6 <sup>1</sup> / <sub>2</sub> 7 <sup>1</sup> / <sub>2</sub> 8 <sup>1</sup> / <sub>4</sub> 9 10 10 <sup>1</sup> / <sub>2</sub> 11 12 <sup>1</sup> / <sub>2</sub> 14 15 16 <sup>1</sup> / <sub>4</sub> 17 <sup>1</sup> / <sub>2</sub> 20 <sup>1</sup> / <sub>2</sub>	34 13/16 17/8 1 1/8 1 1/8 1 1/4 1 1/	105% 1214 1334 16 1912 22 2412 27 2934 3418 38 4234 47 5234 60	834 958 1012 1278 1458 15734 1834 2014 23 2484 3012 3384 3714	5 5½ 6½ 7½ 9 10 12 12 14 16 18 20 20 22 24

## COCKS

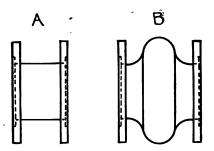


Dimensions								
	1/4	1/4	1/4	$ \begin{array}{c c} 5/16 \\ 31/2 \\ 21/2 \\ 21/2 \end{array} $	3/8	$   \begin{array}{r}     7_{16} \\     4_{34} \\     3_{12} \\     3_{18} \\     4_{18} \\   \end{array} $	7/6	7/16 61/8 45/8
В	$1\frac{7}{8}$	21/2	21/4	31/2	41/8	43/4	55%	61%
$\bar{\mathbf{C}}$	13%	15%	11%	$2^{\frac{1}{2}}$	3	31/3	41/8	45%
Ď	15%	17%	115/16	$2^{\frac{1}{2}}$	21/6	31/8	31176	1
$\widetilde{\mathbf{E}}$	$1\frac{1}{4}$ $1\frac{7}{8}$ $1\frac{3}{8}$ $1\frac{5}{8}$ $2\frac{1}{8}$ $2\frac{5}{8}$ $1\frac{1}{4}$	$2\frac{1}{4}$ $2\frac{1}{4}$ $1\frac{5}{8}$ $1\frac{7}{8}$ $2\frac{5}{16}$ $3$	14 214 178 1156 212 338 134 118	$2\frac{1}{2}$ $3\frac{1}{8}$ $4\frac{1}{2}$ $2\frac{5}{8}$ $1\frac{5}{8}$ $1\frac{1}{4}$	3/8 4 <sup>1</sup> /8 3 2 <sup>7</sup> /8 3 <sup>5</sup> /8 5	41/16	7/16 55/8 41/8 311/16 45/8	418/16 71/2 47/8
F	25/8	3	33/8	$4\frac{1}{2}$	5	$5\frac{3}{4}$	1 7 1	$7\frac{1}{2}$
G	11/4	11/2	13/4	$2\frac{5}{8}$	3	35/8	43/8	47/8
H l	1	$1\frac{1}{8}$	$1\frac{1}{8}$	15%	$1\frac{3}{4}$ $1\frac{1}{2}$	21/2	21/2	21/2
J	5/8	3/4	7/8	11/4	11/2	$1\frac{7}{8}$	$2\frac{1}{8}$	$2\frac{1}{2}$
ABCDEFGHJKLMNOPQRSUVWXY	4	11.1.2.8.4.2.8.8.8.8.8.16.8.8.2.16.8.8.2.16.8.16.8	5	6 1 <sup>5</sup> / <sub>16</sub> 1 <sup>1</sup> / <sub>2</sub> 1 <sup>5</sup> / <sub>8</sub>	7	$\begin{array}{c} 4\frac{1}{16} \\ 5\frac{3}{4} \\ 3\frac{5}{8} \\ 2\frac{1}{2} \\ 1\frac{7}{8} \\ 7\frac{1}{2} \\ 2\frac{1}{8} \end{array}$	21/2 21/8 81/2 21/2	21/2 21/2 9 2 4 2 1 7/8 2 1 1/16 3 3 5/16 2 1 1/16 3 3 5/16 3 1 5/16 3 1 5/16 5 5/16 5/16 5/16 5/16 5/16 5/16 5/16 5/16
L	5/8	<b>7</b> ∕8	$1\frac{1}{8}$ $1\frac{1}{4}$ $1\frac{1}{2}$	15/16	13/4	$2\frac{1}{8}$	$2\frac{1}{2}$	$2\frac{3}{4}$
M	11/8	11/8	11/4	1½	15/8	13/4	$1\frac{7}{8}$	2
N	13/8	13/8	11/2	15/8	13/4	17/8	$1\frac{7}{8}$ $1\frac{7}{8}$	11/8
0	7/8	<b>7</b> /8	1	11/4	$1\frac{1}{2}$	15/8	2	$2^{\circ}$
P	13/16	15/16	13/8	11/4 17/8	$1\frac{3}{4}$ $1\frac{5}{8}$ $1\frac{3}{4}$ $1\frac{1}{2}$ $2\frac{3}{16}$ $2\frac{5}{8}$ $1\frac{3}{4}$ $2\frac{3}{4}$	21/2	$2\frac{7}{8}$	$3\frac{3}{16}$
Q	13/8	15/8	13/4	21/4	$2\frac{5}{8}$	3	33/8	$3\frac{3}{4}$
Ř	11/16	13/16	7/8	11/4	17/16	13/4	2	25/16
$\mathbf{s}$	7/8	7/8	11/8	11/2	13/4	21/6	23/8	$2^{11}_{16}$
U	$1\frac{7}{16}$	15/8	113/16	$2\frac{7}{16}$	$2\sqrt[3]{4}$	$3\frac{3}{16}$	35%	315/16
V	1/2	1/2	1/2	5/8	· $\frac{3}{7}\frac{4}{8}$	3/4	3/4	3/4
$\mathbf{w}$	9/6	9/6	9/16	3/4	1 7/8	<b>7/8</b>	7/8	<b>7</b> ∕8
$\mathbf{X}$	25%	25%	$2\frac{3}{4}$	35/8	I 4	43%	$5\frac{1}{4}$	$5\frac{3}{8}$
Y	25%	23%	21/8	33/4	41/4	45%	53/8	$5\frac{1}{2}$
b	5/8/8/8/8/13/8/8/13/8/8/13/8/13/8/13/8/1	1/16	13/8 13/4 7/8 11/8 11/8 11/9 16 23/4 27/8	21/4 11/4 11/2 27/6 5/8 33/4 35/8 33/4 5/8	5/8	13/4 17/8 15/8 21/16 33/4/8 21/16 33/4/8 44/8 44/8 44/8 44/8	17/8 2 7/8/8 2 23/8/8/4/8/4/8/8 2 23/5/8/7/1/3/5/8 5 5 5 5 5	5/8
b Number of bolts	4	4	4	4	4	4	4	8
Dia. of bolt circle	3	33/8	37/8	43/4	$5\frac{1}{2}$	6	7	7½
d	3/8	7/16	7/16	1/2	1/2	9/16	5⁄8	7½ 5/8

#### **EXPANSION JOINTS**

Of the joints shown on the following pages, the copper expansion joints are for pressures up to 25 lbs., while those of the stuffing box type are for higher pressures as in main steam lines.

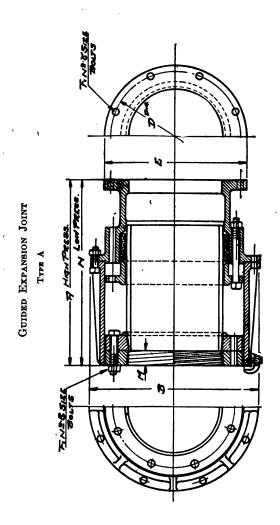
COPPER EXPANSION JOINTS



Copper expansion joints A and B are recommended where the expansion and contraction does not exceed ½ in. A is particularly suitable for high vacuum systems. Besides the joints shown there are others made of corrugated copper which may be used for pressures higher than 25 lbs. Pipe lines must be anchored to force the joints to compensate for the expansion and contraction in the pipe.

Size of		o face inges	Dia. of	Size		o face inges	Dia. of
pipe	Туре А	Туре В	flanges	pipe	Туре А	Туре В	flanges
4 5 6	5½ 5½ 6	8 9 9	9 10	14 15	6	12 12	21 221/4
7 8	6	10 10	$12\frac{1}{2}$ $13\frac{1}{2}$	16 18 20	$   \begin{array}{c c}     6\frac{1}{2} \\     6\frac{1}{2}   \end{array} $	12 13 13	$23\frac{1}{2}$ $25$ $27\frac{1}{2}$
9 10 12	6 6 6	11 11 11	15 16 19	22 24 26	7 7 8	14 14 15	$ \begin{array}{c}   29\frac{1}{2} \\   32 \\   34\frac{1}{4} \end{array} $

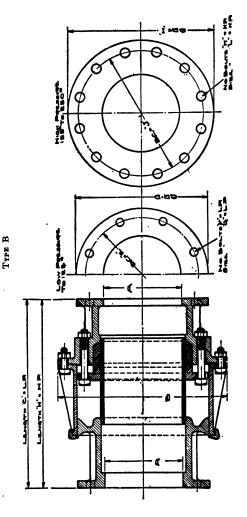
[Crane Co., Chicago, III.]



Pipe Size	11%	11%	2	21/2	3	31%	4	41%	5	9	1	8	6	10	12
( 4" Trav	151%	151%	1638	1616/4	17.14	171%	1739%	1811/4	1815	18174	1915	211%	213%	2576	251/2
A \ 8" Trav	2315/2	2315/2	2315/6	2411/4	25%	25%	254/6	261/4	2615/4	2611/4	2681/2	2818/2	28%	301%	3018
(12" Trav	3178	3115	3115%		337%	333%		341/2	34%	3411/2	3481/2		363%	3819	3818
В	778	778	878		1178	12		121/2	13%	14%	161%			20%	221/2
) Q	3%	435	2		8%	7,		87%	9%	10%	11%			15%	17%
E   High Press	10	9	67%	7%	87%	6	20	101%	11	12%	14	15		17.75	20%
	4-1%	4-5%	4-%		8/2/2/2/2/2/2/2/2/2/2/2/2/2/2/2/2/2/2/2	1/2/2		%-8	8-%	12-3%	12-7%			16-1	16-11/8
д	33%	37%	<b>4</b> %		9	~		7%	87%	9%	10%			14%	17
E < Low Press	475	2	9		7,	872		9%	91	11	121%			16	19
_	4-7/6	4-1%	4-5%		45%	4 5%		%	8	%	8			12-7%	12-78
М	%	%	%		11%	13%		15%	13%	17,	1,7			178	61
( 4" Trav	1511/4	151/4	1578	16%	1678	171%		1781/2	181/6	18%	1912			24%	24%
N \ 8" Trav	23%	2374	2311/6	241/6	243%	22		25%	<b>5</b> 61 <b>⁄4</b>	25%	2619%		_	292%	30%
( 12" Trav	3174	3174	3111/6	321/4	32%	33	33174	334/4	3325/2	3339/4	3417/2	35%	36%	3730	38%
							-			_	-				

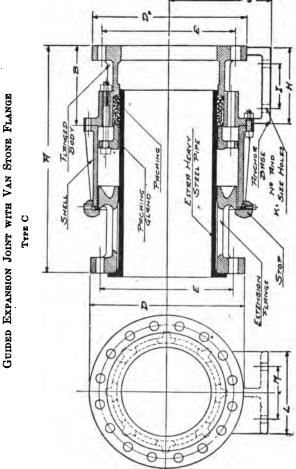
[Howard Iron Works, Buffalo, N. Y.]

GUIDED EXPANSION JOINT WITH EXTENSION FLANGE



12	2235 3356 41156 53156 19 · 17 12	33% 411% 531% 20% 17% 16
10	20% 331% 415% 535% 16 12 12	33.7 2.7 2.7 2.7 3.7 3.7 4.7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
6	183% 29 395% 515% 113%	29 395% 515% 161% 12
8	173% 285% 3815% 5015% 133% 113% 8	28 5% 38 15% 50 15% 15 13 12
7	165 277 377% 497% 1037 8	27% 37% 49% 11 11% 78
9	14 14 14 14 14 14 14 14 14 14 14 14 14 1	25% 36% 48% 12% 10%
22	13.7 25.3% 37.3% 10 8.7% 8.7%	25% 37% 48% 111 8 8 8
41%	25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72 25.72	255% 365% 4885% 1035 835 8
4	247% 365% 488% 9 9 777 8	247% 365% 485% 10 77% 8
31%	12 2476 351876 471876 835 7 7	2476 35136 47136 9 776 8
8	11178 23378 35774 4777 6 6 8 8	23.75 35.76 47.77 87.78 8 8 78
21/5	22 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	22.78 34.78 46.78 77.78 77.78 77.78 78.78
2	99% 34,7% 6 6 74 4 8 74 74 74 74 74 74 74 74 74 74 74 74 74	22.2 34.7 46.7 6.7 7 7 7 8 8 8
11%	77% 221% 3311% 4511% 5 37% 4	221/6 3311/6 4511/6 6 4 4/5 4
11/4	2115 33% 45% 45% 4 45% 4 47% 4 47%	21 <sup>115</sup> / <sub>4</sub> 333% 45% 5 33% 4
A—Sire of Pipe	C = Length of 4"Travel C = Length of 4"Travel C = Length of 12"Travel C = Length of 12"Travel D = Diam. Flange E = Bolt Girele F = No. Bolts	H = Length of 4"Travel     H = Length of 8"Travel     H = Length of 12"Travel     I = Diam. Flange
	Low Press.	High Press.

[Howard Iron Works, Buffalo, N. Y.]



## PIPE, TUBES AND FITTINGS '

			High	High Pressure	sure					-	3oth F	Both Pressures	<b>8</b>					Low	Low Pressure	sure			
	Tra	frav'se	Tra	8" Trav'se	Tra	12" Trav'se	All Trav'ses	Ses.			All Tr	Ill Trav'ses				Tra	4" Frav 86	8" Trav'se	8	12" Trav'se	36.	All Trav'ses	858
Fipe	A	В	4	В	Ą	В	D	田	H	н	-	K	-1	M	Pipe Size	A	Ħ	A	В	4	м	Q	M
35	229	73%					10			- 1		-		270	114					4529	151%	41/2	523
13.6	22134	735	34%	1138	46%	1596	9	41/2	678	312	512	4-96	10	60	13/2	22%	735	33 29	111/8	45.29	151/8	10	378
	23	77%					634					3.		*	67					46%	1576	9	43
3.6	2319	715/6				-	77.2							4	23/2					475%	151/2	-	51
**	2435	85/4					814						-	4	600	_				48	1513/6	73%	9
375	24136	83					6					-		4	33/2	_				483/10	1578	812	7
	25%	811.16					10							4/2	*					4839£	165%	6	73
20	25 36	6				***	101/2							10	416	_				49%	16%	9%	+78
	254322	976				****	11							10	10	_				4995	163,8	10	83
	263	976			-41		123/2							10	9	_				49195	16%	11	93
	27136	966			41.0		14				-			10	1	_				50%	1634	123/2	103
4	2916	1014				_	15							9	00	2868				51232	177/6	13%	118
	2938	1038			_		1614							9	6	20				523,8	1776	15	133
	333%	113%			-		171/2		-					7	10	33)8				5492	183.8	16	141
	8416	1116					2035			9	1335			1	12	333%				54136	1874	19	17

[Howard Iron Works, Buffalo, N. Y.]

## SECTION V

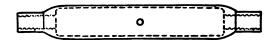
#### ROPE AND CHAIN FITTINGS

TURNBUCKLES—SLEEVE NUTS—THIMBLES—SOCKETS—WIRE ROPE—
SHACKLES—SISTER HOOKS—CLEVIS NUTS—EYE BOLTS—
HOOKS—SLINGS—ROPE AND CHAIN—CHAIN—HOIST—
ING AND ANCHOR—DRUM SCORES FOR
CHAIN AND ROPE

#### TURNBUCKLES

Turnbuckles may have rods with eye or hook ends of sizes shown on pages 211 and 212, one of which is threaded right hand and the other left.

PIPE TURNBUCKLES

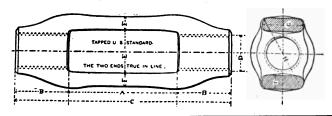


Dia. of screw	Threads per in.	Size of pipe*	Overall length of turnbuckle	Length of screw end	Dia. of screw end
3/8	16	1/2	5	5/8	3⁄4
1/2	13	3⁄4	51/2	7∕8	1
5/8	11	1	. 7	11/8	11/4
3/4	10	1	7	11/8	1½
7∕8	9	11/4	8	11/4	13/4
1	8	1½	91/2	1½	2

<sup>\*</sup> See page 163. Hole for pin 1/4 in. dia.

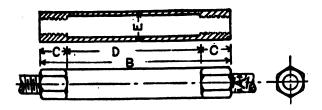
## ROPE AND CHAIN FITTINGS

#### TURNBUCKLES WITH PLAIN STUBS



Size D Out. Dia. Screw, Inches	A Inches	B Inches	C Inches	E Inches	H Inches	F Inches	G Inches
3/8/1/2 5/8/8/1/2 5/8/8/1/2 5/8/8/1/2 11/2/8/1/2 11/2/8/1/2 11/2/8/2 11/2/8/2 11/2/8/2 11/2/8/2 11/2/8/2 11/2/8/2 11/2/8/2 11/2/8/2 11/2/8/2 11/2/8/2 11/2/8/2 11/2/8/2 11/2/8/2 11/2/8/2 11/2/8/2 11/2/8/2 11/2/8/2 11/2/8/2 11/2/8/2 11/2/8/2 11/2/8/2 11/2/8/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 11/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8 1/2/8	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	Inches  9,16,21,22,33,42,21,56,66,16,16,16,16,16,16,16,16,16,16,16,16	7 1/8/66 7 7 1/4/68 7 7 1/4/68 8 8 5/8 9 3/4/18 110 7/4 111 5/8 12 12 3/4 13 1/2 13 1/4 14 15/8 15 15 3/4 16 1/2 17 1/4	Inches  9,66,86,86,66,66,66,66,66,66,66,66,66,66,	11/66 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/3/8 11/	3.66 1.44 1.54 1.55 1.65 1.15 2.25 1.36 1.15 1.36 1.15 1.36 1.15 1.36 1.15 1.36 1.15 1.15 1.15 1.15 1.15 1.15 1.15 1.1	Inches  1/2 5/8 5/8 3/4 3/4 11/4 11/4 11/5/8 13/4 11/8 21/8 21/2 21/2 21/2 3/4 31/4 31/4 31/4 51/8 6
41/4 41/2 43/4 5	9 9 9	6 1/4 6 3/4 7 1/4 7 1/2	21 ½ 22 ½ 23 ½ 24	5 5 3/8 5 1/2 5 7/8	$ \begin{array}{c c} 10\frac{1}{8} \\ 10\frac{1}{4} \\ 11\frac{3}{8} \\ 12 \end{array} $	$ \begin{array}{c} 15_{8} \\ 13_{4} \\ 2 \\ 2\frac{1}{4} \end{array} $	$ \begin{array}{ c c c } 6 & & & \\ 6 & & & \\ 6 & & & \\ 6 & & & \\ 6 & & & \\ 6 & & & \\ \end{array} $

HEXAGON END PIPE TURNBUCKLES

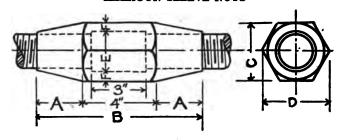


Diameter of Screw	Threads per Inch	Length of Swivel B	Length between Heads D	Length of Heads	Outside diameter of Pipe E
3/8 1/2 5/8 3/4 7/8	16 13 11 10 9	in. 5 5½ 7 7 8	in. 334 334 434 434 51/2	in.  \$ /8  7/8  11/8  11/4	in. .840 1.050 1.315 1.315 1.660
1 11/8 11/4 13/6 11/2 15/6 13/4 17/8	8 7 7 6 6 5 5 5 5	9½ 9½ 11½ 11½ 13½ 13½ 13½ 13½	61/2 6 8 8 81/2 81/2 91/2	11/2 18/4 18/4 11/2 21/2 21/2 21/2 23/4	1.900 1.900 2.375 2.375 2.875 2.875 2.875 2.875 3.500
2 2 <sup>1</sup> / <sub>8</sub> 2 <sup>1</sup> / <sub>4</sub> 2 <sup>3</sup> / <sub>8</sub> 2 <sup>1</sup> / <sub>2</sub> 2 <sup>3</sup> / <sub>4</sub>	41/2 41/2 41/2 4 4 4	15 15 16½ 16½ 18½ 18½	9½ 9½ 11 11 12 12	284 234 234 284 314 314	3.500 3.500 4.000 4.000 4.500 4.500
3	. 3½	19½	123/4	33/8	5.000

[Hoopes & Townsend Co., Philadelphia, Pa.]

With this type of turnbuckle a wrench with an hexagonal opening (page 238) is required to turn it.

## HEXAGON SLEEVE NUTS

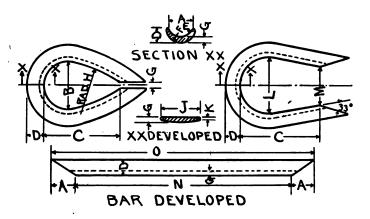


Dia. of Screw	A	В	С	D	Æ	F	Wt. Lbs.
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	7 7 7 7 7 7 7 2 8 8 8 1 2 9 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	158 188 2 2 2 2 3 4 4 8 8 9 2 2 3 4 4 8 8 8 9 2 2 3 4 4 8 8 8 9 2 2 3 4 4 8 8 8 9 2 2 3 4 4 8 8 8 8 9 2 2 3 4 4 8 8 8 8 8 9 2 2 3 4 8 8 8 8 9 2 2 3 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	1 1 2 2 2 3 3 3 5 5 8 6 6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	111 11 11 11 11 11 12 2 2 2 2 2 2 2 3 3 3 3		3 3 4 4 5 6 8 9 10 11 14 15 18 19 23 27 28 35 40 47 55 65 75

[Pocket Companion—Carnegie Steel Co.]

Hexagon sleeve nuts largely used in tie rod connections.

# ROPE THIMBLES



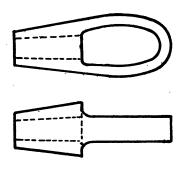
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[Upson-Walton Co., Cleveland, O.]

Thimbles are usually galvanized.

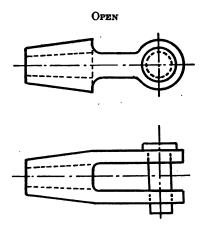
#### WIRE ROPE SOCKETS





Sine Dame	Extreme	Basket							
Size Rope Dia.	Length	Length	Large Diameter Outside	Small Diameter Outside					
1/4/6/8 3/6/8 1/6/8 1/8 1/8 1/8 1/8 1/8 1/8 1/8 1/8 1/8 1	35% 34% 41/2 41/2 51/4 51/4 61/8 7 8 91/4 111/2 13 13	15/8 15/8 2 2 21/4 21/4 25/8 31/2 4 5 55/3/4	13/6 13/16 17/16 17/16 13/4 13/4 23/4 23/4 31/4 4 43/4 43/4	5 8 15 16 12 16 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1					

The socket should have a tapered hole or one as shown on page 207. The rope wires may be bent over, and lead or other soft metal poured in.

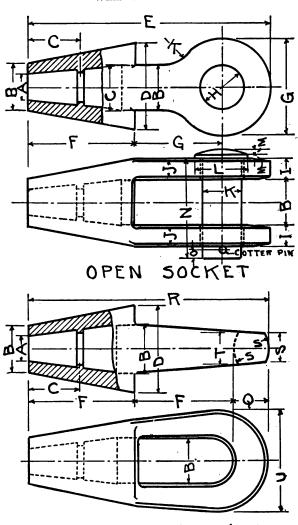


	Extreme Length		Basket		
Size Rope Dia.		Length	Large Diameter Outside	Small Diameter Outside	Diameter Pin
1/6 8/8 1/6 1/2 1/6 8/4 11/8 11/4 11/4 11/6 11/6	37/6 37/6 43/8 43/8 51/8 6 67/8 91/8 91/8 113/8 113 13	15/8 15/8 2 2 21/4 21/4 25/8 31/2 4 4 5 5 53/4	13/6 13/6 17/6 17/6 13/4 13/4 2 23/8 23/4 31/4 4 4 43/4	5 8 5 8 13 16 13 16 1 3 16 1 15 16 1 15 16 1 15 16 2 3 8 2 3 4 2 3 4	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 2 1 1 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

[J. H. Williams Co., Brooklyn, N. Y.]

Pins have a  $\frac{1}{8}$  in. split pin in end close to shoulder. For securing rope in socket see pages 205 and 207.

WIRE ROPE SOCKETS



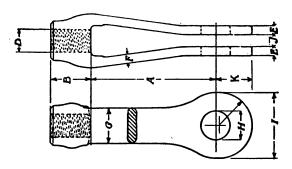
CLOSED SOCKET

WIRE ROPE SOCKETS—Continued

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[Upson-Walton Co., Cleveland, 0.] \* P = Cotter or Split Pin.

# **CLEVIS NUTS**



							Dia	mete	r of l	Pin					
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11/8		X		3	3	3	31/2	31/2			+ + 0	1.34			
11/4	2.4.4	XX.5	200	3	3	3	3/2	31/2	:	2.45					
13/8				3	3	3/2	31/2		4	4.4.4		1.4.6		4.1	
11/2						31/2	4	4	434		251			45.4	
15/8	+ + +				4	4	4	434	43/4	43/4				25.6	
134				,	+	43/4	43/4	43/4	43/4	43/4					
17/8							434	43/4	434	$5\frac{3}{4}$	$5\frac{3}{4}$				-
21/8							434	43/4	$5\frac{3}{4}$	53/4	$5\frac{3}{4}$				
21/8								$5\frac{3}{4}$	$5\frac{3}{4}$	$5\frac{3}{4}$	$5\frac{3}{4}$	53/4	225		
21/4									$5\frac{3}{4}$	$5\frac{3}{4}$	53/4	63/4			4
23/8								$5\frac{3}{4}$		$5\frac{3}{4}$	634		634	63/4	
21/2										634	634	634	63/4	63/4	
25%							V		634	63/4		1 1 1 1	774	8	8
234										634	634	63/4	8	8	8
3		1									8	8	8	8	8

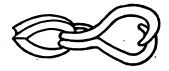
For dimensions of nuts see page 210.

CLEVIS NUTS-Continued

I	В	A	K	G	F	E	J
2 2 <sup>1</sup> / <sub>2</sub> 3 3 <sup>1</sup> / <sub>2</sub> 4 4 <sup>3</sup> / <sub>4</sub> 5 <sup>3</sup> / <sub>4</sub> 6 <sup>3</sup> / <sub>4</sub> 8	114 136 134 2 238 238 2314 31/2 4 1/2 434	5½ 5½ 6 6½ 7 8 9 10 12 12	11/8 17/6 111/6 115/6 21/4 25/8 33/6 33/6 31/8 41/2 5	1 114 158 178 218 218 212 3 34 4 412	3 8 6 1 2 6 8 23 32 27 32 15 16 1 1 16 1 15 16	3 8 15 17 17 12 19 12 22 22 22 22 15 16 11 16 11 12 2	To suit Pin Plate

Dimension "E" will vary slightly, depending upon dimension "J." [Cleveland City Forge & Iron Co., Cleveland, O.]

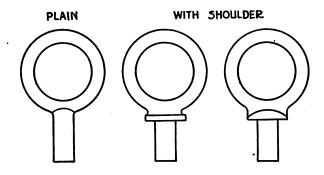
## SISTER HOOKS WITH WIRE ROPE THIMBLE



Size of Iron, Inches	Size Score of Thimble, Inches	Length of Hook, Inches	Diameter of Eye, Inside Inches	Gov't Test. Maximum Strength in Pounds
14 5/6 8/8 1/2 5/8 1/8 1 1/8 1 1/4	3/6 1/4 5/6 1/6 1/2 5/8 3/4 1 1/8	2 1/8/8/8/2 2 1/8/8/8/8/4/8/8/8/8/8/8/8/8/8/8/8/8/8/8/	9/6 5/8 11/16 7/8 11/16 13/16 13/8 15/8	940 1,420 2,030 3,800 7,100 8,920 11,020 11,100 13,050 19,200

For dimensions of thimbles see page 204.

EYE BOLTS

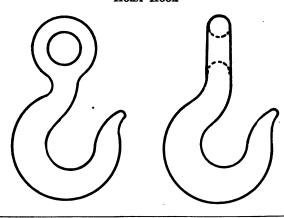


Sh	ank	Maxi-	Diame	ter Eye	Capa	Capacity, Net Tons			
Diamı	Standard Length under Shidr.	mum Length in Stock	Inside	Outside	Safe Working Load	Average Load at Elastic Limit	Approx- imate Breaking Strain		
14468876626884488 18442244	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3 4 4 4 4 4 4 5 5 5 5 6 6 6 6 6	34 78 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	13/6 17/6 12/2 127/2 21/6 22/2 21/3/6 22/2 21/3/6 3/6 4 47/6 6/7/8	.2 .4 .7 1.3 1.5 2. 3.5 4. 5. 7.5 9. 11.	.59 1.4 2.53 3.4.6.7.8.10.15.18.21.25.	1.5 2.3.4.5.6.8.12.16.20.23.33.42.53.68.		

[J. H. Williams Co., Brooklyn, N. Y.]

Plain eye with shank used for turnbuckle ends. Length of ends made to suit turnbuckle.

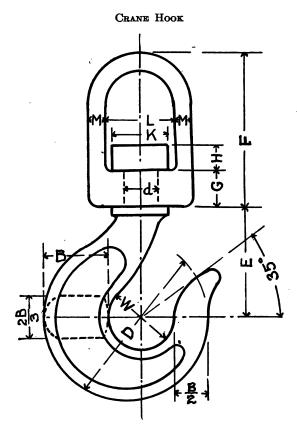
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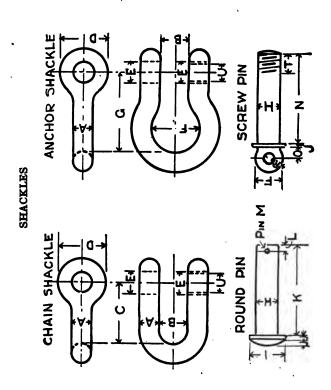
				Сар	acity, Net	Tons
Diamete	er of Eye	Extreme 1	Dimensions	Safe	Average Load at	Approxi- mate Load
Inside	Outside	Length	Width	Working Load	Elastic Limit	Required toStraight- en out
3/4 - 7/8 1 11/8	$ \begin{array}{c c} 1\frac{1}{2} \\ 1\frac{3}{4} \\ 2 \\ 2\frac{1}{4} \end{array} $	43/8 47/8 53/8 63/16	27/8 31/8 31/2 37/8	.5 .6 .7 1.2	.9 1.2 1.5 2.5	1.9 2.3 3. 5.7
$1\frac{1}{4}$ $1\frac{3}{8}$ $1\frac{1}{2}$ $1\frac{5}{8}$	$ \begin{array}{c c} 2\frac{1}{2} \\ 2\frac{3}{4} \\ 3 \\ 3\frac{1}{4} \end{array} $	67/8 75/8 89/16 99/16	4 <sup>3</sup> / <sub>8</sub> 4 <sup>7</sup> / <sub>8</sub> 5 <sup>5</sup> / <sub>8</sub> 6 <sup>3</sup> / <sub>8</sub>	1.7 2.1 2.5 3.	3.5 4.2 5.4 6.2	7. 8.5 10. 13.
$1\frac{3}{4}$ $2$ $2\frac{3}{8}$ $2\frac{3}{4}$	$\begin{array}{c c} 3\frac{1}{2} \\ 4 \\ \cdot 4\frac{5}{8} \\ 5\frac{1}{4} \end{array}$	10 <sup>3</sup> / <sub>8</sub> 11 1/ <sub>2</sub> 13 14 3/ <sub>4</sub>	67/8 71/2 81/4 91/4	4.7 5.5 6.8	8. 9. 11. 13.	17. 19. 26. 32.
$   \begin{array}{c}     3\frac{1}{8} \\     3\frac{1}{2} \\     4   \end{array} $	6½ 7 8½	$\begin{array}{c c} 16\frac{3}{4} \\ 19\frac{1}{8} \\ 22\frac{1}{2} \end{array}$	10 1/8 13 14 3/4	8. 11. 20.	17. 21. 40.	35. 48. 80.

[J. H. Williams Co., Brooklyn, N. Y.]

Hook without eye, but with plain shank used for turnbuckle ends.



Based upon a stress of 3,500 lbs. per sq. in., dia. d of shank of hook = .02  $\sqrt{\text{load.}}$  The width of the hook W = B the width of the hook body, the thickness being  $\frac{2B}{3}$ .

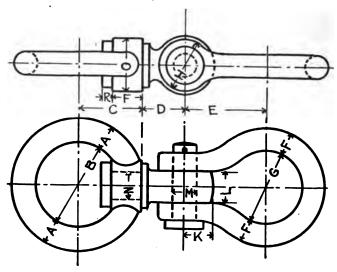


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†8 - threads per in. \* P = dia. of collar on screw pin. [Upson-Walton Co., Cleveland, O.]

## SWIVEL SHACKLES

## Stationary Chain Swivels



## d = diameter of chain

A = 2 d	H = 4 d
B = 7 d	K = 2 d
C = 5 d	L = 2 d
D = 3 d	M = 2 d
E = 7 d	N = 2 d
$\mathbf{F} = 1.8  \mathbf{d}$	O = 4.3 d
G = 6 d	R = 1.5 d

## Anchor Chain Swivels



Diameter of metal in swivel = 1.8 d

Inside diameter of swivel = 6 d

Inside length of swivel = 9 d

Thickness of swivel at shackle = 2 d

Swivel pin (N) dia. = 1.4 d

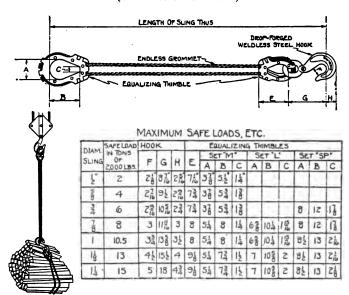
Dia. of metal in shackle = 1.4 d

For dimensions of shackles see pages 214 and 215.

In an anchor chain there should be three or four swivels, the first about five fathoms from the anchor.

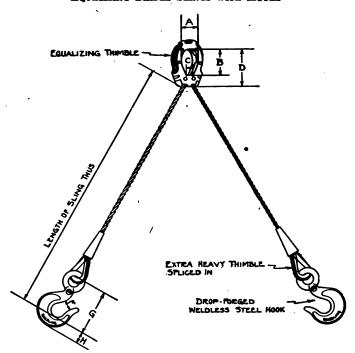
#### WIRE ROPE SLINGS

# EQUALIZING SLINGS WITH HOOK (Grommet Construction)



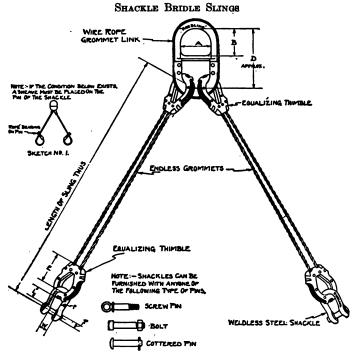
## 218 HANDBOOK OF STANDARD DETAILS

# EQUALIZING BRIDLE SLINGS WITH HOOKS



		ds in tons 00 lbs.		Hook	Hook				E	qual	iring	Equalizing Thimbles							
Dia. Sling	When Used	When Used	P		,,,	I	Set	'M'			Set	"L"		8	et "	SP"			
	Vertical	60° Angle	F	G	H	A	В	c	D	A	ĮB	C	D	A	В	c	D		
	3 4.5 6.25 9 11.5 14 17 20 23 25 29	2.5 4 5.5 8 10 12 14.5 17 20 22 25	11 2 2 2 2 2 2 3 3 3 3 3 4 4 5 5	1276	136 12 256 276 276 3 3 3 4 4	33335555669	55588 779944 15	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	72" 88 101 101 101 101 13 17 191	65 7 7 8 5 1	101" 101 101 101 13	1100 1100 1100 22 2100 22 2100 240	13" 13 13 13 16 16 16 16 16 16 16 16 16 16 16 16 16	8" 81 81 81	12" 12 13 13 13	12" 12" 1256 236 24	15" 15 16 16 16		

[J. A. Roebling's Sons Co., Trenton, N. J.]



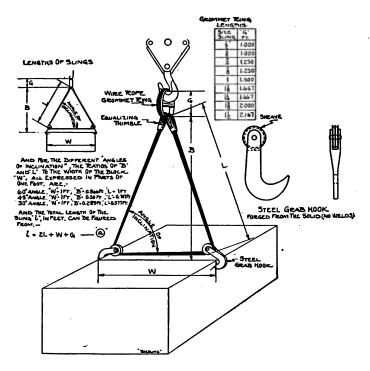
	Safe I	oads in To	ns of 2,0	00 Lbs.	1	F	ittings	<del> </del>
Dia . Sling	When	When used	When used	When used		_	_	
onug	Y	60° Angle	45° Angle	30° Angle	A	В	D	E
1/2" 5/8 3/4 7/8	4	4	3	2	6"	6"	12"	73/4"
5/8	8	7	5.5	4	6	6	12	83/8
3/4	12	10	8.5	6	71/2	7½	15	838 8 8
<b>7∕8</b>	16	13.5	11	8	71/2	7½	15	8
1	21	18	15	10.5	9	9	18	8
11/8	26	22	18.5	13	10	10	20	81/2
11/4	30	26	21	15	10	10	20	81/2
13/8	34	29	24	17	12	12	24	1111/4
11/2	40	34	28	20	13	13	26	111/4
15/8	44	38	31	22	13	13	26	111/4
134	50	43	35	25	14	15	30	191/2

Note—Dimensions "F, L, P and W" of shackles are designed to suit the member hoisted. [J. A. Roebling's Sons Co., Trenton, N. J.]

#### HOOK BRIDLE SLINGS

Same construction as Shackle Bridle Slings except hooks are used instead of shackles. For size of hooks see Equalizing Bridle Slings with Hooks.

#### SLINGS FOR HANDLING STONE BLOCKS



The wire rope grommet ring may be omitted, the equalizing thimbles being attached to the hook. In this case the length of the sling  $l=2\ L+W$ .

The sling shown is also suitable for handling steel plates.

SIZE OF SLINGS REQUIRED FOR DIFFERENT LOADS AND ANGLES
OF INCLINATION

wr. 1 1	Approximate _	Ang	de of Inclinatio	n
Weight of Block	Cubic Feet	60°	45°	30°
4,000*	24	1/2"	1/2".	1/6'
8,000	48	1/2	5%	5%
10.000	60	5/8	5%	8/4
15.000	90	3/4	3/4	<b>7</b> /8
20,000	120	3/4	· 7/8	1 1
25,000	150	7/8	1	11/8
30,000	180	1	1	11/4
35,000	210	1	11/6	$1\frac{3}{8}$
40,000	240	11/8	11/4	11/2
50,000	300	11/4	11/2	· •

<sup>\*</sup>Note—Above figured from—"Marble" at 165 lbs. per cu. ft.; "Granite" 3% heavier.

#### **CHAINS**

#### HOISTING CHAINS

The working load of a chain should not be above one fourth, and at most not over one third of its breaking strength, or but little over one half the proof test.

The distance from the center of one link to the center of the next is the pitch of the chain.

Chains for hoisting purposes should have short links in order to wrap snugly around the drum or sheave without bending.

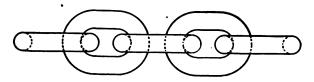
The life of a chain can be increased by frequent annealing and lubricating. If the wear is not uniform throughout the length, the chain should be cut and pieced where partially worn.

Chain having the trade name "B B B" crane chain, dimensions of which are given on page 222, is widely used not only for cranes but for general hoisting.

Drum scores for chain are given on pages 224-225.

Rings are made of heavier stock than the chain—see page 226.

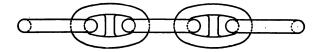
B. B. CRANE CHAIN



Sise Inches	Approximate Links per Foot	Outside Length Inches	Outside Width Inches	Weight per 100 Feet	Proof Test	Approximate Breaking Strain
16 16 16 16 16 16 16 16 16 16 16 16 16 1	15 14 12 11 10 9 814 714	11/8 13/8 15/8 15/8 21/8 23/4 3	3/4 15/16 11/8 17/16 19/16 13/4 2 21/8	52 83 118 175 215 275 340 435 620	1,200 1,750 3,400 4,500 6,300 8,000 10,000 12,500 17,750	2,400 4,500 7,000 9,000 12,500 16,500 22,000 25,000 35,000
1/8 1 1/8 11/4	5 <sup>8</sup> 4 5 4 <sup>8</sup> 4 4 <sup>1</sup> / <sub>2</sub> 4	3½ 4½ 4½ 45/8 5½ 53/4	29/16 3 31/2 37/8 41/4	830 1,040 1,400 1,665	24,000 31,350 38,000 47,000	47,500 64,500 78,000 95,000

[Columbus-McKinnon Chain Co., Columbus, O.]

#### ANCHOR STUD LINK CABLE CHAIN



Studs in chains keep the chains from closing when they are overstrained.

One shot of chain = 15 fathoms = 90 ft.

Ships built in the United States have anchor chain of the dimensions given on page 223.

# (New American Measurements, adopted Aug. 21, 1917)

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	rain	Break Strai Poun	Proof Test Pounds	Average Weight Per Fathom Pounds	ngth of x Links butside t In.		Outside Width of Link Inches	Outside Length of Link Inches	Size Chain Inches
11/6	3,880	33,	22,680		7½		25/8	41/2	3⁄4
11/6	9,872	39,	26,600		$9\frac{1}{8}$		$2\frac{7}{8}$	47/8	13/16
11/6	6,200	46,	30,800		10%		31/8	51/4	$\frac{7}{8}$
11/6	3,088		35,392	53	3/8	2	3%	55/8	15/16
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0,480				2	2	39/16	6	1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8,096	68,	45,472		35/8	2	33/4	63/8	11/16
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6,440	76,	50,960		$5\frac{1}{4}$	2	4	63/4	11/8
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5,120	85,	56,840		$6\frac{7}{8}$	2	41/4	71/8	13/16
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4,360	94,	63,000		8 1/2	2	41/9	7½	11/4
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4,160	104,	69,440		$10\frac{1}{8}$	2	43/4	71/8	15/16
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4,240		76,160		$11\frac{3}{4}$	2	415/16	81/4	13/8
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4,600		83.160		13/8	3	58/10	85/8	17/16
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1,488	131,	90.720		3	3	53/g	9	$1\frac{1}{2}$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7,536	137,	98,336		45/8	3	5%	93/8	19/6
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8,960	148,	106,400		61/4	3	51/8	98/	1%
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0,720	160,	114,800		$7\frac{7}{8}$	3	$6^{1}/_{6}$	101/6	111/16
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2,760	172,	123,480		91/2	3	65/6	101/6 1	13/4
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5,360	185,	132,440		111/8	-3	$6\frac{1}{2}$	10 1/8	113/16
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8,240	198,	141.680		3/4		63/4	111/4	1 1/6
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1,680		151,200	221	23/8		7 1	11%	115/16
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5,792		161.280		4		73/16	12	2 1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9,904	239,	171,360		55/8		7/16	123/8	21/6
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4,800	254,	182,000	260	71/4	4	75%	123/	24/6
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9,920	269,	192,920	278	87/8	4	77/8	131/6	28/6
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5,600		204,120		101/2		81/8	131/2	21/4
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1,840	301,	215,600	313	1/8	5	85/16	137/8	25/0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	<b>8,304</b>	318.	227,360	330	13/4	5	89/16	141/4	$2\frac{3}{8}$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5,160	335,	239,456	348	33/8	5	834	143/8	21/40
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2,800	352,8	252,000	365	5	5	9	15	21/2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5,960	365,	261,408	383	65%	5	91/4	153/8	29/4
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9,120	379,	270,816	400	81/4	5	97/16	15¾ l	25/8
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2,280	392,3	280,224	418	97/8	5	911/6	161/8	211/6
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.440	405.4	289,632	435	111/2	5	97/6	161/6	23/4
$2\frac{7}{8}$ $17\frac{1}{4}$ $10\frac{1}{8}$ $6$ $2\frac{3}{4}$ $480$ $308,224$ $431$ $2\frac{1}{16}$ $17\frac{1}{9}$ $10\frac{1}{9}$ $6$ $4\frac{3}{8}$ $500$ $317,408$ $444$ $3$ $18$ $10\frac{1}{3}$ $6$ $6$ $4\frac{3}{8}$ $500$ $329,509$ $45$	3,320	418.	298,816		11/6	6	101/6	167%	213/4
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1,480	431.4	308,224		23/	6	103/6	1714	27/6
3   18   10132   6   6   590   296 509   455	1,360	444.3	317,408		43/8	6	10%	175%	215/16
(	7,184	457.	326,592		6		10 <sup>i3</sup> /4	18	3 1
$3^{1}_{16}$   $18^{3}_{8}$   11   6   $7^{5}_{8}$   540   $335,552$   469	,728	469.		540	75/8 91/4	6	11 "	$18\frac{3}{8}$ $18\frac{3}{4}$	31/6
31/8   183/4   111/4   6   91/4   560   344,400   482	2,160				91%		111/4	1834	31/8
3 16 19 18 11 12 6 10 18 585 353,248 494	1,480				101/8		111/6	191/8	33/6
31/6 183/8 11 6 75/6 540 335,552 466 31/8 183/4 111/4 6 91/4 560 344,400 482 33/6 191/8 111/2 6 107/8 585 353,248 494 31/4 191/2 1111/6 7 1/2 610 361,984 506	3,688				1/2		1111/6	191/2	31/4

#### CHAIN SLINGS

The table shows safe working loads in pounds of special "CC" sling chains when operated at different angles. When handling molten metals, sling chains should be 25% stronger than in the table

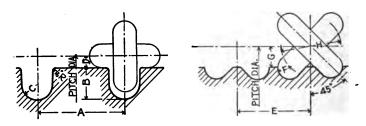
The safe working loads given are for each single strand. When used double or in other multiples, the loads may be increased proportionately.

	Diameter of Iron Inches	When Used Straight	When Used at 60-Degree Angle	When Used at 45-Degree Angle	When Used at 30-Degree Angle
"CC" Dredge Chain  (Best Grade of Hand-made, Tested, Short Link Chain.)	14 38 18 18 58 34 78 1 118 114 114	1,330 2,660 5,330 8,330 12,000 16,330 20,830 26,660 32,000 46,660	1,000 2,050 4,100 6,800 9,400 12,800 16,000 29,400 25,500 38,000	850 1,700 3,400 5,600 7,800 10,400 13,200 16,800 21,000 32,000	600 1,200 2,400 4,000 5,500 7,400 9,400 12,000 15,000 22,000

[Columbus-McKinnon Chain Co., Columbus, O.]

#### DRUM SCORES

#### FOR CHAIN



DRUM SCORES FOR CHAIN-Continued

Size of Chain	A	В	С	D	E	F	G	н
3 8 7 16 1 1 2 9 16 5 8 11 16 3 4 12 16 7 8 16 16 16	1 \\2 \\2 \\11\\6 \\2 \\2 \\6 \\2 \\2 \\7 \\8 \\2 \\7 \\8 \\2 \\7 \\8 \\2 \\7 \\8 \\8 \\3 \\8 \\8 \\8 \\8 \\8 \\8 \\8	916 558 1176 334 1376 788 1576 1 1116 1148 1316	3 16 9 52 5 16 11 52 3 8 13 32 7 7 16 15 52 17 52 17 52 9 16	3/16 7/12 1/4 9/32 5/16 11/32 3/8 13/32 7/16 15/32 1/2	$\begin{array}{c} 1\frac{1}{4}\\ 1\frac{7}{16}\\ 1\frac{9}{16}\\ 1\frac{3}{4}\\ 1\frac{7}{8}\\ 2\frac{1}{16}\\ 2\frac{3}{16}\\ 2\frac{3}{16}\\ 2\frac{1}{16}\\ 2\frac{1}{16}\\ 2\frac{1}{16}\\ 2\frac{1}{16}\\ 1\frac{1}{16}\\ \end{array}$	3 16 7 32 1 4 9 32 5 16 11 12 3 8 13 32 15 12 1 5 2	11 37 8 6 15 15 15 15 15 15 15 15 15 15 15 15 15	1 11/8 11/4 13/8 11/2 15/8 13/4 17/8 2 21/8 21/4

Chain drums and sheaves are usually made with a diameter of 20 to 25 times the thickness of the chain iron, the diameter being taken to the center of the chain.

FOR ROPE



Dia. of Rope	A	В	С	D	Dia. of Rope	A	В	С	D
3/8 7/16 1/2 9/16 5/8 11/16	7/16 1/2 9/16 5/8 11/16 3/4	7/82 1/4/9/82 5/66 11/82 3/8	3 52 3 52 1/8 1/8	3 52 1/8 1/8 5/52 5/52 3/16	34 13/16 7/8 15/16 1 1 1/8	13/16 7/8 15/16 1 11/16 13/16	15 x2 1/2 17 x2 19 x2	5 52 5 52 5 52 3 16 3 16 1 4	3/16 7/32 7/32 1/4 1/4 5/16

See also Pulley Grooves for Rope Transmission, pages 129 and 130.

#### HOOKS AND RINGS FOR CHAIN

Round slip hooks should be made from the best hammered iron three times the diameter of the material in the chain. Thus a slip hook for a ¾ inch chain should be of 2¼ inch stock.

Square grab hooks should be made from material twice the diameter of the chain. A grab hook for a  $\frac{3}{4}$  inch chain, use  $\frac{1}{2}$  stock.

Inside diameter of ring should be six times the diameter of the chain iron, and the ring stock twice the size of the chain. A ring for a  $\frac{3}{4}$  inch chain should be made from  $\frac{1}{2}$  inch material and be  $\frac{4}{2}$  inches inside diameter.

#### TREATMENT OF STEEL

Annealing gives the steel a finer grain, and makes it more ductile. Steel castings and anchor chains are frequently annealed to increase their tensile strength and resistance to sudden shocks.

Hardening steel increases its tensile strength and elastic limit, but 'decreases its ductility. Steel is heated to a high temperature and then plunged into oil or water. Cutting tools for lathes, shapers, etc., are hardened.

Case hardening causes the steel to have a hard exterior surface and a soft interior. Gears and armor are case hardened.

Tempering is reheating hardened steel to restore a part of its ductility. Drills, metal working tools, etc., are tempered.

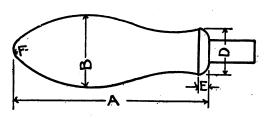
# SECTION VI

### MISCELLANEOUS DETAILS

HANDLES—HAND WHEELS—KNOBS—KNURLED SET—WRENCHES—
STUFFING BOXES—DRILL SHANKS—WASHERS—CLINCH RINGS—
SPRINGS — ANGLE COUPLINGS — KNUCKLE JOINTS — YOKE
ENDS—ROD ENDS—TOOL STRAPS AND BOLTS—TAPER
PINS — FINISHED ENDS OF SHAFTS, STUDS,
SCREWS AND BUSHINGS—STANDARD SQUARES
FOR CHUCK SCREWS AND WRENCHES

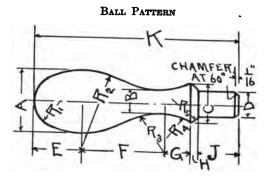
#### MACHINE HANDLES

## CONE PATTERN



A	В	D	E	F	Dia. of Shank
2 2½ 3 3¼ 3½ 3¾	34 1 1 1 1/8 1 3/6 1 15/6 1 3/8	7/66 9/66 5/8 3/4 7/8	1/8 5/82 8/16 1/4 1/4	1/8 5/82 8/6 1/4 5/6 8/8	5 16 3/8 1/2 5/8 11/6 3/4

7/



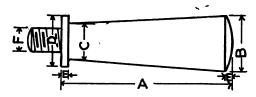
A	В	C	D	E	F	G	н	J	K	Rı	Ra	R3	R4	R
7/16	3/16	5/16	. 252 . 253	3/8	5/8	*	1/2	₹/16	123/22	3/16	E:/64	53,64	%	⅓
5∕8	5/16	3/8	.252	₹/s	49/64	11/64	3/42	7∕16	129/52	%	11/16	11/4	5/8	⅓
<b>¾</b>	3∕8	%	.3145	23/64	55/64	1/4	3/62	7/16	25/2	23/64	53/64	13%	3/8	3/16
13/16	5/16	1/2	.3155	5/8	31/22	5/16	3/62	7/16	27/16	23/64	111/64	27/2	%	³/16
<b>7⁄8</b>	3∕8	%	.3155 .377	5/8	11/16	5∕16	⅓	%6	211/16	13/2	1%	176	19/2	3/16
1	7∕16	11/16	.378 .4395	3/4	11/8	3∕8	⅓	11/16	31/16	1∕16	1%	11/16	5/8	3/16
13/8	7∕16	11/16	.4405	7/8	111/2	13/2	1/8	11/16	37/16	1/2	121/82	11/2	45,64	1/4
13/6	⅓	3/4	.4405 .4395	7/8	13/4	7∕16	5/2	11/16	329/42	%	21/16	27/16	29/12	1/4
134	⅓	7/8	.4405 .503	1	17/8	17/2	1∕42	15/16	4%	%	25/16	221/22	34	5/16
13%	1/2	15/16	.504 .503	1	21/8	3/4	3/16	15/16	5	21/22	225/42	21/2	17/6	5/16
1/2	5/8	11/8	. 504 . 628 . 629	11/8	21/4	1∕8	5/16	13/16	5¾	11/16	221/42	31/2	119/2	%

[Cincinnati Ball Crank Co., Cincinnati, O.]

Handles can be obtained with plain shanks that are riveted over, or with threaded shanks. The latter are preferable as it is not necessary to drill through the part the handle is to operate. Shanks of handles operating wheels or cranks turning right handed should have left hand threads to prevent unscrewing.

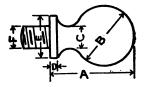
Handles are usually of drop forged steel, and are finished all over.

TAPERED SIDES



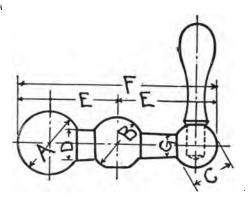
A	В	С	D	E	F
2½	34	1/2	3/4	3/2	3/8
3	1	5/8	7/8	1/8	7/6
3½	11/6	11/6	1	5/22	1/2
4	11/4	1	11/8	3/16	5/8

SPHERICAL END



A	В	С	D	E	F
34 1 138 158 134	5/8 3/4 1 11/4 13/8	1/4	3 122 1/8 1/8 1/8 5/22 3/16	716 1/2 11/16 1 1 1/8	1.4 5.16 3.8 1.2 5.8

BALANCED CRANK



							Smal	l Ball
A	В	С	D	E	F	G	Dia. of Hole	Depth of Hole
1 1 <sup>1</sup> / <sub>8</sub> 1 <sup>1</sup> / <sub>4</sub> 1 <sup>3</sup> / <sub>8</sub> 1 <sup>1</sup> / <sub>2</sub> 1 <sup>5</sup> / <sub>8</sub> 1 <sup>3</sup> / <sub>4</sub> 2	7/8 1 11/8 11/4 15/6 13/8 11/2 113/6	5/8 3/4 13/16 15/16 1 1 11/16 11/4	1/2 1/2 9/16 9/16 11/16 3/4 27/32	1½ 1¾ 2 2¼ 2½ 3 4 5½	3 3½ 4 4½ 5 6 8 11	3/8 3/8 7/16 7/16 1532 1/2 1732 5/8	.25 .3125 .3125 .375 .4375 .4375 .4375	1/2 9/16 9/16 11/16 25/32 25/32 11/32

[Cincinnati Ball Crank Co., Cincinnati, O.]

For handles see Machine Handles.

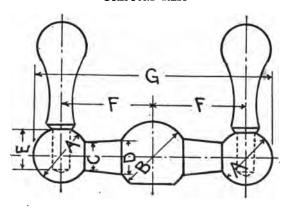
The center ball B may have a flat surface at the top as at the bottom.

The crank can be secured to the part it is to operate in a variety of ways. For instance, the ball B may have a square hole fitting over the end of the operated part, which is squared to suit and finished with a thread at the end. A nut is screwed onto the thread, thus holding the crank in place. Instead of a nut, the end may be riveted over.

Handles shown are screwed on, but by drilling through the balls and countersinking they can be riveted over.

Instead of the crank having a handle screwed or riveted into the ball C, the crank with handle can be made in one piece of drop forged steel.





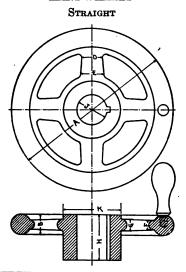
A	В	C	D	E	F	G
5/8 8/4	13 16 11 16	5/16 13/32	3/8 13/32	15/32 9/16	15 16 7 8	$2\frac{1}{2}$ $2\frac{1}{2}$ $3$ $3\frac{1}{2}$
34 7/8 1 <sup>1</sup> / <sub>16</sub> 1 <sup>1</sup> / <sub>16</sub>	$1^{1}_{16}$ $1^{1}_{16}$ $1^{3}_{16}$ $1^{3}_{8}$ $1^{3}_{8}$	5 16 13 3 3 8 13 82 7 16 1 2 1 1 2	8/8 13/32 7/16 17/32 5/8 5/8	15 52 9 16 9 16 9 16 9 16 11 16 25 52	$ \begin{array}{c} 1\frac{1}{8} \\ 1\frac{3}{8} \\ 1\frac{9}{6} \\ 1^{11} \cancel{16} \\ 1^{31} \cancel{32} \end{array} $	3½ 4 4½

[Cincinnati Ball Crank Co., Cincinnati, O.]

For handles see Machine Handles.

Steel cranks and compound rests which come in contact with moisture should be lacquered to prevent rusting.

## HANDWHEELS

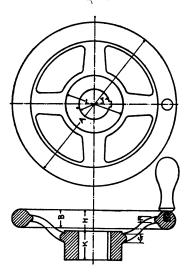


	Rim	Arm						Hub		
Diameter	· Thickness	Width at Small End	Width at Large End	Thickness at Small End	Thickness at Large End	Number of Arms	Length	Bore	Dia.	Size of Keyway
A	В	D	Е	F	G	Ź	н	J `	К	
7 8 9 10 12 14 16 18 20 24	7/8 1 11/8 11/4 11/2 11/2 11/2 15/8 15/8 13/4	7/8 15/16 1 1 13/8 11/2 11/2 15/8 11/2 13/4	1 1½ 1¼ 1¼ 1¼ 1¾ 1¾ 1¾ 1¾ 2 2¼	3/8/6/8/2/8/8/4/4/4/4/4/4/4/4/4/4/4/4/4/4/4/4	1/2/16/5/8/8/7/8/7/8/11/11/11/11/11/11/11/11/11/11/11/11/1	4 4 4 4 4 6 6 6	27/8 2 13/8 31/2 11/2 23/4 21/4 33/4 2 31/8	7/8 13/6 19/3 11/4 11/2 11/2 11/3 8/8 19/6 18/4	21/22/3/4 121/22/3/4 22/3/4 31/22/3/4 31/2/8	3 16 x x x 1 18 16 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

[Niles-Bement-Pond Co., New York.]

For handles see Machine Handles.

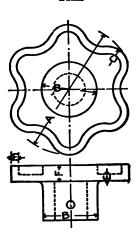
DISHED



	Rim		Arm						Hub	)	
Diameter	Thickness	Width at Small End	Width at Large End	Thickness at Small End	Thickness at Large End	Number of Arms	Dish to Hub Face	Bore	Length	Diameter	Size of Keyway
A	В			F	G	ź₹	н	J	к	L	
9 10 12 13 14½ 18 20 20 20	1½8 1¼ 1½2 1½2 1½2 1½2 158 158 158	1 1 1 <sup>1</sup> / <sub>8</sub> 1 <sup>1</sup> / <sub>4</sub> 1 <sup>1</sup> / <sub>2</sub> 1 <sup>3</sup> / <sub>8</sub> 1 <sup>3</sup> / <sub>8</sub>	11/4 11/4 13/4 13/4 13/4 17/8 13/4 13/4	3/8/8/8/3/1/2/8/4/4/4/4/4/4/4/4/4/4/4/4/4/4/4/4/4/4	5/8 / 5/8 / 8/4 / 3/4   1   1   1   1   1   1   1   1   1	4 4 4 4 5 6 6 6	9/16 1 1 1 3/4 2 1 1/8 2 1/8 2 1/8 2 1/8 2 1/8	1 1/4 1/7 1/8 1 1/7 8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1 1/8 1	2 1 <sup>1</sup> / <sub>2</sub> 1 <sup>1</sup> / <sub>2</sub> 3 2 <sup>5</sup> / <sub>8</sub> 3 <sup>1</sup> / <sub>4</sub> 5 <sup>3</sup> / <sub>8</sub> 2 <sup>1</sup> / <sub>4</sub> 9	21/2/2 21/2 2 1/2 3 1/2/4/4/4/4 3 3 3 3 3 3 3 3 3 3 3 3	14 x 1/8 14 x 1/8 14 x 1/8 14 x 1/8 14 x 1/8 1/2 x 1/4 1/2 x 1/4 1/2 x 3/6 1/2 x 3/6 1

[Niles-Bement-Pond Co., New York.]





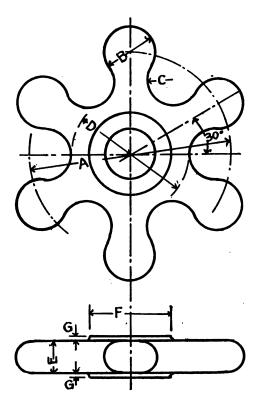
A	В	С	E	F.	
2 2½ 3 3½ 4 5	7/8 1 11/4 13/8 11/2 15/8	5/16 3/8 7/16 1/2 5/8	1/8 1/8 6/2 1/6 1/4	5 16 5 16 3 8 7 16 1 2 2 5 8	Depth of hub to suit work

This wheel is usually of cast iron, and can be connected to the part it is to operate by a cylindrical, square or hexagonal projection to which it is pinned.

The dimension B is dependent on the size of the projection on which the star wheel is to be fitted.

No finish is generally required.

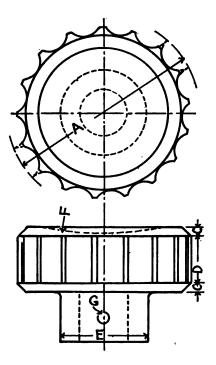
CAPSTAN



A	В	С	D	E	F	G
$\frac{2\frac{1}{2}}{3}$ $\frac{3}{1/2}$	5/8	5 16	1¼	3/8	11/4	1/6
	3/4	3 8	1¾	1/2	11/2	1/6
	15/16	15 82	2	9/16	13/4	8/2

May be keyed on, or fitted on the squared end of operated part.





dia. of rod = d

A = 4 d

C = .2 d

D = d

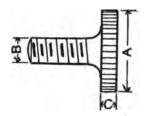
Length of hub to suit work.

E = 1.8 dRadius F = 6 dPin G, ½" dia. for rods ¾" to ½" ¼" dia. for rods ¾" to 1"

To obtain the flutings on the side, divide the circumference of the circle having a diameter equal to 4d into any number of divisions, arbitrarily selected in the present case as 18, and describe arcs which are tangent to each other at the circumference of the circle. As the half circles spaced around will leave sharp points, cut them back so there is a flat face of 1/16" or 3/2".

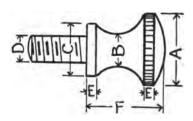
KNURLED SETS

PLAIN KNURLED SET



A	В	С
84	3 16	1/8
7/8	1 4	5/42
11/8	5 16	3/16
11/4	3 8	1/4

## SHOULDER SINGLE KNURLED

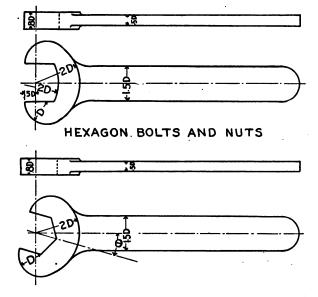


A	В	С	D	E	F
5/8 3/4 7/8 1	5 16 3/8 7/16 1/2	8/8 1/2 5/8 8/4	3/16 1/4 5/16 3/8	3 12 1/8 1/8 5/82	34 7/8 15/16 11/16

#### WRENCHES FOR BOLTS AND NUTS

#### OPEN WRENCH

#### SQUARE BOLTS AND NUTS



D = dia. of bolt

Angle  $\theta = 0$  degs. for machine tool wrenches

= 15 degs. for engineer's wrenches

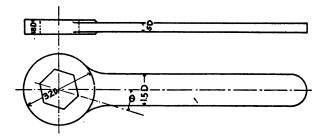
= 22½ degs. for textile machines

Length of wrench = 12 to 16 D.

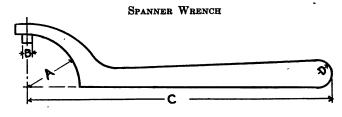
#### Finishes

Unfinished or rough—opening milled, otherwise rough. Semifinished—opening milled, head brightened and case hardened. Finished—opening milled, case hardened and polished all over.

Box Wrench

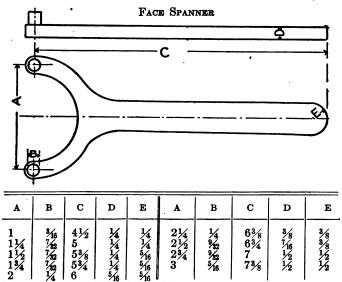


For D,  $\theta$  and length see Open Wrench.



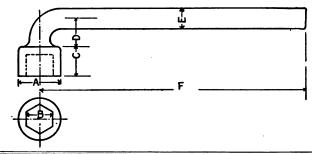
A	В	С	D	Thickness
3/4 7/8 1 11/8 11/4 11/2 15/8 13/4	7,52 15,64 1,4 17,64 9,32 19,64 5,16 21,64	5 5 <sup>1</sup> / <sub>2</sub> 6 6 <sup>1</sup> / <sub>2</sub> 7 7 <sup>1</sup> / <sub>2</sub> 8	3 16 3 16 1 4 5 16 3 8 7 16 1 2 9 16	14 14 5 16 8 8 7 16 7 16 1 12 1 2

The diameter of the holes in the operated part should be  $\frac{1}{14}$  in. greater than the diameter of the pin B.



For diameter of hole, see note, page 239.

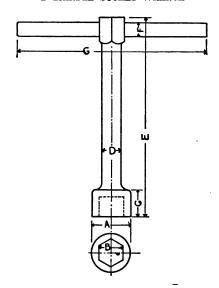
## OFFSET HANDLE SOCKET WRENCH



U. S. Standard Bolt Dia.	A	В	C .	D	E	F
3/8 1/2 5/8 3/4 1/8 1 1/4	11/8 11/4 15/8 17/8 21/8 21/2 21/2 23/4	45,64 57,64 15,64 19,62 115,62 121,62 127,63	11/6 7/8 7/8 1 11/8 11/4 13/8 11/2	11/6 7/8 7/8 1 11/8 11/4 13/8 11/2	1/2 5/8 3/4 7/8 1 11/8 11/8 13/6	6½ 7¾ 9 10 10¾ 11¼ 11½ 12

pth of hole in wrench should be 1/6 in. less than thickness of nut.

T HANDLE SOCKET WRENCH

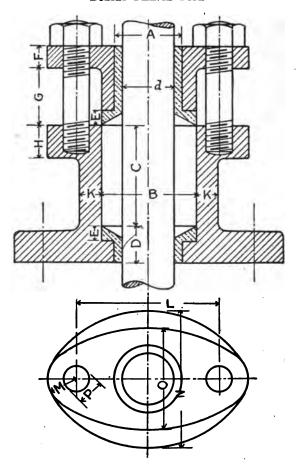


U. S. Standard Bolt Dia.	A	В	С	D	E	F	G
1/4 5/16 3/8 7/16	34 7/8 11/8 13/6	33,64 39,64 45,64 51,64	9/16 5/8 11/16 3/4	3/8 7/16 1/2 9/16	51/4 51/2 53/4 6	1/4 5/16 3/8 7/16	4½ 4⅓ 5 5½ 6
5 (6 (8 (1 (8 (8 (8 (8 (8 (8 (8 (8 (8 (8 (8 (8 (8	1 1/2 1 1/8 1 7/8 2 1/8	15 64 19 62 11 15 64	1 1 1/8	34 7/8	6½ 7½ 8½ 9¼ 10¼	9 16 5 8 5 8 3 4	8 8 8 <sup>3</sup> 4 9 <sup>1</sup> 4
1 1 <sup>1</sup> / <sub>8</sub> 1 <sup>1</sup> / <sub>4</sub> 1 <sup>3</sup> / <sub>8</sub> 1 <sup>1</sup> / <sub>2</sub>	21/2 21/2 23/4 35/6 35/6	$1^{21}\sqrt{2}$ $1^{27}\sqrt{2}$ $2^{1}\sqrt{2}$ $2^{1}\sqrt{2}$ $2^{13}\sqrt{2}$	$ \begin{array}{c} 1  \overset{1}{1} \overset{3}{4} \\ 1  \overset{3}{3} \overset{8}{8} \\ 1  \overset{1}{1} \overset{1}{2} \\ 1  \overset{1}{1} \overset{1}{1} \overset{6}{1} \\ 1  \overset{1}{3} \overset{1}{1} \overset{6}{1} \\ \end{array} $	1 1/8 1 1/8 1 3/6 1 3/8 1 3/8	10¼ 10¾ 10¾ 11¼ 11¼ 12¼	3,4 7,8 7,8 1 1,1,6 1,1,6	91/2 91/2 10 11 11

Hexagon head for pin same size as bolt head. For depth of hole, see note, page 240.

# STUFFING BOXES

# BOLTED FLANGE TYPE



d = dia. of rod			
A = 1.31 d	•	H = .63 d	
B = 1.8 d		K = .44 d	
C = 2. d	•	L = 2.8 d	
D = .7 d		M = .56 d	
E = .31 d		N = 2.75 d	
F = .44 d		O = 2. d	
G = 1.13 d	For r	ods ½" to ½" d	ia. of stud $P = \frac{3}{8}$ "
	66	" ¾""1¼"	" " " = ½"
	"	" 18/8" " 15/8"	""""= 5/8"
	"	" 1¾" " 2⅓"	··· ·· · · · · · = 3/4"
	u	" 2¼" " 2½"	

The top gland may be of composition instead of cast iron lined with composition. For large rods the gland in contact with the rod is reduced in length to cut down friction.

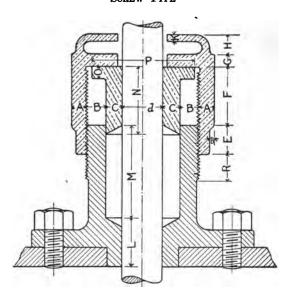
Studs of steel or bronze with steel nuts. Bronze studs with steel or composition nuts should be fitted where there is excessive moisture. Hole in gland for stud  $\frac{1}{16}$  in. larger than stud.

The part K may be cast on the engine cylinder or on the valve body, thus doing away with bolts.

It is important that the gland stud nuts be equally tightened so the pressure on the rod is the same at all points in its circumference. If the rod is well oiled the friction may be considerably reduced.

For low steam pressures hemp and cotton packings are suitable, but for high, metallic should be used.

SCREW TYPE

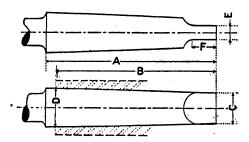


d = dia. of rod

A = .34 d	L = 1.5 d
B = .52 d	M = 2. d
C = .43 d	N = 2.37 d
E = .75 d	O = .31 d
F = 1.4 d	P = 2.62 d
G = .31 d	R = d
H = .5 d	Gland of composition
K - 15 d	

The screw type is for smaller rods than the bolted flange and also for installations where the studs would be in the way. The gland is screwed down by using a wrench on the part A, which can be made with 6 or 8 notches or ribs in its circumference.

# TAPERED DRILL SHANKS



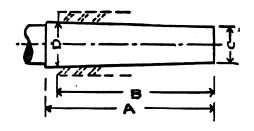
# Morse Twist Drill & Mach. Co.

No.	A	В	С	D	Е	F	Taper in 12-Inch
0	2 <sup>11</sup> 32	$2^{7}_{32}$ $2^{3}_{8}$ $2^{7}_{8}$ $3^{9}_{16}$ $4^{1}_{2}$ $5^{3}_{4}$ $8$	.240	.356	5 32	9,82	. 625
1	2 <sup>9</sup> 16		.356	.475	13 64	3,8	• 600
2	3 <sup>1</sup> 16		.556	.700	1 4	7,16	. 602
3	3 <sup>3</sup> 4		.759	.938	5 16	9,16	. 602
4	4 <sup>3</sup> 4		.997	1.231	15 32	5,8	. 623
5	6		1.446	1.748	5 8	3,4	. 630
6	8 <sup>5</sup> 16		2:077	2.494	3 4	1,1/8	. 626

# Brown & Sharpe

No.	A	В	C	D	E	F	Taper in 12-Inch
4 5 6 6 7 7 8 9 9 10 10 10 11 11	1344 $2932$ $23132$ $32732$ $358$ $458$ $434$ $434$ $516$ $634$ $794$ $713$ $689$ $22$	121 522 23 66 27 8 33 4 317 52 4 1 7 8 4 7 8 6 13 52 6 15 16 7 15 52 7 15 16	.333 .432 .479 .479 .578 .578 .727 .874 .1.022 1.022 1.022 1.220 1.466	. 402 . 523 . 599 . 635 . 725 . 767 . 898 1.067 1.277 1.260 1.289 1.312 1.531	7 12 4 52 52 6 6 5 5 16 5 5 7 16 7 7 16 7 7 7 16 7 7 7 16 7 7 7 16 7 7 7 16 7 7 7 16 7 7 7 16 7 7 7 16 7 7 7 16 7 7 7 16 7 7 7 7	11 32 3/8 7/16 7/16 15/32 15/32 1/2 9/16 21/32 21/32 21/32 21/32 3/4	.500 .500 .500 .500 .500 .500 .500 .500

# Jarno



$$D = Dia.$$
 of large end  $= \frac{No. \text{ of taper}}{8}$ 

$$C = Dia. of small end = \frac{No. of taper}{10}$$

$$B = Length of taper = \frac{No. of taper}{2}$$

No.	A	В.	C	D	Taper in 12 Inches
2	1½ 1½ 1½	1	.20	. 250	. 600
3	15/8	1½	.30	.375	.600
4	$2\frac{3}{16}$	2	.40	. 500	.600
2 3 4 5 6 7 8 9	211/16	2 <sup>1</sup> / <sub>2</sub> 2 <sup>1</sup> / <sub>2</sub> 3 3 <sup>1</sup> / <sub>2</sub>	.50	.625	. 600
6	33/16	3	.60	.750	. 600
7	3 <sup>1</sup> 1∕1a	3½	.70	.875	. 600
8	43/16	1 4	.80	1.000	.600
9	411/16	4½ 5 5½ 6	.90	1.125	.600
10	51/4	5	1.00	1.250	.600
11	534	$5\frac{1}{2}$	1.10	1.375	.600
12	61/4	6	1.20	1.500	.600
13	63/4	6½ 7	1.30	1.625	.600
14	71/4	7	1.40	1.750	.600
15	73/4 .	7½	1.50	1.875	.600
16	85/16	8	1.60	2.000	.600
17	813/4	81/2	1.70	2.125	.600∖
18	95/16	7½ 8 8½ 9	1.80	2.250	.600
19	91% (a	9½	1.90	2:375	.600
20	105/16	10	2.00	2.500	.600

WASHERS

# CIRCULAR PLATE IN EFFECT JAN. 20, 1910 U. S. Standard

Diamatan	Cif YI-1-	Thiel	eness.	Size of Bolt	Number in	
Diameter	Size of Hole	Wire Gauge	Ins.	Size of Boit	100 Lbs.	
916 94 78 11 12 13 13 2 2 14 2 2 2 14	14 516 88 716 172 916 11,16 13,16 15,16	18 16 16 14 • 14 12 12 10 9 8	.05 .06 .06 .08 .08 .11 .11 .14 .16 .17	8 1 4 16 0 16 17 16 0 14 18 17 18 18 18 18 18 18 18 18 18 18 18 18 18	39,400 15,600 11,250 6,800 4,300 2,600 2,250 1,300 900 782 568	
2½ 23/4 3 1/4 3 3/4 4 1/4 4 1/2	176 114 138 1158 134 178 2	9 8 8 8 7 7 7 7 7	.17 .17 .18 .18 .18 .18 .18	1 11/8 11/4 13/6 11/2 15/8 13/4 17/8	568 473 364 275 256 220 197 174 160	

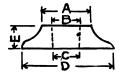
## SQUARE PLATE

Inches Square	Size of Hole, Inches	Thickness, Inches	Thickness Decimal Parts of an Inch	Size of Bolt, Inches	Average Number in 100 Lbs.
1 1/2 1 3/4 2 1/4 2 1/2 3 3 1/2 4 1/2 5	7/6 1/2 9/6 28/5/2 27/5/2 31/2 13/2 11/4 11/4	1/8/8/8/8/8/8/8/8/8/8/8/8/8/8/8/8/8/8/8	.125 .125 .1875 .25 .25 .25 .375 .375 .375	\$ 8 746 146 146 146 146 146 146 146 146 146 1	1,300 1,100 500 315 250 165 87 65 48 40
$\frac{6}{6}\frac{1}{2}$	$1\frac{5}{8}$ $1\frac{7}{8}$ $2\frac{1}{8}$	3/8 3/8 3/8 3/8	.375 .375 .375	11/2 13/4 2	28 24 21

# PLANER HEAD BOLT WASHERS

Dia. of bolt	17/18	9/16 17/16 1/16	5/8 1 <sup>1</sup> / <sub>2</sub> 1/6	11/16 19/16 1/16	1 <sup>3</sup> / <sub>16</sub> 9/ <sub>12</sub>
•				i	

# O. G. CAST IRON WASHERS

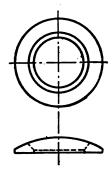


Dia. of Bolt, Inches	A	В	С	D	Е	Approximate Weight Each
3/8/2/8/4/7/8 11/8/4 11/8/4 11/8/4 11/8/4	1 15/8 2 2 21/2 21/2 21/2 31/2 31/4	1/2 11/16 13/16 15/16 11/16 13/16 11/16 15/16 17/16 11/16	7/65 5/8 3/4 7/8 1 11/8 11/4 11/2 15/8	114 212 3 3 3 312 4 412 514 6	7/66 1/2 5/8 8/4 7/8 1 11/8 11/4 11/4	2½ oz. 7 oz. 12 oz. 1 lb. 1 lb. 6 oz. 2 lb. 2 lb. 6 oz. 4 lb. 4 oz. 4 lb. 4 oz. 6 lb.

# Washers for Screws

Dia. of Screw	Dia. of Washer	Thickness
1/8 8/6/4 6/6/8/8 8/8 1/2/6	11, 6 13, 16 15, 16 1 1, 16 1 3, 16 1 7, 16 1 11, 16 1 15, 16 23, 16	5316141618787515215

CLINCH RINGS
COUNTER SUNK OR RECESSED HOLE



Size of	Outside	Thick-	Number	Size of	Outside	Thick-	Number
Hole,	dia.,	ness	in one	Hole,	dia.,	ness	in one
Ins.	Ins.	Ins.	Lb.	Ins.	Ins.	Ins.	Lb.
1/2 5/8 8/4 7/8	13/8 11/2 15/8 13/4	3/6 7/32 7/32 7/32	18 15 11 10	1 1½ 1¼ 1¼ 1¾	2½ 2½ 2¾ 2½ 2½ 2½ 2½	9 32 5 16 5 16 7 16	5 3 <sup>3</sup> ⁄ <sub>4</sub> 2 <sup>3</sup> ⁄ <sub>4</sub> 2 <sup>1</sup> ⁄ <sub>4</sub>

## STRAIGHT HOLE

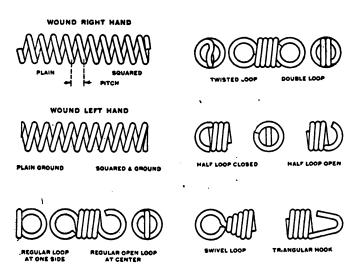
Size of	Outside	Thickness	Size of Hole	Outside	Thickness
Hole, Ins.	Dia., Ins.	Ins.	Ins.	Dia., Ins.	Ins.
5 (6 3/8 7 (6 1/2 5/8	34 15/6 1 11/16 17/16	1/8 5/32 5/32 8/16 7/32	3/4 7/8 1 11/4 13/8	19/16 2 2 2 29/16 27/8	7,52 7,52 9,52 5,16 7,16

#### **SPRINGS**

In general a helical compression spring will give the best results if its outside diameter equals eight times the diameter of the wire. In designing compression springs with squared ends, two inactive coils should be allowed for squaring.

250

The load a spring will sustain can be increased by increasing the diameter of the wire, diminishing the number of coils or decreasing the outside diameter.



Torsion springs should be so designed that their action will be in the direction that tends to reduce the diameter of the spring.

#### SPECIFICATIONS FOR ORDERING SPRINGS

#### Compression Type

Material.

Size of wire.

Inside diameter if spring works on a rod. " in "hole.

Outside

Free length. Pitch, or number of coils.

Style of ends, whether plain, squared only, ground only or squared and ground.

Distance to be compressed and with what weight or power.

## Extension Type

Material.

Size of wire.

Outside diameter.

Length of coils in inches, or number of coils.

Length over all.

Style of ends, whether loop or hook, parallel or at right angles.

Distance to be extended and with what weight or power.

W. Barnes Co., Bristol, Conn.!

#### SPRING FORMULÆ

P = safe load in lbs. r = mean radius of coil E = modulus of elasticity d = dia. of coil wire G = modulus of torsion l = length of spring s = safe shearing stress in lbs. per sq. in. <math>n = number of coils f = deflection of spring in ins. for  $\sigma = 3.1416$ 

SPRING IN COMPRESSION OR TENSION WHEN LOADED AXIALLY

Cylindrical helical spring, circular cross section.  $P = \frac{8\pi d^3}{16r}$ ;  $f = \frac{32 \text{ Plr}^2}{\pi d^4 G} = \frac{64 \text{ Pnr}^3}{d^4 G}$ .

 $\pi d^4G$   $d^4G$ Rectangular cross section, t = thickness, w = width

 $P = \frac{st^2w^2}{3r\sqrt{t^2+w^2}}; \; f = \frac{3\; Pr^2l\; (t^2+w^2)}{Gt^3w^3}.$ 

#### SPRING SUBJECT TO BENDING

Rectangular plate  $P = \frac{St^2w}{6l}$ ;  $f = \frac{Pl^8}{Et^3w}$ .

Triangular plate  $P = \frac{St^2w}{6l}$ ;  $f = \frac{6 Pl^3}{Et^3w}$ 

Compound (leaf or laminated) triangular plates. k = number of plates.  $P = \frac{Skt^2w}{6l}$ ;  $f = \frac{6}{Ekt^3w}$ .

#### TABLE FOR DETERMINING CAPACITIES

D = Outside Diam. of Spring. W = Safe Load Note-To find values for square wire multiply the

Size of Wire   D   .250   .3125   .375   .4375   .500   .5625   .625   .750	.875	1.000	1.125	1.250
	.11	.098	1.120	1.200
			l .	1
.016   F   .1302   .302   .470   .760   1.150   1.66   2.30   4.02	6.95	9.42		1
#24   W   1.18   .92   .76   .45   .56   .50   .45   .37	.31	.28	.24	ľ
.0225   F   .0278   .0631   .1135   .1857   .282   .408   .569   .975	1.66	2.42	3.46	1
#22 W 2.35 1.84 1.49 1.26 1.095 .96 .865 .715	.61	.53	.47	1
#22 W 2.35 1.84 1.49 1.26 1.095 96 865 715 028 F 0119 0250 0453 0742 1140 165 231 408	.660	.995		1
.028 F .0119 .0200 .0493 .0742 .1140 .103 .231 .408			1.42	1
#20   W   4.70   3.64   2.97   2.5   2.18   1.92   1.72   1.42	1.20	1.05	.93	.84
.035 • F  .00451 .00952 .0175 .0290 .0447 .0651 .0914 .163	.264	.400	.575	.792
#19 W 7.87 6.05 4.93 4.15 3.58 3.16 2.82 2.32	1.97	1.74	1.54	1.34
.041 F   .00234   .0047   .0088   .0106   .0228   .0334   .0410   .0842	1370	.208	.305	.430
.041 F .00234 .0047 .0088 .0106 .0228 .0334 .0410 .0842 #18 W 12.05 9.2 7.40 6.57 5.4 4.75 4.23 3.48				
#18   W   12.05   9.2   7.40   6.57   5.4   4.75   4.23   3.48	2.95	2.85	2.27	2.02
.047 F   .00115   .00294   .00488   .00824   .0132   .0187   .0264   .0396	.0785	. 126	.175	.242
#17 W 18.9 14.3 11.5 9.67 8.3 7.3 6.47 5.32 054 F .00059 .00138 .00256 .0044 .00702 .0103 .0145 .0267	4.5	3.91	3.45	3.1
.054 F  .00059 .00138 .00256 .0044 .00702 .0103 .0145 .0267	.0437	.067	.0971	.1502
#16 W 31.5 23.61 18.8 15.7 13.8 11.8 10.5 8.57	7.25	6.28	5.04	4.96
710 17 91.0 20.01 10.0 10.1 10.0 11.0 10.0 0.01	0000		0.02	
.063 F   .00026   .00085   .00122   .00222   .0051   .0053   .00704   .0129	.0233	.0327	.0476	.066
#15   W     29   24.1   20.5   17.9   15.85   12.92	10.9	9.46	8.35	7.45
.072   F      .00066 .0012  .0018  .0029  .00404 .0074	.0124	.0189	.0279	.039
#14 W 41 33.5 28.8 24.9 22.2 18.1	15.2	13.15	11.6	10.35
.080 F   .00041 .00074 .00128 .00203 .0034 .0057	.0082	.0127	.0186	.026
.000 F .00041 .00074 .00205 .00205 .0007	.0002		.0100	
#13 W   45.7 40.7 35 28.4	23.8	20.3	17.75	16.15
.092 F      .00063 .00085 .0014  .0026	3 .0045	.0072	.01035	.0148
#12 W   52.5   42.2	35.4	30.4	26 74	23.8
.105 F   .00069 .0014		.0039	.0058	.0083
			40.51	
	54	46		36
.120   F	.0013		.00326	
#10   W	77	67	58.6	52
.135   F	.00081	.00135	0019	.0027
# 9   W	105	90	78	69
.148 F		.00035	00100	
	1.00000		.00128	
• # 8   W	1	120	104	98
.162   F	1	1.00057	.00087	.0012
# 7   W	1	159	138	122
.177   F	1			.00083
#6   W	1	1.00000		158
	Į.			100
.192 F	1	1	I	.00057
#5   W	1	1	i	ł
.203 F	1	1	ı	1
#4 W .	1	1	ĺ	Į
.225   F	1	1	1	1
	1	1	l	ì
	1	1	ĺ	1
.244   F   -		i	1	1
# 2   W   T	1	1	I	1
.263 F	1		I	1
#1 W	1		I	1
	1		I	1
.283 F	1		Ι.	1
#0   W	1		1	I
.307   F	1	l	1	1
#00   W	1	1	1	1
.331 F	1	1	l	i
	1		1	1
#000   W	1		1	1
.362   F				

ILLUSTRATION OF THE USE

Required a spring ½" O. D. that will give a resistance of 42 lbs. when compressed to a length of 3".

1. What size of wire is required?

2. What will be the uncompressed length of the spring?

3. How many coils?

In the table we follow the horizontal colors.

3. Now many colls:
In the table we follow the horisontal column, giving the values of D, until we come to the vertical column captioned .500 (1/2" O. D.)

Searching down this column we find 45.7 lbs. as the nearest W. (safe load) value to the 42 lbs. required.

Glancing from this point toward the left we find the size wire to be .092" and the F Value (deflection of one

1 under one lb.) to be .00063.

Ve therefore have .00063 x 42 equal to .026 + as the deflection of one coil under a load of 42 lbs.

#### FOR ROUND WIRE HELICAL SPRINGS

in Lbs. F = Deflection of One Coil per One Lb. given safe load by 1.2 and the given deflection by .59.

1.375  1.500  1.750  2.00  2	2.25  2.50  2.75  3	.00 3.25 3.50 3.75	4.00  4.50  5.00
.0354   .0548   .0757   .116   .0114   .01197   .0266   .0425   .0658   .0124   .0124   .0149   .0245   .0374   .0124   .0149   .0245   .0374   .0024   .0344   .0244   .0244   .0244   .0244   .0244   .0344   .0344   .0344   .0346   .0044   .0346   .0346   .0034   .0346   .0046   .0046   .0046   .0046   .0055   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057   .0057	24   22   2   2   2   2   2   2   2	777   18	44 .0266 53 .0222 .0298 71 .013 .0202 .0208 88 80 .022 .0086 .0116 .020 .015 .0072 .0106 .0148 .027 .0106 .0148 .027 .0106 .0148 .027 .0106 .0148 .027 .0106 .0148 .028 .029 .028 .038 .049 .049 .053 .007 .0106 .0149 .020 .028 .038 .049 .049 .053 .007 .0106 .0148 .020 .028 .038 .048 .048 .053 .007 .0106 .0148 .020 .028 .038 .038 .048 .048 .053 .007 .0053 .007 .0053 .007 .0055 .007 .0055 .007 .0055 .007 .0055 .007 .0055 .007 .0055 .007 .0055 .007 .0055 .007 .0055 .007 .0055 .007 .0055 .007 .0055 .007 .0055 .007 .0055 .007 .0055 .007 .0055 .007 .0055 .007 .0055 .007 .0055 .007 .0055 .007 .0056 .007 .0056 .007 .0056 .007 .0056 .007 .0056 .007 .0056 .007 .0056 .007 .0056 .007 .0056 .007 .0056 .007 .0056 .007 .0056 .007 .0056 .007 .0056 .007 .0056 .007 .0056 .007 .0056 .007 .0056 .0056 .0056 .0057 .0056 .0057 .0056 .0057 .0056 .0057 .0056 .0057 .0056 .0057 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .0056 .00

#### OF THE ABOVE TABLE

Assuming that the spring is not to be at its solid height when compressed to the specified 3" we have 3" divided by .092 equal to 32.6 coils as the number in the solid height or 30 coils as a desirable number for the

There being 28 free coils in a spring containing 30 coils we have 28 multiplied by .026 equal to .728 as the total deflection of the spring when resisting a load of 42 lbs.

We have then: .092 as the size wire required 3" + .728 = 3.728 as the free length.

Thirty as the number

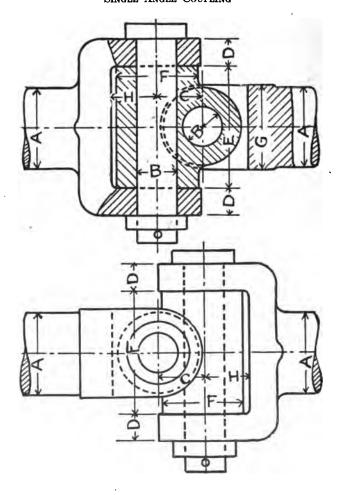
Note: The above tables are not guaranteed to be absolutely correct, as allowances have to be made for various grades of material. They will, however, be a good working basis for general estimating and experimental purposes.

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# ANGLE COUPLINGS

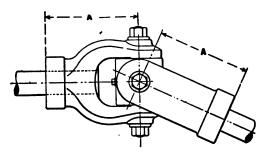
(Universal Joints)

SINGLE ANGLE COUPLING



A = d = dia. of shaft	E = 1.5 d
B = .5 d	F = d
C = .56 d	G = 1.1 d
D = .32 d	$\mathbf{H} = .56  \mathbf{d}$

#### SINGLE ANGLE COUPLING



Will work to an angle of 25 degs.

Dia. of Shaft	A	Dia. of Shaft	A	Dia. of Shaft	A
Inches	Inches	Inches	Inches	Inches	Inches
15/16 13/16 17/16 111/16 115/16	3½ 4½ 6¼ 6¼ 8	28/6 27/6 211/6 215/6 37/6	8 10 10 11 <sup>1</sup> / <sub>2</sub> 11 <sup>1</sup> / <sub>2</sub>	3 <sup>15</sup> /6 4 <sup>7</sup> /6 4 <sup>18</sup> /6	14 16 20

[A. & F. Brown, Elizabeth, N. J.]

With single angle couplings the angular velocity is variable and is dependent on the angle of inclination of the shafts. The variation is of little consequence except where extreme accuracy is required as in time recording machines.

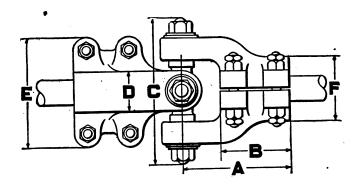
The joint shown is often installed in line shafts of motor boats and in shafts from engine to driving gear on the rear axle of automobiles.

The shafts in coupling on page 255 are keyed or pinned in, while those on page 256 are keyed and the parts held together by bolts.

Angle couplings are sometimes called Hooke's joints.

The type shown on page 254 is more frequently used where the angle between the shafts is large.

# SINGLE ANGLE COUPLING

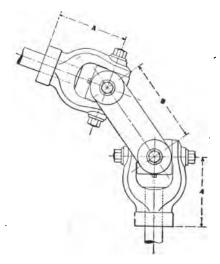


Will work to an angle of 25 degs.

Dia. of Shaft	A	В	С	D	E	F	Standard Keyway
13/6 $17/6$ $111/6$ $111/6$ $23/6$ $21/6$ $21/6$ $215/6$ $33/6$ $37/6$ $316/6$ $47/6$ $416/6$	8½ 9 98¼ 10 11 12 12½ 13½ 14¼ 15½ 16½ 17¾	41/4 41/2 5 6 61/2 7 71/2 81/4 8/4 9 10 10 <sup>3</sup> /4 11 <sup>1</sup> / <sub>2</sub>	7½ 7¾ 8½ 10 10¾ 11½ 12¼ 13 14½ 16 18 20 22	2 1/4 2 2 1/4 3 3 4 4 4 3 4 5 5 1/2 6 6 1/2	41/2 51/2 7 71/2 73/4 83/4 10/4 10/2 11/2 12/2 13/2	3 1/4 3 1/2 4 8/4 5 3/4 6 6 3/4 7 1/2 8 1/2 9 1/4 10	7 32 5 16 7 16 7 16 9 16 9 16 11 16 11 16 13 16 13 16

[Cresson-Morris Co., Phila., Pa.]

Double Angle Coupling

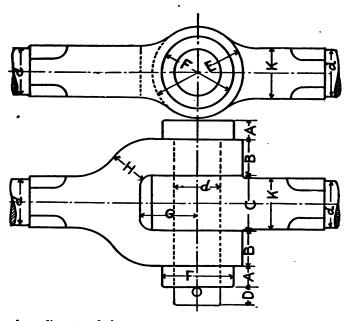


Will work to an angle of 70 degs.

Dia. of Shaft Ins.	A Ins.	B Ins.	Dia. of Shaft Ins.	A Ins.	B Ins.	Dia. of Shaft Ins.	A Ins.	B Ins.
15 16 13 16 17 16 111 16 115 16	3½ 4½ 6¼ 8 8	4 <sup>3</sup> / <sub>4</sub> 5 <sup>1</sup> / <sub>2</sub> 8 <sup>1</sup> / <sub>4</sub> 8 <sup>1</sup> / <sub>4</sub> 10	$\begin{array}{c} 2^{3}/_{16} \\ 2^{7}/_{16} \\ 2^{11}/_{16} \\ 2^{15}/_{16} \\ 3^{7}/_{16} \end{array}$	8 10 10 11 <sup>1</sup> / <sub>2</sub> 11 <sup>1</sup> / <sub>2</sub>	10 12 <sup>8</sup> / <sub>4</sub> 12 <sup>8</sup> / <sub>4</sub> 14 <sup>1</sup> / <sub>2</sub> 14 <sup>1</sup> / <sub>2</sub>	3 <sup>15</sup> / <sub>16</sub> 4 <sup>7</sup> / <sub>16</sub> 4 <sup>15</sup> / <sub>16</sub>	14 16 20	17½ 20 24

The variation in angular velocity is overcome by two single angle joints connecting two parallel shafts through an intermediate shaft.

# KNUCKLE JOINTS



d = diameter of pin	
A = .43 d	$\mathbf{F} = 1.5  \mathbf{d}$
B = .75 d	G = 1.25 d
C = 1.25 d	H = .9 d
D = .43 d	K = 1.1 d
Tr = 1.02 d	

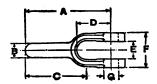
Diameter of head of pin same as washer F.

For tables of yoke and rod ends for forming knuckle joints see pages 259-261.

#### YOKE ENDS

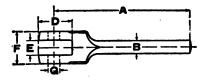
Dimensions of yoke and rod ends given in the following tables are of steel, drop forged. The dimensions can be followed in making castings of iron and composition, but neither will be equivalent to steel in strength.

PLAIN
SOCIETY OF AUTOMOTIVE ENGINEERS' STANDARD



A	В	C	D	E	F	G
1¼ 1¾ 2 2½ 2¼ 2¼ 2½	3/6 1/4 5/6 3/8 7/5 1/2	78 114 138 176 112 158	7/6 5/8 3/4 27/32 1 1 1/8	3/6 9/22 11/32 7/16 1/2 9/16	7/6 5/8 3/4 7/8 1 11/8	3 16 14 5 16 3 8 7 16 1 2

## BILLINGS AND SPENCER STANDARD

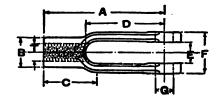


(See next page for table.)

BILLINGS AND SPENCER STANDARD

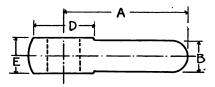
A	В	D	E	F	G
4½ 4¾	1/4 5/6	25 32 15 16	5/16 3/8	3/4 7/8	5/16 5/16
4½ 4¾ 5 5¼ 5½ 5¾ 6¼	3/8 7/16	$1^{1}_{16}$ $1^{5}_{32}$	7/16 1/2 9/16 5/	11/8	5 16 5 16 3 8 7 16
$   \begin{array}{c}     5 \% \\     5 \% \\     6 \% \\   \end{array} $	72 916 5/8 3/4	11/16 15/32 15/16 17/16 1.5/8 1.15/8 2.17/32 2.17/32 2.29/32 3.7/32	38	11/8 11/4 13/8 15/8 17/8 28/16 21/2 213/16 31/8	72 9/16 5/8 3/4 7/8
7	3/4 7/8	1 <sup>15</sup> / <sub>16</sub> 2 <sup>7</sup> / <sub>32</sub> 2 <sup>17</sup> / <sub>4</sub>	7/8 1 1 1/4	$\begin{array}{c c} 1\frac{7}{8} \\ 2\frac{3}{16} \\ 2\frac{1}{2} \end{array}$	3/4 1/8
73/4 81/2 91/4 10	. 1½ 1¼	2 <sup>29</sup> / <sub>32</sub> 3 <sup>7</sup> / <sub>32</sub>	$   \begin{array}{c}     1\frac{1}{8} \\     1\frac{1}{4} \\     1\frac{3}{8}   \end{array} $	$2^{13}_{16}$ $3^{1}_{8}$	1½ 1¼ 1¼

Adjustable
Society of Automotive Engineers' Standard



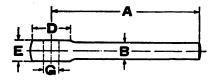
								T
A	В	С	D	E	F	G	Dia.	S. A. E. threads per inch
2 2½ 2½ 2½ 2½ 3	7/16 1/2 5/8 23/52 13/16	7/8 1 11/8 11/4 13/8	1 1/4 17/16 15/8 1 7/8 1 7/8	9/82 11/82 7/16 1/2 9/16	5/8 3/4 7/8 1 11/8	1/4 5/16 3/8 7/16 1/2	1/4 5/16 3/8 7/16 1/2	28 24 24 20 20

ROD ENDS
SOCIETY OF AUTOMOTIVE ENGINEERS' STANDARD



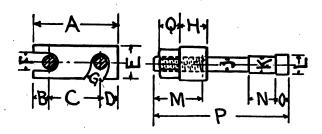
A	В	D	E	Dia. of Hole
11/4 11/4 13/8 11/2 11/2 13/4	3 16 14 5 16 3 8 7 16 1 2	3/8 1/2 19/2 11/16 13/16	3 16 9 82 11 82 7 16 1 / 2 9 16	316 14 516 38 716 12

## BILLINGS AND SPENCER STANDARD

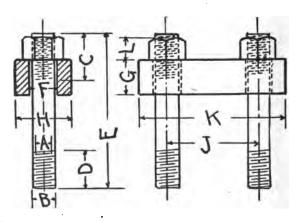


A	. В	D	E	G
315/16	. 1/4	11/16	5/16	5/16
3 <sup>15</sup> / <sub>16</sub> 4 <sup>1</sup> / <sub>16</sub> 4 <sup>1</sup> / <sub>4</sub>	3/8	13 16 7/8	8/8 7/16	3/8
4/16 45/8	16 1/2	1 1½	9/16	716 1/2
4 <sup>18</sup> / <sub>16</sub> 5 <sup>3</sup> / <sub>16</sub>	9/16 5/8	1½ 1¼ 1½ 1¾	5/8 3/4	9/16 5/8
45/6 45/6 413/6 53/6 53/6 61/2 71/52 79/6	3/4 7/8		1 7/8	3/4 7/8
$\frac{6\frac{1}{2}}{7\frac{1}{32}}$	1 11/8	21/4 29/16 27/8	1½ 1¼	1 11/8
$7\frac{9}{16}$	1½ 1¼	27/8	13/8	1½ 1¼

# TOOL STRAPS AND BOLTS



Strap					Bolt				Nut						
A	В	c-	D	E	F	G	н	J	K	L	M	N	0	P	Q
5 6 6 7 71/2 81/4	1 1 11/4 11/8 13/6 15/6 11/4	3 3 1/2 3 3/4 4 5/8 4 5/8 4 5/8 4 5/8	1 1 1 1/4 1 1/8 1 1/6 1 1/4	184 112 184 218 218 218 218 218	13 16 13 16 15 16 11 16 13 16 13 16 15 16	13 16 13 16 15 16 1 16 1 3 16 1 3 16 1 5 16	11/2 11/2 18/4 21/8 21/8 21/8 21/8 21/8	\$4 34 7/8 1 11/8 11/8	18 16 18 16 15 16 11 16 11 16 1 14 1 15 16	11/16 1 18/16 19/16 111/16 113/16	21/2 41/4 48/4 415/6 51/4	113 43 131 43 21 16 21 16 29 16 28 4 35 16	18/16 3/8 28/12 3/4 3/4 3/4	7½ 7½ 8½ 8¾ 95% 10¾ 12 2	11/4 11/4 11/4 15/6 18/4 15/4



For dimensions see page 263.

Bolt					Strap				Nut	
B dia. of bolt	A dia. at root ef thread	С	D	E	F	G	н	J	К	L
3/4 1 11/8 11/8 11/4 11/4 13/4	. 620 . 838 . 939 . 939 1 . 064 1 . 064 1 . 490	2½8 3 2¾4 5½ 5 3½ 5	11/4 18/4 17/8 2 21/2 18/4 21/2	6¼ 8½ 9½ 10¼ 10¼ 12 9¼ 13	7/8 11/8 11/4 11/4 13/8 13/8 17/8	1½ 2 2½ 2½ 2½ 2½ 2½ 3¼	1½ 2 2½ 2½ 2½ 2½ 2½ 3¼	4 6 5½ 6 8 5½ 10½	7 9 9 <sup>3</sup> ⁄ <sub>4</sub> 10 <sup>3</sup> ⁄ <sub>4</sub> 14 10 18	1 1/4 15/8 13/4 13/4 2 2 2 1/2

[Niles-Bement-Pond Co., New York.]

#### MATERIALS OF MACHINE PARTS

Cast Iron—weak in tension and strong in compression. Tensile strength 22,500 lbs. per sq. in., compression 90,000. Weight per cu. ft. 449 lbs.

Malleable Iron—cast iron heated in retorts with an oxide of iron. Malleable iron has a tough outside surface like wrought iron and an interior like cast iron. 'Pipe fittings often made of it. Tensile strength 37,000 lbs.

Wrought Iron—tough, ductile, weldable but cannot be tempered. Tensile strength 50,000 lbs., compression 55,000. Weight per cu. ft. 485 lbs.

Composition or Brass—copper 65.3%, zinc 32.7%, lead 2%. The lead content makes a soft brass that can be readily machined. Navy brass 62% copper, 36 to 37% zinc, 1 to 1½% tin. Weight per cu. ft. 505 lbs.

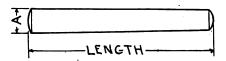
Cast Steel—has a lower carbon content than cast iron, and is used for parts which would be too weak if made of iron. Tensile strength 60,000 lbs. Weight per cu. ft. 490 lbs.

Bronze—as ordinarily understood is an alloy of copper and tin, varying from 8 to 25% of tin. Other metals may be added as phosphorus, making an alloy known as phosphor bronze containing 82.2% copper, 12.95% tin, 4.28% lead and .52% phosphorus. This bronze has a tensile strength of about 50,000 lbs. Weight per cu. ft. 508 lbs.

## TAPER PINS

The pins should force the parts together, and in proper relation to each other when driven home, thus preventing the pins from working loose. They are made of steel and finished all over.

PLAIN



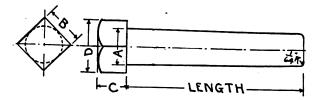
A	Approximate Equivalent	A	Approximate Equivalent
.156 .172 .193 .219 .250 .289	5 ½2 11,64 3 ¼6 7,62 1,4 19,64	.341 .409 .492 .591 706	11/62 13/52 1/2 1/2 19/33 45/64

Taper 1/4" in 12".

Lengths  $\frac{5}{8}$ ", 1" to  $5\frac{3}{4}$ " advancing by  $\frac{1}{4}$ ".

[Cincinnati Bickford Tool Co., Cincinnati, O.]

#### SQUARE HEAD



For dimensions see page 265.

. <b>A</b>	Approximate Equivalent	В	С	D
. 156 . 172 . 193 . 219 . 250 . 289 . 341 . 409 . 492 . 591 . 706	5 /2 11 /6/4 2 /6 7 /6 1 /4 10 /6 11 /2 13 /2 1 /2 2 /2 4 /6 1 /2 2 /6 1 /6 1 /6 1 /6 1 /6 1 /6 1 /6 1 /6 1	14 14 14 14 14 14 14 14 14 14 14 14 14 1	16 16 18 16 14 14 14 18 18 18 19 19 19 19 19 19 19 19 19 19 19 19 19	11/22 11/23 11/25 11/25 17/25 17/25 17/25 23/25 23/25 11/26

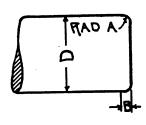
Taper 1/4" in 12".

Lengths from 34" to 51/2" advancing by 14".

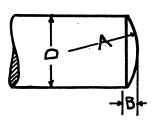
[Cincinnati Bickford Tool Co., Cincinnati, O.]

# FINISHED ENDS OF SHAFTS, BOLTS AND BUSHINGS

SOLID OR HOLLOW SHAFTS

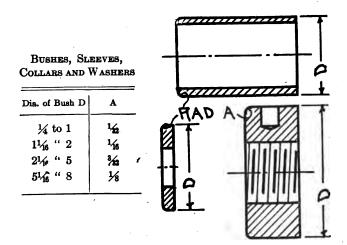


Dia. of Shaft D	A	B End of Shaft to Bearing
14 to 12 16 " 1 116 " 2 216 " 3 316 " 4 416 " 6 6 " 8	1/32 1/16 3/32 1/8 5/32 3/16 1/4	1/6 3/2 1/2 3/6 3/6 1/4 3/8



Dia. of D	<sup>4</sup> A	В
14 to 7/6 1/2 " 11/6 3/4 " 15/6 1 " 11/4 15/6 " 15/8	11/ <sub>32</sub> 19/ <sub>32</sub> 27/ <sub>32</sub> 1 1/ <sub>8</sub> 1 15/ <sub>32</sub>	1/6 3/2 1/8 5/2 7/2

Bolts



# RADA

## GEARS AND RACKS

Diametral Pitch	Circular Pitch	· A
1 to 11/4 11/2 " 2 21/4 " 3 31/2 " 4 5 " 7 8 " 10 11 " 16	3.142 to 2.513 2.094 " 1.571 1.396 " 1.047 .898 " .785 .628 " .449 .393 " .314 .286 " .196	1/2 1/4 8/6 1/8 8/22 1/66

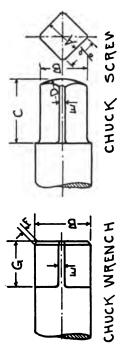
[Gisholt Mach. Co., Madison, Wis.]

Screw points—see page 42. Nail points—see page 78.

7, 15% 1%  $\frac{27}{2}$ 

1,7 111/6

STANDARD SQUARES FOR CHUCK SCREWS AND WRENCHES



		٠			<u> </u>			<u> </u>
1.	15%	11/4	115%	101	88	1.414	%	17%
%	11%	15%	111/6		82	1.237	1,26	-
%	37 <sub>18</sub>	11%	17,6	.094	83		72	%
11/16	2%	1	15%	760.	80	.972	3,5	13/6
*	18/6	15/6	11%	.072	83	.884	1/6	×
%	3%	13/6	1	820.	80	. 796	1/6	11/18
72	37/16	%	15/6		85	•	3,4	
15/2	3%1	11/6	7/8	.068	79		*	%
2,2	3%	%	13/6	.055	82	.618	*	%
13/2	17,6	%	1		85	.574	1,42	×
%	31,64	7%	%	.046	11	. 530	1/6	7,8
%	13/2	7,88	%	.036	28	.442	7,1	%
×	3/8	%	15/2	.041	77	.353	*	32
78	3%	%	13,6	.029	81		1,7	3%
7,2	13,7	<b>%</b>	%	.031	92	.265	1,7%	×
%	13,75	×	%	.018	æ	.221	1,54	×
		٠, ۵	<u></u>	21	<u></u>	1		

. 142

2%

\$

88

1.592 1.767 ×  $\frac{1}{\chi}$ 

74

13%

[Gisholt Machine Co., Madison, Wis.]

G.....

Sharp Corners..

% of A .....

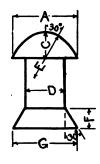
# SECTION VII

## STRUCTURAL DETAILS

RIVETS—RIVETED JOINTS—STRUCTURAL SHAPES—PLATES—WIRE AND SHEET METAL GAUGES—GAUGES FOR PUNCHING—RIVET SPACING—BEAM CONNECTIONS

## RIVETS

There are no universal proportions for structural and ship rivets, but those given on the following pages represent good practice.

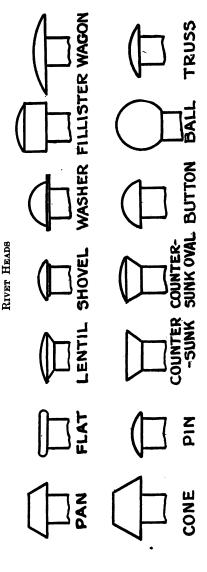


#### STRUCTURAL RIVETS

# American Bridge Co. Standard

Full driven head, diameter,  $A = 1.5 \, D + \frac{1}{8}$ Full driven head, depth,  $C = .425 \, A$ Full driven head, radius,  $E = 1.5 \, C$ Countersunk head, depth,  $F = .5 \, D$ Countersunk head, diameter,  $G = 1.577 \, D$ 

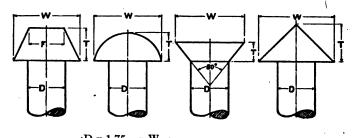
Dia. D	A	С	E	F	G
3/8 1/2 5/8 3/4 7/8 1 11/8 11/4	11/6 7/8 11/6 11/4 17/6 15/8 113/6 2	1964 38 2964 1752 3964 1116 4964	7.66 9.16 29.44 5.164 5.964 1.1.52 1.522 1.522	\$1.50 \$7.12 \$7.12 \$7.12 \$6.80 \$7.12 \$6.80	1952 2552 1 1366 138 1966 134 1156



Points for structural work are generally button while for ship they may be either button or flush, and for Button heads for structural work. Pan and flush for ship. For steeple head, see page 270. boilers, steeple.

## RIVET HEAD FORMULÆ

# Hoopes & Townsend



Cone Head . . 
$$\{D \times 1.75 = W \\ D \times .875 = T \\ D \times .9375 = F \}$$

Button Head 
$$\begin{cases} D \times 1.75 = W \\ D \times .75 = T \end{cases}$$

Countersunk Head D x 
$$.50 = T$$

Steeple Head . . . . 
$$\begin{cases} D \times 2 . &= W \\ D \times 1 . &= T \end{cases}$$

## SIZES OF RIVET HEADS

	Cone		Button		Countersunk		Steeple		
	Wide	Thick	Тор	Wide	Thick	Wide	Thick	Wide	Thick
Diameter 1,8,12,13,16,13,16,13,16,16,16,16,16,16,16,16,16,16,16,16,16,	7/8 63/44 13/52 11/5/64 11/7/52 14/1/64 13/1/52 25/64 23/16	7.16 1.22 35.54 35.54 45.54 13.76 55.54 11.32 11.32 11.32	15 52 17 52 87 64 41 64 49 64 53 64 7 8 15 16 1 11 64	7/8 63/44 13/52 113/64 15/64 117/52 14/64 13/4 155/64 131/52 25/64 23/6	3/8 27/64 115/32 33/64 9/16 33/64 21/52 45/64 51/64 51/64 51/64 51/64	15/16 11/16 15/32 11/4 13/8 11/2 15/8 13/4 113/16 131/32 22/16 25/16	1,4 9,5 11,8 8,3 1,7 15,3 1,7 15,8 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 12,18 1	1 11/8 11/4 18/8 11/2 15/8 13/4 17/8 2 21/8 22/4 22/4	1/2 9/16 5/8 11/16 18/16 18/16 11/18 11/18 11/14

## Champion Rivet Co., Cleveland, Ohio

let d = dia. of rivet

Cone Head. Least dia. =  $^{15}$ /<sub>16</sub>  $\times$  d Greatest dia. =  $1.75 \times$  d

Height =  $\frac{7}{8} \times d$ 

Button Head. Dia. =  $1.75 \times d$ Height =  $.75 \times d$ 

Steeple Head. Dia. =  $2 \times d$ Height =  $1\frac{1}{8} \times d$ 

Flat Head Countersunk. Height = 1/2 × d. Taper 78 degs.

Pan Head. Greatest dia. =  $1.75 \times d$ 

Height =  $\frac{9}{16} \times d$ 

Flat surface on top of head equals diameter of rivet, tapering in a rounding oval to the outside edge.

Oval Countersunk. Greatest dia. =  $1.75 \times d$ 78 degs. taper of countersink. Height of countersink =  $.5 \times d$ " " oval =  $^36 \times d$ Radius of oval =  $21/4 \times d$ 

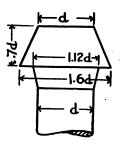
## SHIP RIVETS

## Lloyds

Form of Rivet, in Outside Plating.

Tapered neck of rivet to be of suitable length in relation to the thickness of plate in which it will be used.

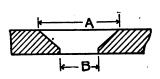
Countersink Rivets.—The countersink is to extend through the whole thickness of the plate when not more than .60 of an inch in thickness, when .60 of an inch or above, the countersink is to extend through nine tenths the thickness of the plate.



Tests.—Rivet shank bent cold on itself without cracking. Heads while hot can be flattened without cracking. Tensile strength 50,000 to 60,000 lbs. per sq. in., with an elongation of not less than 25% of the gauge length of eight times the diameter of the test piece.

SHIP RIVETS

Lloyds



Dia. of Rivet, Ins.	A, Ins.	B, Ins.
5 8 3 4 4 7 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	$ \begin{array}{c} 1 \\ 1^{3} \\ 1^{3} \\ 8 \\ 1^{9} \\ 1^{6} \\ 1^{3} \\ 1^{15} \\ 1^{6} \end{array} $	11 16 13 16 15 16 13 16 15 16 15 16

## TRUSS HEAD RIVETS

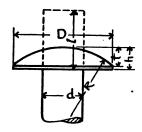
D = 2.5d

h = .5d

R = 2d

t = .4375d

l =1.81d

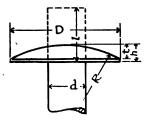


d	D	h	R	t	1
1/8 52 16 52 14 52 16 8 16 16 16 16 16 16 16 16 16 16 16 16 16	.3125 .3000 .4687 .5450 .6250 .7250 .7812 .9375 1.0937 1.2500	.0625 .0780 .0937 .1090 .1250 .1400 .1560 .1875 .2187	.250 .312 .375 .437 .500 .562 .625 .750 .875 1.000	.055 .0680 .082 .095 .109 .125 .137 .164 .191	.240 .282 .360 .395 .480 .510 .600 .720 .840

In rivet calculations (page 276) it is customary to disregard friction and proportion rivets to the entire stress to be transmitted.

#### WAGON BOX HEAD RIVETS





d	D	h	R	t	1
1/8/55 3/16/75 3/16/8/5/16/8/7/16/2	.350 .4375 .525 .6093 .7031 .7812 .875 1.050 1.220 1.400	.0547 .0680 .0820 .0950 .1090 .1230 .1365 .1640 .1910 .2188	.3500 .4375 .5250 .6093 .7031 .7812 .8750 1.0500 1.2200 1.4000	.0467 .0585 .0700 .0820 .0940 .1050 .1170 .1400 .1640 .1875	. 285 . 356 . 427 . 497 . 570 . 644 . 712 . 855 . 996 1.140

[The Atlas Bolt and Screw Co., Cleveland, Ohio.]

## Lengths of Rivets for Ordering

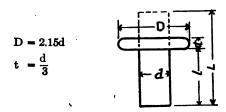
The length for ordering pan and button head rivets is measured exclusive of the head; for countersunk rivets and taps the ordered length includes the head to the top of the countersink.

ALLOWANCE FOR POINTS IN LENGTH OF RIVETS WITH TWO THICK-NESSES CONNECTED

	Diameters of Rivets (Ins.)						
Type of point	1/2	. 5/8	3/4	₹	1	11/8	
Countersunk	1/2 1/2 7/8 7/8	5/8 1/2 1 7/8	3/4 1/2 11/8 	7/8 5/8 11/4	1 5/8 13/8	1½ 5/8 1½	

#### 274 HANDBOOK OF STANDARD DETAILS

TINNERS RIVETS



Sise	Max. Dia. d	1	D	t	L
6 oz. 8 " 10 "	.082 .092 .095 .106 .109 .112 .120 .130 .134 .144 .148 .161 .165 .176 .181 .186 .203 .216 .225 .234 .238 .259	5/22	11/64 8/16	.027	9/2
8 "	.092	5/82	8/16	.031	1 %2
10 "	.095	1164	1864	.032	5/16
12 "	.106	5 22 5 32 11 64 3 16 13 64 7 32 15 64	1/2	.035	1964
14 " 1 lb.	.109	<sup>3</sup> / <sub>16</sub>	15,64	.036	11/2
1 lb.	.112	13.64	1/4	.037	13/52
1¼ "	.120	7/22	17/64	.040	2764
1½ " 1½ " 1¾ " 2 " 2½ " 3 " 3½ "	. 130	1574	1764 952 1964 5/6	.043	15/22
134 "	. 134	- <del>7</del> 4	1964	.044	81/64
2 "	.144	17.7 84	5/16	.048	15/82
2½ "	.148	9/12	21,64	.049	37/64
3´ "	.161	5/16	11/32	.053	8764
3½ "	. 165	21/64	43/64	.055	5/8
4 "	.176	1172	3/8	.058	41/64
41/2 "	. 181	23/64	25/64	.060	11/16
5 "	. 186	3/8	13 % 7 %	.062	23/32
6 "	.203	25/64	7/6	.067	11/16
41/2 " 5 " 6 " 7 " 8 "	.216	13/32	15 32	.072	23/52
8 "	. 225	7 16 29 64 15 59	81,64	.075	25/32
9 "	.234	2964	1/2	.078	4964
10	.238	15 32	33 64 9 16 39 64 41 64	. 027 . 031 . 032 . 035 . 036 . 037 . 040 . 043 . 044 . 048 . 049 . 053 . 055 . 058 . 060 . 062 . 067 . 072 . 075 . 078 . 079 . 086	27/82
12 "	.259	1/2	9/16	.086	55/64
14 "	.284	33 64 17 32	3964	.094	58/64
16 "	.300	17,32	41/64	.1	1 1/8

In ordering rivets, the diameter should be given first and then the length, thus— $\frac{1}{2}$ " x 3". Rivets are usually shipped in kegs of 100 lbs.

#### CONVENTIONAL SIGNS FOR RIVETS

#### RIVET SIGNS

SHOP RIVETS

2 FULL HEADS



CSK FAR SIDE



C'S'K NEAR

C'5'K NOT CHIPPED '%" HIGH



CSK BOTH SIDES



NEAR SIDE







FLATTENED TO 14" HIGH





#### FIELD RIVETS

2 FULL HEADS



C'5'K FAR SIDE AND CHIPPED



C'5'K NEAR SIDE AND CHIPPED

C'S'K BOTH SIDES

Allowable Single Shearing Stress in lbs. per sq. in.

Shop rivets	.12,000	lbs.
Field rivets and turned bolts	.16,000	"
Field rough bolts	. 8,000	"

#### RIVETED JOINTS

Diameter of rivet is 1.2 to 1.4 times  $\sqrt{}$  thickness of plate.

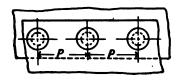
Distance from center of rivet to plate edge  $1\frac{1}{2}$  to 2 times the diameter of the rivet; for water tight work use  $1\frac{5}{8}$ .

Water tight spacing 3½ times the diameter of the rivet; oil tight, 3 to 3½ times.

In chain riveting distance between rows of rivets is 2 to 2½ times the diameter of the rivet. In staggered riveting 1.7.

Tensile strength of steel plates generally taken at 60,000 lbs. per sq. in. Shearing strength of rivets 50,000 lbs. per sq. in.

Shearing strength of a rivet in double shear is usually about 1.75 times the strength in single shear.



All dimensions in inches, and stresses in pounds per square inch. Lap Joint, Single Riveted

Resistance to tearing plate between rivets = t (p-d) T

" " crushing of one rivet = t d C

" shearing " " " = 
$$\frac{1}{4}\pi d^2 S$$

Lap Joint, Double Riveted

Resistance to tearing plate between two rivets = t (p-d) T

" " crushing of two rivets = 2 td C

" shearing " " " = 
$$\frac{2 \pi d^2 S}{4}$$

Butt Strap, Single Riveted, Two Cover Plates

Resistance to tearing plate 
$$= t (p-d) T$$
" " crushing of one rivet  $= t d C$ 
" " shearing " " "  $= \frac{2 \pi d^2 S}{4}$ 

#### Butt Strap, Double Riveted, Two Cover Plates Resistance to tearing plate

" crushing of two rivets

"shearing "

$$= t (p-d) T$$
  
= 2 t d C  
4  $\pi$  d<sup>2</sup> S

#### STRUCTURAL SHAPES

(Rolled by Carnegie Steel Co.)

I = moment of inertia about line through center of gravity

y = distance from center of gravity to extreme fiber

 $s = section modulus = \frac{I}{y}$ . A = area of section

 $r = radius of gyration = \sqrt{\frac{I}{A}}$ .

#### STRUCTURAL CHANNELS

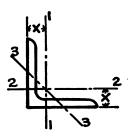


	th of	Weight per Foot	to d	th of	of	A	xis 1-1			Axis	2-2	
Section Index	Depth of Channel	Weių per	Ares of Section	Width (Flange	Thick- ness of Web	I	r	8	I	r	8	x
	In.	Lbs.	Sq. ins.	In.	In.	In.4	In.	In.ª	In.4	In.	In.3	In.
C 1	15	55.0 50.0 45.0 40.0 35.0 33.0	14.71 13.24 11.76 10.29	3.426	.622 .524 .426	430.2 402.7 375.1 347.5 319.9 312.6	5.16 5.23 5.32 5.43 5.58 5.62	57.4 53.7 50.0 46.3 42.7 41.7	12.2 11.2 10.3 9.4 8.5 8.2	.87 .88 .89 .91	4.1 3.8 3.6 3.4 3.2 3.2	.82 .80 .79 .78 .79
C 2	12	40.0 35.0 30.0 25.0 20.5	10.29 8.82 7.35	3.296 3.173	.636 .513 .390	196.9 179.3 161.7 144.0 128.1	4.09 4.17 4.28 4.43 4.61	32.8 29.9 26.9 24.0 21.4	6.6 5.9 5.2 4.5 3.9	.75 .76 .77 .79 .81	2.5 2.3 2.1 1.9 1.7	.72 .69 .68 .68 .70
C 3	10	35.0 30.0 25.0 20.0 15.0	8.82 7.35 5.88	3.183 3.036 2.889 2.742 2.600	.676 .529 .382	115.5 103.2 91.0 78.7 66.9	3.35 3.42 3.52 3.66 3.87	23.1 20.7 18.2 15.7 13.4	4.7 4.0 3.4 2.9 2.3	.67 .68 .70 .72	1.9 1.7 1.5 1.3 1.2	.70 .65 .62 .61 .64

#### STRUCTURAL CHANNELS-Continued

	Depth of Channel	Weight per Foot	o of ion	th of	450	A	xis 1-	1		Axis	2–2	
Section Index	00 to	Wei.	Area of Section	Width o Flange	Thick- ness of Web	I	r	8	I	r	8	x
	In.	Lbs.	Sq.ins.	In.	In.	In.4	In.	In.*	In.4	In.	In.ª	In.
C 4	9	25.0 20.0 15.0 13.25	7.35 5.88 4.41 3.89	2.815 2.652 2.488 2.430	.615 .452 .288 .230	70.7 60.8 50.9 47.3	3.10 3.21 3.40 3.49	15.7 13.5 11.3 10.5	3.0 2.5 2.0 1.8	.67	1.4 1.2 1.0 0.97	.62 .59 .59
C 5	8	21.25 18.75 16.25 13.75 11.25	6.25 5.51 4.78 4.04 3.35	2.622 2.530 2.439 2.347 2.260	.582 .490 .399 .307 .220	47.8 43.8 39.9 36.0 32.3	2.77 2.82 2.89 2.98 3.11	11.9 11.0 10.0 9.0 8.1	2.3 2.0 1.8 1.6 1.3	.61	1.1 1.0 0.95 0.87. 0.79	.59 .57 .56 .56
C 6	7	19.75 17.25 14.75 12.25 9.75	5.81 5.07 4.34 3.60 2.85	2.513 2.408 2.303 2.198 2.090	.633 .528 .423 .318 .210	33.2 30.2 27.2 24.2 21.1	2.39 2.44 2.50 2.59 2.72	9.5 8.6 7.8 6.9 6.0	1.9 1.6 1.4 1.2 0.98	.56 .57 .57 .58 .59	0.96 0.87 0.79 0.71 0.63	.58 .56 .54 .53 .55
C 7	6	15.5 13.0 10.5 8.0	4.56 3.82 3.09 2.38	2.283 2.160 2.038 1.920	.563 .440 .318 .200	19.5 17.3 15.1 13.0	2.07 2.13 2.21 2.34	6.5 5.8 5.0 4.3	1.3 1.1 0.88 0.70	.53 .53 .53 .54	0.74 0.65 0.57 0.50	.55 .52 .50 .52
C 8	5	11.5 9.0 6.5	3.38 2.65 1.95	2.037 1.890 1.750	.477 .330 .190	10.4 8.9 7.4	1.75 1.83 1.95	4.2 3.6 3.0	0.82 0.64 0.48	.49 .49 .50	0.54 0.45 0.38	.51 .48 .49
C 9	4	7.25 6.25 5.25	2.13 1.84 1.55	1.725 1.652 1.580	.325 .252 .180	4.6 4.2 3.8	1.46 1.51 1.56	2.3 2.1 1.9	0.38 0.44 0.32	.46 .45 .45	0.35 0.32 0.29	.46 .46 .46
C 72	3	6.0 5.0 4.0	1.76 1.47 1.19	1.602 1.504 1.410	.362 .264 .170	2.1 1.8 1.6	1.08 1.12 1.17	1.4 1.2 1.1	0.31 0.25 0.20	.42 .42 .41	0.27 0.24 0.21	.46 .44 .44

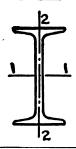
#### EQUAL ANGLES



	Size	Weight	Area of	Ax	is 1–1 an	d Axis 2	-2	Axis 3-3
Section Index	5156	per Foot	Section	I	r	8	x	r min.
	Ins.	Pounds	In.2	In.4	In.	In.*	In.	In.
A 3 A 4 A 5 A 6 A 7 A 8 A 88	6 x 6 x 3/4 11/19 5 6 9/19 1/2 7/16 3/8	28.7 26.5 24.2 21.9 19.6 17.2 14.9	8.44 7.78 7.11 6.43 5.75 5.06 4.36	28.2 26.2 24.2 22.1 19.9 17.7 15.4	1.83 1.83 1.84 1.85 1.86 1.87 1.88	6.7 6.2 5.7 5.1 4.6 4.1 3.5	1.78 1.75 1.73 1.71 1.68 1.66 1.64	1.17 1.17 1.17 1.18 1.18 1.19 1.19
A 11 A 12 A 13 A 14 A 15 A 16 A 17	5 x 5 x 3/4 11/6 5 8 9 6 1/2 1/6 3/8	23.6 21.8 20.0 18.1 16.2 14.3 12.3	6.94 6.40 5.86 5.31 4.75 4.18 3.61	15.7 14.7 13.6 12.4 11.3 10.0 8.7	1.50 1.51 1.52 1.53 1.54 1.55 1.56	4.5 4.2 3.9 3.5 3.2 2.8 2.4	1.52 1.50 1.48 1.46 1.43 1.41 1.39	.97 ' .97 .97 .98 .98 .98
A 19 A 20 A 21 A 22 A 23 A 24 A 25	4 x 4 x 3/4 11/6 5/8 1/2 1/6 3/8	18.5 17.1 15.7 14.3 12.8 11.3 9.8	5.44 5.03 4.61 4.18 3.75 3.31 2.86	7.7 7.2 6.7 6.1 5.6 5.0 4.4	1.19 1.19 1.20 1.21 1.22 1.23 1.23	2.8 2.6 2.4 2.2 2.0 1.8 1.5	1.27 1.25 1.23 1.21 1.18 1.16 1.14	.77 .77 .77 .78 .78 .78
A 29 A 30 A 31 A 32 A 33 A 99 A 285	31/2×31/2×5/8 1/2 1/2 1/4 8/8 1/8	13.6 12.4 11.1 9.8 8.5 7.2 5.8	3.98 3.62 3.25. 2.87 2.48 2.09 1.69	4.3 4.0 3.6 3.3 2.9 2.5 2.0	1.04 1.05 1.06 1.07 1.07 1.08 1.09	1.8 1.6 1.5 1.3 1.2 .98	1.10 1.08 1.06 1.04 1.01 .99	.68 .68 .68 .69 .69
A 36 A 37 A 38 A 39 A 40	3 x 3 x 1/2	9.4 8.3 7.2 6.1 4.9	2.75 2.43 2.11 1.78 1.44	2.2 2.0 1.8 1.5 1.2	.90 .91 .91 .92 .93	1.1 .95 .83 .71 .58	.93 .91 .89 .87	.58 .58 .58 .59
A 48 A 49 A 50	2½x2½x¾ 16	5.9 5.0 4.1	1.73 1.47 1.19	.98 .85 .70	.75 .76 .77	.57 .48 .39	.76 .74 .72	.48 .49 .49
A 59 A 60	2 x 2 x 1/4	3.19 2.44	.94 .71	.35 .28	.61 .62	.25 .19	.59 .57	.39 .40

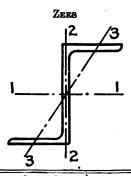
Structural Shapes—of steel made by the open hearth process. The steel used in ships has a tensile strength of 58,000-68,000 lbs. per sq. in.; yield point minimum .5 tensile strength; elongation in 8 ins. minimum per cent  $\frac{1,500,000}{\text{tensile strength}}$ . Steel for buildings has a slightly lower tensile strength.





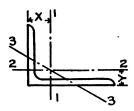
dex	Depth of Beam	tht Foot	of	Width of Flange	of of	A	xis 1-1	l	A	xis 2-	2
Section Index	of D Bagi	Weight per Foot	Area of Section	Wid of F	Thick- ness of Web	I	r	8	I	r	В
Sect	In.	Lbs.	In.3	In.	In.	In.4	In.	In.	In.4	In.	In.8
B 61	27	90	26.33	9.000	. 524	2958.3	10.60	219.1	75.3	1.69	16.7
B 24	24	115 110 105	33.98 32.48 30.98	8.000 7.938 7.875	.750 .688 .625	2955.5 2883.5 2811.5	9.42	246.3 240.3 234.3	83.2 81.0 78.9	1.57 1.58 1.60	20.8 20.4 20.0
B 1	24	100 95 90 85 80	29.41 27.94 26.47 25.00 23.32	7.254 7.193 7.131 7.070 7.000	.754 .693 .631 .570 .500	2379.6 2399.0 2238.4 2167.8 2087.2	9.09 9.20 9.31	198.3 192.4 186.5 180.7 173.9	48.6 47.1 45.7 44.4 42.9	1.28 1.30 1.31 1.33 1.36	13.4 13.1 12.8 12.6 12.3
B 62	24	74	21.70	9.000	.476	1950.1	9.48	162.5	61.2	1.68	13.6
B 63	21	60.5	17.68	8.250	.428	1235.5	8.36	117.7	43.5	1.57	10.6
<b>B</b> 2	20	100 95 90 85 80	29.41 27.94 26.47 25.00 23.73	7.284 7.210 7.137 7.063 7.000	.884 .810 .737 .663 .600	1655.6 1606.6 1557.6 1508.5 1466.3	7.58 7.67 7.77	165.6 160.7 155.8 150.9 146.6	52.7 50.8 49.0 47.3 45.8	1.34 1.35 1.36 1.37 1.39	14.5 14.1 13.7 13.4 13.1
В 3	20	75 70 65	22.06 20.59 19.08	6.399 6.325 6.250	.649 .575 .500	1268.8 1219.8 1169.5	7.70	126.9 122.0 117.0	30.3 29.0 27.9	1.17 1.19 1.21	9.5 9.2 8.9
B 81	18	90 85 80 75	26.47 25.00 23.53 22.05	7.245 7.162 7.083 7.000	.807 .725 .644 .562	1260.4 1220.7 1181.0 1141.3	6.99 7.09	140.0 135.6 131.2 126.8	52.0 50.0 48.1 46.2	1.40 1.42 1.43 1.45	14.4 14.0 13.6 13.2
B 80	18	70 65 60 . 55	20.59 19.12 17.65 15.93	6.259 6.177 6.095 6.000	.719 .637 .555 .460	921.2 881.5 841.8 795.6	6.69 6.79 6.91 7.07	102.4 97.9 93.5 88.4	24.6 23.5 22.4 21.2	1.09 1.11 1.13 1.15	7.9 7.6 7.3 7.1
B 64	18	48	14.08	7.500	.380	737.1	7.23	81.9	30.0	1.46	8.0
В 5	15	75 70 65 60	22.06 20.59 19.12 17.67	6.292 6.194 6.096 6.000	.882 .784 .686 .590	691.2 663.7 636.1 609.0	5.60 5.68 5.77 5.87	92.2 88.5 84.8 81.2	30.7 29.0 27.4 26.0	1.18 1.19 1.20 1.21	9.8 9.4 9.0 8.7

dex	th ea.m	oot	of on	Width of Flange	of <sup>k</sup>	A	xis 1–1		A	xis 2-	2
Section Index	Depth of Beam	Weight per Foot	Area of Section	Wid of Fi	Thick- ness of Web	I	r	8	I	r	8
Sec	In.	Lbs.	In.º	In.	In.	In.4	In.	In.3	In.4	In.	In.
В 7	15	55 50 45 42	16.18 14.71 13.24 12.48	5.746 5.648 5.550 5.500	.656 .558 .460 .410	511.0 483.4 455.9 441.8	5.62 5.73 5.87 5.95	68.1 64.5 60.8 58.9	17.1 16.0 15.1 14.6	1.02 1.04 1.07 1.08	5.9 5.7 5.4 5.3
B 65	15	37.5	10.91	6.750	.332	405.5	6.10	54.1	19.9	1.35	5.9
В 8	12	55 50 45 40	16.18 14.71 13.24 11.84	5.611 5.489 5.366 5.250	.821 .699 .576 .460	321.0 303.4 285.7 269.0	4.45 4.54 4.65 4.77	53.5 50.6 47.6 44.8	17.5 16.1 14.9 13.8	1.04 1.05 1.06 1.08	6.2 5.9 5.6 5.3
В 9	12	35 31. 5	10.29 9.26	5.086 5.000	.436 .350	228.3 215.8	4.71 4.83	38.0 36.0	10.1 9.5	.99 1.01	4.0 3.8
B 66	12	28	8.15	6.000	.284	199.4	4.95	33.2	12.6	1.24	4.2
B 11	.10	40 35 30 25	11.76 10.29 8.82 7.37	5.099 4.952 4.805 4.660	.749 .602 .455 .310	158.7 146.4 134.2 122.1	3.67 3.77 3.90 4.07	31.7 29.3 26.8 24.4	9.5 8.5 7.7 6.9	.90 .91 .93 .97	3.7 3.4 3.2 3.0
B 67	10	22.25	6.54	5.500	.252	113.6	4.17	22.7	9.0	1.17	3.3
B 13	9	35 30 25 21	10.29 8.82 7.35 6.31	4.772 4.609 4.446 4.330	.732 .569 .406 .290	111.8 101.9 91.9 84.9	3.29 3.40 3.54 3.67	24.8 22.6 20.4 18.9	7.3 6.4 5.7 5.2	.84 .85 .88 .90	3.1 2.8 2.5 2.4
B 15	8	25. 5 23 20. 5 18	7.50 6.76 6.03 5.33	4.271 4.179 4.087 4.000	.541 .449 .357 .270	68.4 64.5 60.6 56.9	3.02 3.09 3.17 3.27	17.1 16.1 15.2 14.2	4.8 4.4 4.1 3.8	.80 .81 .82 .84	2.2 2.1 2.0 1.9
B 68	8	17. 5	5.12	5.000	.220	58.4	3.38	14.6	6.2	1.10	2.5
B 17	7	20 17. 5 15	5.88 5.15 4.42	3.868 3.763 3.660	.458 .353 .250	42.2 39.2 36.2	2.68 2.76 2.86	12.1 11.2 10.4	3.2 2.9 2.7	.74 .76 .78	1.7 1.6 1.5
B 19	6	17.25 14.75 12.25	5.07 4.34 3.61	3.575 3.452 3.330	.475 .352 .230	26.2 24.0 21.8	2.27 2.35 2.46	8.7 8.0 7.3	2.4 2.1 1.9	.68 .69 .72	1.3 1.2 1.1
B 21	5	14.75 12.25 9.75	4.34 3.60 2.87	3.294 3.147 3.000	.504 .357 .210	15.2 13.6 12.1	1.87 1.94 2.05	6.1 5.5 4.8	1.7 1.5 1.2	.63 .63 .65	1.0 .92 .82
B 23	4	10. 5 9. 5 8. 5 7. 5	3.09 2.79 2.50 2.21	2.880 2.807 2.733 2.660	.410 .337 .263 .190	7.1 6.8 6.4 6.0	1.52 1.55 1.59 1.64	3.6 3.4 3.2 3.0	1.0 .93 .85 .77	.57 .58 .58 .59	.70 .66 .62 .58
B 77	3	7. 5 6. 5 5. 5	2.21 1.91 1.63	2.521 2.423 2.330	.361 .263 .170	2.9 2.7 2.5	1.15 1.19 1.23	1.9 1.8 1.7	.60 .53 .46	. 52 . 52 . 53	.48 .44 .40



		Sise		W'ght.	Area	A	xis 1	-1	A	xis 2-	-2	Axis 3–3
Sec- tion Index	Depth	Flanges	Thick- ness	Foot.	Sec- tion	I	r	8	I	r	8	r min.
	In.	In.	In.	Lbs.	In.2	In.4	In.	In.3	In.4	In.	In.3	In.
<b>Z</b> 3	6½ 6½ 6	35/8 39/16 31/2	7/8 13/19 3/4	34.6 32.0 29.4	10.17 9.40 8.63	46.1	2.22	16.4 15.2 14.0	17.3	1.36	6.0 5.5 4.9	.83 .82 .81
Z 2	6½ 6½ 6	35/6 35/6 31/2	11 16 5 8	28.1 25.4 22.8	8.25 7.46 6.68	38.9	2.28	14.1 12.8 11.5	14.4	1.39	5.0 4.4 3.9	.84 .82 .81
Z 1	61/8 61/16 6	35/8 35/6 31/2	1/2 1/16 3/8	21.1 18.4 15.7	6.19 5.39 4.59	34.4 29.8 25.3	2.36 2.35 2.35	11.2 9.8 8.4	12.9 11.0 9.1	1.43	3.8 3.3 2.8	.84 .83 .83
Z 6	51/8 51/16 5	33/8 35/6 31/4	13/6 3/4 11/16	28.4 26.0 23.7	8.33 7.64 9.96	28.7 26.2 23.7	1.85	11.2 10.3 9.5	14.4 12.8 11.4	1.30	4.8 4.4 3.9	.76 .74 .73
<b>Z</b> 5	51/8 51/16 5	33/8 35/6 31/4	5/8 9/16 1/2	22.6 20.2 17.9	6.64 5.94 5.25	$24.5 \\ 21.8 \\ 19.2$	1.91		12.1 10.5 9.1	1.33	3.9 3.5 3.0	.76 .75 .74
Z 4	51/8 51/16 5	33/8 35/16 31/4	7/16 3/8 5/16	16.4 14.0 11.6	4.81 4.10 3.40	19.1 16.2 13.4	1.99	7.4 6.4 5.3	7.7	1.38 1.37 1.35	2.9 2.5 2.0	:77 .76 .75
Z 9	41/8 41/16 4	3 <sup>3</sup> /6 3 <sup>1</sup> /8 3 <sup>1</sup> /6	3/4 11/16 5/8	23.0 20.9 18.9	6.75 6.14 5.55	15.0 13.5 12.1	1.48	6.7	11.2 10.0 8.7	1.27	4.0 3.6 3.2	.68 .67 .66
Z 8	41/8· 41/16 4	33/8 31/8 31/16	16 1/2 7/16	18.0 15.9 13.8	5.27 4.66 4.05	12.7 11.2 9.7	1.55 1.55 1.55	6.2 5.5 4.8	9.3 8.0 6.7	1.31	3.2 2.8 2.4	.68 .67 .66
Z 7	4½ 4½ 4	3 <sup>3</sup> / <sub>16</sub> 3 <sup>1</sup> / <sub>8</sub> 3 <sup>1</sup> / <sub>16</sub>	3/8 5/16 1/4	12.5 10.3 8.2	3.66 3.03 2.41	7.9	1.62 1.62 1.62	4.7 3.9 3.1	6.8 5.5 4.2	1.34	2.3 1.8 1.4	.69 .68 .67
Z 12	31/16 3	234 211/4	16	14.3 12.6	4.18 3.69	5.3 4.6	1.12 1.12	3.4 3.1	5.7 4.9		2.3 2.0	.54 .53
Z 11	31/16 3	234 211/16	7/16 3/8	11.5 9.8	3.36 2.86	4.6 3.9	1.17 1.16	3.0 2.6	4.8 3.9		1.9 1.6	.55 .54
Z 10	31/4 3	23/4 211/4	12	8.5 6.7	2.48 1.97	3.6 2.9	1.21 1.21	2.4 1.9	3.6 2.8		1.4 1.1	. 56 . 55

UNEQUAL ANGLES



	Sise	Weight	Area		Axi	is 1–1			Ax	is 2–2	3	Axis 3-3
Section Index	Size	Foot	of section	I	r	8	x	I	r	8	x	r min.
	Ins.	Pounds	In.3	In.4	In.	In.	In.	In.4	In.	In.3	In.	In.
A 171 A 172 A 173 A 174 A 175 A 176 A 177	6x3½x¾ 11,4 5,6 1,4 1,4 1,4 1,4 1,4 1,4 1,4 1,4 1,4 1,4	22.4 20.6 18.9 17.1 15.3 13.5	6.56 6.06 5.55 5.03 4.50 3.97 3.42	21.7 20.1 18.4 16.6	$\frac{1.92}{1.93}$	5.6 5.2 4.7 4.2 3.7	2.18 2.15 2.13 2.11 2.08 2.06 2.04	5.8 5.5 5.1 4.7 4.3 3.8 3.8	.94 .95 .96 .96 .97 .98	2.3 2.1 1.9 1.8 1.6 1.4	.93 .90 .88 .86 .83 .81	.75 .75 .75 .75 .76 .76
A 201 A 202 A 203 A 280	5 x 3 x 1/2 7/6 3/8	12.8 11.3 9.8 8.2	3.75 3.31 2.86 2.40	8.4 7.4	1.59 1.60 1.61 1.61	2.6 2.2	1.75 1.73 1.70 1.68	2.6 2.3 2.0 1.8	.83 .84 .84 .85	1.1 1.0 .89 .75	.75 .73 .70 .68	.65 .65 .65
A 225 A 226 A 227 A 228	4 x 3 x 1/2 1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4	11.1 9.8 8.5 7.2	3.25 2.87 2.48 2.09	4.5	1.25 1.25 1.26 1.27	1.7 1.5	1.33 1.30 1.28 1.26	2.4 2.2 1.9 1.7	.86 .87 .88 .89	1.1 1.0 .87 .74	.83 .80 .78 .76	.64 .64 .64 .65
A 234 A 235 A 236 A 237 A 286	31/4x3x1/4 1/4 3/4 1/4	10.2 9.1 7.9 6.6 5.4	3.00 2.65 2.30 1.93 1.56	3.1 2.7 2.3	1.07 1.08 1.09 1.10 1.11	1.3 1.1 .96	1.13 1.10 1.08 1.06 1.04	2.3 2.1 1.8 1.6 1.3	.88 .89 .90 .90	1.1 .98 .85 .72 .58	.88 .85 .83 .81 .79	.62 .62 .63 .63
A 255	3x2½x3/8	6.6	1.92	1.7	.93	.81	.96	1.0	.74	.58	.71	. 52
A 256 A 257	16	5.6 4.5	1.62 1.31	$\frac{1.4}{1.2}$	.94 .95	. 69 . 56	.93 .91	.90 .74	.74 .75	.49 .40	.68 .66	. 53 . 53

Ordering Shapes.—Beams, channels, bulb angles, Tees and Zees should be ordered to weight per linear foot. Angles may be ordered either to weight per foot or to thickness, but never both.

WIRE AND SHEET METAL GAUGES

DIAMETERS AND THICKNESSES IN DECIMAL PARTS OF AN INCH

Gauge number	Am. wire gauge or Brown & Sharpe	Birmingham wire gauge (B. W. G.) or Stube	Steel wire gauge or Washburn & Moen or Roebling	Trenton Iron Co.	Stubs' steel wire	U. S. Standard for sheet metal	Imperial wire or N. B. S.
000000					<del></del>	.4687	. 464
00000				. 4500		. 4375	. 432
0000	.4600	. 454	.3938	.4000		. 4062	.400
000	.4096	.454 .425	. 3625	.3600		.3750	. 372
00	. <b>364</b> 8	.380 .340	.3310	. 3300		.3437	.348 .324
0	.3249	.340	.3065	.3050		.3125	.324
1	.2893	.300	.2830	.2850	.227	.2812	.300
2	.2576	.284	.2625	.2650	.219	.2656	.276
3	.2294	.259 .238	.2437	.2450	.212	.2500	. 252 . 232
1 2 3 4 5 6 7 8	.2043	.238	.2253	.2250	.207	.2344	.232
5	.1819	.220	.2070	.2050	.204	.2187	.212
0 7	. 1620 . 1443	.203	. 1920 . 1770	.1900	.201 .199	.2031	.192
6	.1285	. 180 . 165	.1620	.1750 .1600		. 1875 . 1719	.177 .160
9	.1144	.148	.1483	.1450	.197 .194	.1562	.144
10	.1019	.134	.1350	.1300	.191	.1406	.128
11	.0907	.120	.1205	.1175	.188	.1250	.116
12	.0808	109	. 1055	.1050	185	.1094	104
13	.0720	. 109 . 095	.0915	.0925	.185	.0937	.104 .092
14	.0641	.083	.0800	.0800	.180	.0781	.080
15	.0571	.072	.0720	.0700	.178	.0703	.072
16	.0508	.065	.0625	.0610	.175	.0625	.064
17	.0453	.058	.0540	.0525	.172	.0562	. 056
18	.0403	.049	.0475	.0450	.168	. 0500	.048
19	.0359	.042	.0410	.0400	. 164	.0437	.040
20	.0320	.035	.0348	.0350	.161	.0375	.036
21	.0285	.032	.0317	.0310	. 157	.0344	.032
22	.0253	.028	.0286	.0280	. 155	.0312	.028
23	.0226	.025	.0258	.0250	. 153	.0281	.024
24	.0201	.022	.0230	.0225	.151	.0250	.022
25 26	.0179	.020 .018	.0204 .0181	.0200 .0180	.148 .146	.0219 .0187	.020 .018
20 27	.0159 .0142	.018	.0181	.0170	.146	.0172	.0164
28	.0142	.016	.0173	.0160	.139	.0172	.0104
29	.0120	.013	.0150	.0150	.134	.0141	.0136
30	.0100	.013	.0140	.0140	.127	.0125	.0124
31	.0089	.012	.0132	.0130	.120	.0123	.0116
32	.0079	.009	.0128	.0120	.115	.0102	.0108
33	.0071	.008	.0118	.0110	.112	.0094	.0100

Gauge number	Am. wire gauge or Brown & Sharpe	Birmingham wire gauge (B. W. G.) or Stubs.	Steel wire gauge or Washburn & Moen or Roebling	Trenton Iron Co.	Stubs' steel wire	U. S. Standard for sheet metal	Imperial wire or N. B. S.
34	.0063	.007	.0104	.0100	.110	.0086	.0092
35	.0056	.005	.0095	.0095	.108	.0078	.0084
36	.0050	.004	.0090	.0090	.106	.0070	.0076
37	.0045			.0085	.103	.0066	.0068
34 35 36 37 38	.0040			.0080	.101	.0062	.0060
39	.0035			.0075	.099		.0052
40	.0031			.0070	.097		.0048

#### WEIGHT OF FLAT BAR STEEL, PER LINEAL FOOT

- Control	1/2	58	3/4	7/8	1	11/8	11/4	13/8	11/2	13/4	2	21/4	21/2	23/4	3	31/2
	.213	.266	.320	372	.426			.585		.745	.850	.955	1.07	1.18	1.28	1.49
ı	.319	.399	480	.558			.790			1.12	1.28	1.43	1.60	1.76	1.92	2.2
1	.425		.640		.852			1.17			1.70	1 91	2.13	2.34	2.56	2.9
1	.531	.665	.800			1.20				1.86	2.13	2.39	2.66	2.92	3.19	3.7
ч	.638	.798	.960		1.28		1.59		1.91		2.55	2.87	3.20	3.51	3.83	4.4
	.744	,931	1.12	1.30			1.86		2.23		2.98	3,35	3.72	4.09	4.46	5.2
-1		1.07	1.28	1.49	1.70	1.91	2.13	2.34	2.55	2.98	3.40	3.83	4.26	4.68	5.10	5.9
1		1.20	1.44	1.67	1.91	2.15	2.39	2.63	2.87	3.35	3.83	4.30	4.78	5.26	5.74	6.6
		12.07	1.60	1.86	2.12	2.39	2.66	2.92	3.19	3.72	4.26	4.79	5.32	5.86	6.39	7.4
6			1.76	2.04	2.34	2.63	2.92	3.22	3.51	4.09	4.68	5.26	5.84	6.43	7.01	8.1
" I								3.50			5.10	5.74	6.40	7.02	7.65	8.9
1								3.80			5.53	6.22	6.91	7.60	8.29	9.6
Ô	3.0				2 98			4.09			5.96	6.70	7.46	8.19	8.94	
6		1 6 7 7	****		3.19			4.38			6.38	7.17	7.97	8.77	9.56	
1		1	2017	100				4.68			6.80	7.66	8.52		10.20	

#### WEIGHTS OF STEEL PLATES

Thickness Ins.	Weight per Sq. Ft. Lbs.	Thickness Ins.	Weight per Sq. Ft. Lbs.	Thickness Ins.	Weight per Sq. Ft. Lbs.
14 52 51 6 11 2 3 8 13 2 7 16 16 16 16 16 16 16 16 16 16 16 16 16	10.200 11.475 12.750 14.025 15.300 16.575 17.850 19.125 20.400	17, 52 9 16 19, 53 5, 6 21, 52 11, 16 23, 52 3, 4 25, 52	21 .675 22 .950 24 .225 25 .500 26 .775 28 .050 29 .325 30 .600 31 .875	13 /6 27 /2 7/2 7/8 29 /2 15 /6 31 /2 1	33 . 150 34 . 425 35 . 700 36 . 975 38 . 250 39 . 525 40 . 800

#### ' GAUGES FOR PUNCHING

As punching injures the metal around the hole, the hole should be punched  $\frac{1}{16}$  in. smaller than the rivet and then reamed, the finished hole being about  $\frac{1}{16}$  in. greater than the diameter of the rivet. The burr caused by punching must be removed before the parts are riveted together.

Drilled holes are  $\frac{1}{16}$  in. larger than the bolt or rivet. When holes are drilled, the metal is not injured as in punching. For boilers the plates are drilled, as they are also in many cases for tanks.

I BEAMS



Depth of beam	Gage G	Max. rivet in flange	Depth of beam	Gage G	Max. rivet in flange
27 24 21 20 18 15 12 10	4 4 4 3 3 3 2 8 4	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	9 8 7 6 5 4	2½ 2¼ 2¼ 2¼ 2 1¾ 1½	3/4 8/4 5/8 5/8 1/2 1/2

The spacing of the rivets longitudinally in structural shapes depends on the loads to be carried. In ship work the rivet spacing in frames, beams and stiffeners is given in the classification rules (Lloyds or American Bureau of Shipping) under which the ship is built.

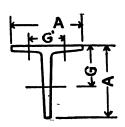
For spacing in riveted joints see page 276.

#### CHANNELS

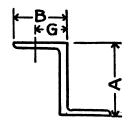


Depth of channel and weight	Gage G	Max. rivet in flange	Depth of channel and weight	Gage G	Max. rivet in flange
15 { 50-55 lb. 33-45 lb.	21/2	₹8	8 { 16.25-21.25	1½ 1¾ 1¾8	3/4
13 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	284 21/2 2 18/4 11/2 11/6	7/8	$7 \begin{cases} 17.25-19.75 \\ 9.75-14.75 \\ 6 \begin{cases} 13 & -15.5 \\ 8 & -10.5 \end{cases}$	1 1 1 2 1 1 1 3 8 1 1 8	5/8 5/8 
$9 \begin{cases} 20 \text{ to } 25 \\ 13.25 \text{ to } 15 \end{cases}$	13%	<b>^</b>			::::

[Carnegie Steel Co., Pittsburgh, Pa.]



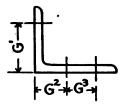
		TE	ES		
A	G	G′	A	G	G'
$   \begin{array}{c}     4 \\     3\frac{1}{2} \\     2\frac{3}{4} \\     2\frac{1}{2}   \end{array} $	21/4 2 17/8 13/8	2 1 <sup>8</sup> / <sub>4</sub> 1 <sup>3</sup> / <sub>8</sub> 1 <sup>1</sup> / <sub>4</sub>	2½ 2 1½ ···	11/4 11/8 3/4	1½ 1 3⁄4



ZEES

A	В	G	A	В	G
6 5	3½ 3¼	2 1¾	4 3	3 23/4	13/4 11/2

ANGLES



Leg	8 41/2	7	$\begin{vmatrix} 6 \\ 3 \frac{1}{2} \end{vmatrix}$	5 3	4 21/2	31/2	3 13⁄4	2½ 1¾8	2 1½	13⁄4 1	11/2	13/8	1 ½ 3⁄4	1 5⁄8	3/4 1/2
$G^2$ $G^3$ Max. rivet	3 1½8	2½ 3 1	$\frac{2\frac{1}{2}}{2\frac{1}{4}}$	1 3/4 7/8	7/8	7/8	···· 7⁄8	3/4	 5⁄8	1/2	3/8	 3/8	 3⁄8	 1∕4	 !⁄4

For column details 6' leg ( $\frac{1}{2}$  inch thick or less) against column shaft  $G^2 = \frac{1}{4}$ ',  $G^3 = 3$ '.

For diagonal angles, etc., gauge in middle, where riveted leg equals or exceeds 3" for  $\frac{3}{2}$ " rivets,  $\frac{3}{2}$ " for  $\frac{7}{2}$ " rivets.

#### RIVET SPACING

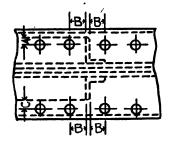
RIVETS IN CRIMPED ANGLES



Distance A should never be less than 2 ins. This applies to button, pan and countersunk head rivets, and also whether angles are watertight or non-watertight.

See also pages 276 and 286.

#### CLEARANCE FOR COVER PLATE RIVETING

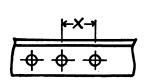


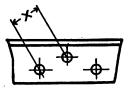
#### CLEARANCE FOR WEB RIVETING

Minimum A	Standard A
7/8" 1 11/8 11/4 13/8	1½8" for 5%" rivets 1¼ " 3¼ " " 1¾6 " ½8 " 1½ " 1 " " 1½ " 1 " " 1½ " 1½ "



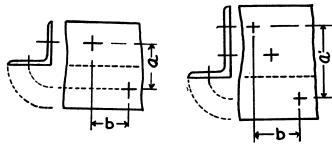
#### MINIMUM RIVET SPACING





Dia. of rivetX minimum		3/8 11/4	1½ 1¾	25/8	3/4 21/4	7/8 25/8	1 3	1½ 3¾
2 mmmum	1	174	174	4	274	278	J	1 228

#### STAGGER OF RIVETS TO MAINTAIN NET SECTION Am. Bridge Co.—Standard



One hole out

Two holes out

a = sum of gauges minus thickness of angle.

$$y = diameter of rivet + \frac{1}{8}$$

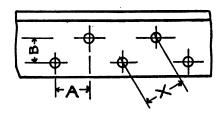
$$a - y = \sqrt{a^2 + b^2 - 2y}$$
  $a^1 - 2y = \sqrt{a^2 + b^2 - 3y}$   
 $b = \sqrt{2ay + y^2}$   $b = \sqrt{2ay + y^2}$ 

$$b = \sqrt{2av + v^2}$$

#### Dimensions in inches

a	Rivet	7'8" Rivet	81	Rivet	Rivet	
1 1½2 2 2½ 3 3½ 4 4½	$\begin{array}{c} 15 \\ 8 \\ 17 \\ 8 \\ 2! \\ 16 \\ 2! \\ 4 \\ 27! \\ 6 \\ 29! \\ 6 \\ 2^{13} \\ 16 \\ 2^{15} \\ 16 \end{array}$	13/4 2 21/4 27/6 25/8 213/6 3 33/6	5 5½ 6 6½ 7 7½ 8 8½	3 <sup>1</sup> / <sub>16</sub> 3 <sup>1</sup> / <sub>4</sub> 3 <sup>3</sup> / <sub>8</sub> 3 <sup>1</sup> / <sub>2</sub> 3 <sup>5</sup> / <sub>8</sub> 3 <sup>3</sup> / <sub>4</sub> 3 <sup>7</sup> / <sub>8</sub>	35/16 31/2 35/8 33/4 37/8 41/8 41/4	5%" rivets can be taken at ½" less than for ¾", and 1" rivets at ½" more than for ½"

#### DISTANCE CENTER TO CENTER OF STAGGERED RIVETS

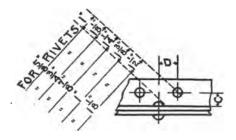


#### All dimensions in inches

#### Values of X for varying values of A and B

Value	Values of B													
of A  11/8 11/4 13/8 11/5 11/8 21/8 21/8 21/4 23/8 21/2	78 1716 1916 158 134 178 1156 2116 2316 2516 212 258	1 1158 1116 1136 178 2 218 214 256 216 226 216 2116	11/8 19/6 11/6 13/4 17/8 2 21/6 28/6 28/6 28/8 21/2 25/8 23/4	$\begin{array}{c} 1 \frac{1}{4} \\ 1^{11} \frac{1}{6} \\ 1^{3} \frac{1}{4} \\ 1^{7} \frac{1}{8} \\ 1^{15} \frac{1}{6} \\ 2^{1} \frac{1}{6} \\ 2^{1} \frac{1}{6} \\ 2^{11} \frac{1}{6} \\ 2^{11} \frac{1}{6} \\ 2^{13} \frac{1}{6} \end{array}$	$\begin{array}{c} 138 \\ 134 \\ 178 \\ 178 \\ 2 \\ 218 \\ 276 \\ 276 \\ 278 \\ 234 \\ 278 \end{array}$	$\begin{array}{c} 1\frac{1}{2}\\ 178\\ 178\\ 2\\ 2\frac{1}{5}6\\ 2\\ 2\frac{1}{5}6\\ 2\frac{3}{5}6\\ 2\frac{1}{2}\\ 2\frac{1}{5}8\\ 2\frac{1}{5}6\\ 2$	15/8 2 21/6 21/8 23/8 23/8 21/6 21/6 23/4 21/8 23/4 23/8	134 21/48 21/8 25/60 25/60 25/8 27/60 25/8 27/8 215/6 31/6	17/8 23/6 23/6 23/8 21/2 29/6 25/8 213/6 213/6 213/6 31/8	2 25/6 23/8 27/6 25/8 23/4 215/6 3 31/8 33/8 33/8	21/8 23/8 27/6 21/2 25/8 211/6 21/8 21/6 31/6 31/6 31/6 31/4	21/4 21/2 29/6 21/6 21/8 21/8 21/8 31/6 31/6 33/8 33/8 33/8	25.8 21.5 21.5 21.5 21.5 33.6 33.6 33.6 33.6 33.6 33.6	213 213 213 213 213 314 314 314 314 314 314 314

#### MINIMUM STAGGER FOR RIVETS

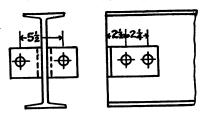


						Min	imu	m sta	gger	D, i	18.					
Dia. of Rivet		C, ins.														
	11/8	13/16	11/4	15/6	13/8	11/16	11/2	1%	15%	111/16	1¾	113/16	1 7/8	115/6	21/16	23/6
\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	15/16 11/2 11/2 1 13/16 21/16	7/8 13/6 17/6 13/4 2	13/16 11/8 13/8 111/6 1 15/6	11/6 11/6 15/6 15/6 15/8	15/6 11/4 19/6 17/8	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3/4 11/6 11/6 13/4	%6 1 13% 1 11%	15/6 15/6 15/6 15/8	18/16 18/16 19/16	5/8 11/8 11/2	7/6 1 13%	7/8 15/16	11/4	1	11/6

#### BEAM CONNECTIONS

5", 6" and 7" beams

2 angles  $6'' \times 4'' \times \frac{3}{8}'' \times 3''$ , wt. 7 lbs.



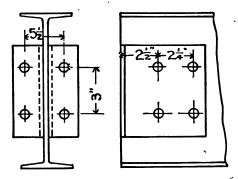
12" I beam connections two angles  $4" \times 4" \times \frac{7}{16}" \times 8\frac{1}{2}"$  wt. 17 lbs., 3 rivets 3" pitch

15", 18", 20" beam connections two angles  $4" \times 4" \times \frac{7}{6}" \times 11\frac{1}{2}"$  wt. 23 fbs., 4 rivets 3" pitch

21" beam connections two angles 4"  $\times$  4"  $\times$  ½"  $\times$  1"—2½" wt. 33 fbs., 5 rivets 3" pitch

8", 9" and 10" beams

2 angles  $6'' \times 4'' \times \frac{3}{8}'' \times 5\frac{1}{2}''$ , wt. 13 fbs.



24" beam connections two angles 4"×4"×½"×1"—5½" wt. 39 lbs., 6 rivets 3" pitch

27" beam connections two angles 4"  $\times$  4"  $\times$  ½"  $\times$  1"-8½" wt. 46 fbs., 7 rivets 3" pitch

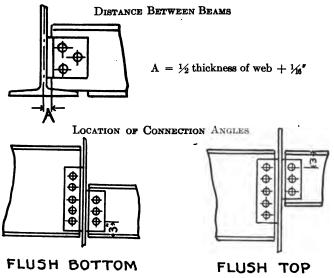
Rivets and bolts 3/4" diameter

Weights given are for ¾" shop rivets and angle connections, about 20% should be added for field rivets or bolts.

LIMITING VALUES OF BEAM CONNECTIONS

		Value of web con-	Values	of outst	anding	legs of con	nection s	ngles
1 150	ams	nection	Fie	eld rivets		F	ield bolts	
Depth ins.	Weight lbs. per ft.	Shop rivets in enclosed bearing lbs.	in. rivets or turned bolts single shear lbs.	Mini- mum allow- able span in ft. uniform load	t in.	¾ in. rough bolts single shear lbs.	Mini- mum allow- able span in ft. uniform load	t in.
27	90	82530	61900	18.9	5/8	49500	23.6	5/8
24	80	67500	53000	17.5	5/8	<b>42400</b>	21.9	5%
21	601/2	48150	44200	14.2	5/8	35300	17.8	5/8
20	65	45000	35300	17.6	5/8	28300	22.1	5/8
18	55	41400	35300	13.3	5/8	28300	16.7	5/8
15	42	36900	35300	8.9	5/8	28300	11.1	5/8
12	31½	23600	26500	8.1	%	21200	9.0	5/8
10	25	27900	17700	7.4	5/8	14100	9.2	5/8
9	21	26100	17700	5.7	5/8	14100	7.1	5/8
9 8 7	18	24300	17700	4.3	0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,	14100	5.4	\$\\$\\$\\$\\$\\$\\$\\$\\$\\$\\$\\$\\$\\$\\$\\$\\$\\$\\$\
7	15	11300	8800.	6.2	5/8	7100	7.8	5/8
6	$12\frac{1}{4}$	10400	8800	4.4	5/8	7100	5.5	5/8
5	934	9500	8800	2.9	5/8	7100	3.6	5/8

t = web thickness in bearing to develop max. allowable reactions when beams frame opposite. [Pocket Companion, Carnegie Steel Co.]



#### SECTION VIII

#### **USEFUL TABLES**

WEIGHTS AND MEASURES — METRIC SYSTEM — METRIC AND U.S.
EQUIVALENT MEASURES—DECIMAL EQUIVALENTS OF AN INCH—
INCHES AND FRACTIONS IN DECIMALS OF A FOOT—STRENGTH
OF MATERIALS—SPECIFIC GRAVITIES AND WEIGHTS OF
MATERIALS—EQUIVALENT VALUES OF ELECTRICAL,
MECHANICAL AND HEAT UNITS

### WEIGHTS AND MEASURES (United States and Great Britain)

#### TROY WEIGHT

24 grains = 1 pennyweight (pwt.) 20 pwts. = 1 ounce

= 1 pound

#### 12 ounces = 1 pound

20 grains = 1 scruple 8 drams = 1 ounce 3 scruples = 1 dram 12 ounces = 1 pound

#### AVOIRDUPOIS WEIGHT

APOTHECARIES' WEIGHT

16 drams = 1 ounce 2000 pounds = 1 short ton 16 ounces = 1 pound 2240 pounds = 1 long ton

#### SHIPPING WEIGHT

28 pounds = 1 quarter 4 quarters or 112 pounds = 1 hundredweight (cwt.) 20 cwt.

2240 pounds = 1 ton.

16 ounces

#### LINEAR MEASURE (Land)

12 inches = 1 foot 40 rods = 1 furlong 3 feet = 1 yard 8 furlongs  $5\frac{1}{2}$  yards = 1 rod 0r 5280 ft. = 1 mile

294

#### LINEAR MEASURE (Nautical)

6 feet = 1 fathom 6080 feet = 1 nautical mile or knot

120 fathoms = 1 cable length 3 knots = 1 league

#### SQUARE MEASURE

144 square inches = 1 square foot 40 square rods = 1 rood 9 square feet = 1 square yard 4 roods = 1 acre 30½ square yards = 1 square rod 640 acres = 1 square mile

#### TIME MEASURE

60 seconds = 1 minute 24 hours = 1 day 60 minutes = 1 hour 7 days = 1 week

28, 29, 30 or 31 days = 1 calender month (30 days = 1 month in computing interest)

365 days = 1 year

366 days = 1 leap year

#### CIRCULAR MEASURE

60 seconds = 1 minute 90 degrees = 1 quadrant

60 minutes = 1 degree 360 degrees = 1 circumference

Instead of an angle being given in degrees it can be given in radians, one radian being equal to the arc of a circle whose length is the radius. Thus if R denotes the radius, the circumference of the circle  $2\pi$  R, then the circular measure of  $90 = \frac{1/4 \times 2\pi}{R} = \frac{\pi}{2}$ ;

similarly the circular measure of  $180^{\circ} = \pi$ ;  $60^{\circ} = \frac{\pi}{3}$  &c.

#### DRY MEASURE

2 pints = 1 quart 4 pecks = 1 bushel 8 quarts = 1 peck 36 bushels = 1 chaldron

One United States struck bushel contains 2150.42 cu. ins. or 1.244 cu. ft. A British bushel contains 2218.19 cu. ins. or 1.2837 cu. ft. or 1.032 U. S. bushels.

#### LIQUID MEASURE

4 gills = 1 pint  $31\frac{1}{2}$  gallons = 1 barrel

2 pints = 1 quart 2 barrels or 63 gallons = 1 hogs-

4 quarts = 1 gallon head

One United States gallon contains 231 cu. ins. or .134 cu. ft. or 1 cu. ft. = 7.481 gallons. One British Imperial gallon both liquid and dry contains 277.27 cu. ins. or .160 cu. ft.

#### 296

#### BOARD MEASURE

To find the number of feet board measure in a stick of timber, multiply the length in feet, by the breadth in feet, by the thickness in inches.

Example. Find the board measure of a piece of timber 20 ft. long, 2 ft. wide by 2 ins. thick.

20 ft.  $\times$  2 ft.  $\times$  2 ins. = 80 ft. board measure

#### CUBIC MEASURE

1,728 cubic inches = 1 cubic foot
27 cubic feet = 1 cubic yard
128 cubic feet = 1 cord of wood

#### SURVEYOR'S OR GUNTER'S MEASURE

7.92 inches = 1 link 4 rods = 1 chain 25 links = 1 rod 80 chains = 1 mile

#### METRIC SYSTEM

The fundamental units are—meter for length, liter for volume and gram for weight. Multiples are obtained by prefixing deka (10), hekto (100) and kilo (1,000), and divisions by deci (1/10), centi (1/100) and milli (1/1000). Abbreviations of the multiples begin with a capital letter, and of the divisions with a small.

#### MEASURES OF LENGTH

10 millimeters (mm.)	=	1 centimeter	cm.
10 centimeters	=	1 decimeter	dm.
10 decimeters	=	1 meter	m.
10 meters	=	1 dekameter	Dm.
10 dekameters	=	1 hektometer	Hm.
10 hektometers	=	1 kilometer	Km.

#### MEASURES OF SURFACE (NOT LAND)

100 square millimeters (mm.2)	=	1 square centimeter	cm.²
100 square centimeters	=	1 square decimeter	dm.²
100 square decimeters	=	1 square meter	m.2

#### MEASURES OF VOLUME

1000 cubic millimeters (mm. <sup>3</sup> )	=	1 cubic centimeter	cm.8
1000 cubic centimeters	=	1 cubic decimeter	dm.8
1000 cubic decimeters	=	1 cubic meter	m.3

#### MEASURES OF CAPACITY

10 mililiters (ml.)	=	1 centiliter	cl.
10 centiliters	=	1 deciliter	dl.
10 deciliters	=	1 liter	1.
10 liters	=	1 dekaliter	Dl.
10 dekaliters	===	1 hekoliter	Hl.
10 hekoliters	==	1 kiloliter	Kl.

Note.—The liter is equal to the volume occupied by 1 cubic decimeter.

#### MEASURES OF WEIGHT

10 milligrams (mg )	=	1 centigram		cg.
10 centigrams	=	1 decigram		dg.
10 decigrams	=	1 gram		g.
10 grams		1 dekagram		Dg.
10 dekagrams	=	1 hektogram		Hg.
10 hektograms	=	1 kilogram	•	Kg.
1000 kilograms	=	1 ton		T.

Note.—The gram is the weight of one cubic centimeter of pure distilled water at a temperature of 39.2° F., the kilogram, is the weight of 1 liter of water, the ton is the weight of 1 cubic meter of water.

Equivalent Values of Metric and United States (Great Britain) Measures

#### MEASURES OF LENGTH

#### MEASURES OF SURFACE

1 square meter =  $\begin{cases} 10.764 \text{ square feet} \\ 1.196 \text{ square yards} \end{cases}$ 1 square centimeter = .155 square inch. 1 square millimeter = .00155 square inch

1 square yard = .836 square meter 1 square foot = .0929 square meter

1 square inch =  $\begin{cases} 6.452 \text{ sq. centimeters} \\ 645.2 \text{ sq. millimeters} \end{cases}$ 

#### MEASURES OF VOLUME AND CAPACITY

1 cubic meter = {35.314 cubic feet 1.308 cubic yards 264.2 gallons (231 cubic inch)

1 cubic decimeter =  $\begin{cases} 61.023 \text{ cubic inch} \\ .0353 \text{ cubic feet} \end{cases}$ 

1 cubic centimeter = .061 cubic inch

1 cubic decimeter 61.023 cubic inches .0353 cubic foot 1 liter = { 1.0567 quarts (U. S.) .2642 gallon (U. S.) 2.202 lbs. of water at 62° F.

1 cubic yard = .7645 cubic meter

1 cubic foot =  $\begin{cases} .02832 \text{ cubic meter} \\ 28.317 \text{ cubic decimeters} \\ 28.317 \text{ liters} \end{cases}$ 

1 cubic inch = 16.393 cubic centimeters

1 gallon (British) = 4.543 liters

#### 1 gallon (U. S.) = 3.785 liters

MEASURES OF WEIGHT

1 gram = 15.432 grains

1 kilogram = 2.2046 pounds

(.9842 ton of 2240 lbs.

1 metric ton =  $\begin{cases} 19.68 \text{ cwts.} \\ 2204.6 \text{ lbs.} \end{cases}$ 

1 grain = .0648 gram

1 ounce avoirdupois = 28.35 grams

1 pound = .4536 kilogram

1 ton of 2240 lbs. =  $\begin{cases} 1.016 \text{ metric ton} \\ 1016 \text{ kilograms} \end{cases}$ 

#### MISCELLANEOUS

1 kilogram per meter = .6720 pounds per foot

1 gram per square millimeter = 1.422 pounds per square inch

1 kilogram per square meter = 0.2084 pounds per square foot

1 kilogram per cubic meter = .0624 pounds per cubic foot

- 1 degree centigrade = 1.8 degrees Fahrenheit
- 1 pound per foot = 1.488 kilograms per meter
- 1 pound per square foot = 4.882 kilograms per square meter
- 1 pound per cubic foot = 16.02 kilograms per cubic meter
- 1 degree Fahrenheit = .5556 degrees centigrade
- 1 Calorie (French Thermal Unit) = 3.968 B. T. U. (British Thermal Unit)
- 1 Horse Power =  $\begin{cases} 33,000 \text{ foot pounds per minute} \\ 746 \text{ Watts} \end{cases}$
- 1 Watt (Unit of Electrical Power) =  $\begin{cases} .00134 \text{ Horse Power} \\ 44.22 \text{ foot pounds per minute} \end{cases}$ (1000 Watts
  - $1 \text{ Kilowatt} = \begin{cases} 1000 \text{ Watts} \\ 1.34 \text{ Horse Power} \\ 44220 \text{ foot pounds per minute} \end{cases}$

#### Conversion Table of Inches and Feet to Millimeters, Centimeters and Meters

Inches	Feet	Milli- meters	Centi- meters	Me- ters	Inches	Feet	Milli- meters	Centi- meters	Me- ters
15.6 11.6 11.6 11.6 11.6 11.6 11.6 22.6 22	1/2	23.8 25.4 30.1 36.5 38.1 42.9 49.2 55.5 61.9 63.5 74.6 20.8 87.3 88.9 71.0 101.6 104.7 111.3 117.8 127.0 152.4 228.6 224.0	2.38 2.54 3.61 3.65 3.81 4.29 5.78 5.55 6.19 6.35 6.83 7.46 7.62 8.73 8.89 9.87 10.00 10.14 11.73 11.73 11.73 20.32 22.86 25.49 27.94	.023 .025 .030 .036 .038 .042 .049 .050 .055 .061 .063 .068 .074 .076 .087 .089 .093 .100 .101 .114 .117 .123 .127 .1228 .228 .259	14 16 18 20 22 24 26 30 32 34 38 40 42 44 48 50 52 54 66 68 70 72	11½ 2 2½ 3 33½ 4 4½ 5 5½ 6 7 8	355. 6 406. 4 457. 2 508. 0 558. 8 609. 6 660. 4 711. 2 762. 0 812. 8 863. 6 914. 4 965. 2 1016. 0 1168. 4 1177. 6 1129. 2 1270. 0 1320. 8 1371. 6 1422. 4 1473. 2 1524. 0 1574. 8 1676. 4 1777. 2 1778. 8 1828. 8 2133. 6	35.56 40.64 45.72 50.80 55.88 60.96 66.04 71.12 76.20 81.28 86.36 91.44 96.52 101.80 111.76 111.76 1121.92 127.00 132.08 137.16 142.24 147.32 152.40 157.48 167.64 167.64 172.72 177.88 182.88 213.36	355 406 457 508 558 8609 860 711 762 812 863 914 965 1 016 1 117 1 168 1 219 1 370 1 371 1 524 1 1574 1 1778 1 1778 1 1778 1 1778 1 1828 2 133 2 438

#### HANDBOOK OF STANDARD DETAILS

### DECIMAL EQUIVALENTS OF AN INCH AND MILLIMETER-INCH CONVERSION TABLE

Fract.	Dec.	MM.	Fract.	Dec.	MM.	MM.	Dec. Inch	MM.	Dec. Inch
% %	.015625	.397	17/4	.515625	13.1	1	.039370	51	2.007892
^ <b>™</b> 1∠	.03125	.79	172	.53125	13.49	2	.078740	52	2.047262
/AL	.00120		<b>~</b>	.00120	10.10	3	.118110	53	2.086632
<b>1</b> 64	.046875	1.19	25/4	.546875	13.89	4	.157480	54	2.126002
1/4	.0625	1.59	%	.5625	14.29	5	.196850	55	2.165372
						6	.236220	56	2.204742
4	.078125	1.98	87/4	.578125	14.68	7	.275509	57	2.244112
34	.09375	2.38	87/64 19/52 /	.59375	15.08	8	.314960	58	2.283482
						9	.354330	59	2.322852
64	. 109375	2.77	3964	. 609375	15.48	10	.393704	60	- 2.362226
1/8	. 125	3.17	5/8	.625	15.87	11	.433074	61	2.401596
						12	.472444	62	2.440966
4	. 140625	3.57	41/64	.640625	16.27	13	.511814	63	2.480336
**±	. 15625	3.97	41/64	.65625	16.7	14	.551184	64	2.519706
i						15	.590554	65	2.559076
164	. 171875	4.37	4%	.671875	17.06	16	. 629924	66	2.598446
. 1						17	.669294	67	2.637816
³ <b>∕</b> 6	. 1875	4.76	11/16	.6875	17.46	18	.708664	68	2.677186
4. "	.203125	5.16	4564 29/53	.703125	17.86	19	.748034	69	2.716556
~ ½	. 21875	5.56	7%	.71875	18.26	20	.787409	70	2.755930
I						21	.826779	71	2.795300
×4	. 234375	5.95	4764	.734375	18.65	22	.866149	72	2.834670
1/4	. 25	6.35	*	.75	19.05	23	.905519	73	2.874040
ا بـ			ا بسا			24	.944889	74	2.913410
764	. 265625	6.75	4964	.765625	19.45	25	.984259	75	2.952780
ایر	00105		ايسا	20102	40.04	26	1.023629	76	2.992150
<u>,</u> %	.28125	7.14	35%	.78125	19.84	27	1.062999	77	3.031520
%i	.296875	7.54	51/64	.796875	20.24	28	1.102369	78	3.078090
	.3125	7 04	19.	.8125	20.64	29 30	1.141739 1.181113	79 80	3.110260
5/16	.3125	7.94	13/16	.8125	20.04	31			3.149635
1/	.328125	0 22	53/	.828125	21.03	32	1.220483	81	3.189005
164 11 <sub>62</sub>	.34375	8.33 8.73	53/4 37/63	.84375	21.43	33	1.259853	82 83	3.228375 3.267745
-712	.04010	0.13	"/ts	.0%373	21.90	34	1.338593	84	3.307115
%4	.359375	9.13	55/64	.859375	21.83	35	1.377963	85	3.306485
784 3/8	.375	9.13	784 7/8	.875	22.22	36	1.417333	86	3.385855
78	.010	9.52	/8	.010	22.22	37	1.456703	87	3.425225
564	.390625	9.92	57/64	.890625	22.62	38	1.496073	88	3.464595
784	. 380023	9.92	784	.090020	20.02	39	1.535443	89	3.503965
13/4	.40625	10.32	29/2	.90625	23.02	40	1.574817	96	3.543339
764 782	421875	10.72	59/4	.921875	23.41	41	1.614187	l šĭ l	3.582709
784	.421010	10.72	764	.921010	20.41	42	1.653557	92	3.622079
7∕6	.4375	11.11	15/16	.9375	23.81	43	1.692927	93	3.661449
	. 2010	44.41		.00.0	-0.01	44	1.732297	94	3.700819
19 <sub>4</sub>	.453125	11.51	61/64	.953125	24.21	45	1.771667	95	3.740189
15/ <sub>22</sub>	.46875	11.91	8142	.96875	24.61	46	1.811037	96	3.779559
		12.01	′.34			47	1.850407	97	3.818929
1/4	.484375	12.30	63/64	.984375	25	48	1.889777	98	3.858299
~ ½	.5	12.7	<sup>764</sup> 1		25.4001	49	1.929147	99	3.897669
/4						50	1.968522	100	3.937043

#### USEFUL TABLES

#### Inches and Fractions in Decimals of a Foot

Inches and	Decimals of a	Inches and	Decimals of a	and	Decimals of a	and	Decimals of a
fractions	foot	fractions	foot	fractions	foot	fractions	foot
140	.0052	31/16	.2552	61/16	. 5052	9116	.7552
116 18 316	.0104	31/8	.2604	61/8	.5104	918	.7604
8%	.0156	33/16	.2656	63/16	.5156	93 16	.76562
1/2	.0208	31/4	.2708	61/4	.5208	91/4	.77080
52	.0260	06.7	.2760	06.7	.5260	06.2	.77600
3/2	.0312	الإدمة	.2812	63%	.5312	93/8	.78125
78	.0364	ຄ້າ	.2865	27 /	.5364	077	.7865
1/6	.0417	31/2	.2917	61/2	.5417	91/16	.7917
9/2		3916	.2968		.5468	09.7	.7968
716 57	.0468 .0521		.3021	6 <sup>9</sup> 16 6 <sup>5</sup> /8	.5521	95/8	.8021
78		35/8 311/6		611/		911/6	.8073
3 16	.0573	المواد	.3073	63/6	.5573	- 10	.8125
13/	.0625	3%	.3125	634	.5625	9 <sup>3</sup> / <sub>4</sub> 9 <sup>13</sup> / <sub>6</sub>	.8177
716	.0677	31376	.3177	613/16	.5677	978	
15/8	.0729	37/8	.3229	67/8	.5729		.8229
15/16	.0781	31516	.3281	61516	.5781	915 16	.8281
1	.0833	4	.3333	7	.5833	10	.8333
11/16	.0885	41/16	.3385	71/16	.5885	101/16	.8385
11/8	.0937	41/8	.3437	71/8	.5937	101/8	.8437
13/16	.0990	43/16	.3490	73/16	.5990	103/16	.8490
1/4	.1042	41/4	.3542	71/4	.6042	101/4	.8542
15/16	.1093	45/16	.3593	7516	.6093	$10^{5}_{16}$	.8593
13/8	.1146	43/8	.3646	73/8	.6146	103/8	.8646
1/16	.1198	47/16	.3698	71/16	.6198	$10^{7}$ /16	.8698
11/2 19/16	.1250	41/2	.3750	71/2	.6250	101/2	.8750
19/16	.1302	4916	.3802	79/16	.6302	$10\frac{9}{16}$	.8802
1%	. 1354	45/8	.3854	75/8	.6354	105/8	.8854
111/16	.1406	411/16	.3906	71116	.6406	1011/6	.8906
134	.1458	43/4	.3958	73/4	.6458	103/4	.8958
113/16	.1510	413/16	.4010	713/16	.6510	1013/6	.9010
17/8	.1562	47/8	.4062	71/8	.6562	10%	.9062
115/16	. 1615	415 16	.4114	715/16	.6615	1015/16	.9115
2	. 1667	5	.4167	8	.6667	11	.9167
$2^{1}/_{6}$	.1718	51/16	.4218	81/16	.6718	111/16	.9218
21/8	.1771	51/8	.4271	81/8	.6771	111/8'	.9271
$2\frac{3}{16}$	.1823	53/16	.4323	83/16	.6823	113/6	.9323
21/4	.1875	$5\frac{1}{4}$	.4375	81/4	.6875	111/4	. 9375
$2^{5}_{16}$	. 1927	55/16	.4427	85/16	.6927	115/6	.9427
23/8	.1979	$5\frac{3}{8}$	.4479	83/8	.6979	113%	.9479
$27_{16}$	.2031	57/16	.4531	87/16	.7031	111/16	. 9531
$2\frac{1}{2}$	.2083	$5\frac{1}{2}$	.4583	81/2	.7083	111/2	. 9583
$2^{9}/_{16}$	.2135	59/16	.4635	89/16	.7135	11½ 11½	.9635
25%	.2187	55/8	.4687	85%	.7187	115%	.9687
211/16	.2240	511/16	.4740	811/6	.7240	1111/6	.9740
$2\frac{3}{4}$	.2292	534	.4792	83/4	.7292	1134	.9792
213/16	.2343	51316	.4843	81316	.7343	111376	.9843
21/8	.2395	57/8	.4896	87/8	.7396	$11\frac{94}{11}$ $11\frac{13}{16}$ $11\frac{7}{8}$	.9896
215/16	.2448	515/16	.4948	815/16	.7448	1115/6	.9948
3	.2500	6	.5000	9 10	.7500		1.0000

Strength of Materials Stresses per Square Inch

		Stresses in thousands of pounds	thousands	punod jo			
Material	Tension ultimate	Elastic limit	Com- pression ultimate	Bending	Shearing	Modulus of elasticity pounds	Elongation %
1 :	15	16-30	12		12	11,000,000	
Aluminum, wife, Aluminum bronze, 5 to 7½ al. Brass, cast.	18-24	909	120	20	36	9,000,000	
Brass, wife Bronze, manganese cast, 105 tin, 25 mm. Bronze, manganese rolled, 105 tin, 25 mm. Bronze, phosphor cast, 95 tin, 15 P.	88525	808 74	125				
bronze, prosphor wree, 3, tal., 12% tin, 25% P. Bronze, Tobin, cast, 38% zine, 135% tin, 25% P. Bronze, Tobin, rolled, 38% zine, 125% tin, 25% P. Bronze, 8% tin.	28.88 2.52 2.53 2.53	190	212	43.7	18.90	4,500,000	70
Cast from, gormon Cast from, malleable Copper, cast	18-24 27-35 25	15-20	46	25.82	30	10,000,000	
Copper, wire Skeel shapes. Skeel invets Skeel crattings (medium) Wrought iron	28-68 25-65 48 48	15 tensile 15 tensile 31.5 26	tensile tensile tensile tensile	tensile tensile tensile	% tensile % tensile % tensile 5-6 tensile	29,000,000 29,000,000 29,000,000 28,000,000	25.9-22.1 27.3-23.0 18

# Specific Gravities and Weights of Materials Metals and alloys

		METALS	METALS AND ALLOIS		
Substance	Specific gravity	Wt. per cu. ft. lbs.	Substance	Specific gravity	Wt. per cu. ft. lbs.
Aluminum, cast-hammered Aluminum, bronze Brass, cast-colled Bronze, 7.9 to 14; tin Copper, cast-colled Gold, cast-hämmered Iron, cast. Iron, wrought Lead Manganese Mercury	2.6 7.4-7.9 8.5 7.4-7.9 10.0 17.2 7.6-7.9 11.37 7.11.37	165 481 534 538 1205 1205 450 471 849	Nickel Platinum, cast-hammered Silver, cast-hammered Steel, tool Tit, cast-hammered Tit, cast-hammered Zinc, cast-rolled	8.9 21.5 10.5 7.72 7.3	537 1330 656 459 440

# TIMBER, U. S. SEASONED 15 to 20%-moisture

		77 M OT	omognation of on or		
Ash, white-red	.6265	9	Maple, white	53.	33
Cedar, white-red	.3238	22	Oak, live	95	20
Chestnut	8.	41	Oak, chestnut	88	72
Cypress	.48	8	Pine, Oregon	.51	32
fir, Douglas	.51	31	Pine, white	.41	56
Ar, Eastern	<b>4</b> .	22	Pine, long leaf yellow	20	4
Hemlock	2	8	Pine, short leaf yellow	.61	88
Hickory	69	48	Spruce	44	27
Cocust	.67	46	Teak, African	86	62
Mahogany	٠ <del>۲</del> . 8. <del>۲</del> .	44	Walnut, black	.6	8

# MISCELLANEOUS MATERIALS

tter, fresh, 4° C max, dens	1.0	62.42	Petroleum, gasoline	775	45
Water salt	02-1 03	64	Cement, Portland, loose.	1.4	00
	00 00	1	Con anthuments		200
	0000.	10	Coarl anturacine	1.4-1.1	16
roleum	.87	54	Coal, bituminous	1.2-1.5	84

#### 304 HANDBOOK OF STANDARD DETAILS

#### EQUIVALENT VALUES OF MECHANICAL, ELECTRICAL AND HEAT UNITS

Unit Equivalent value in other units

1 Ft. lb. 1.3558 joules

.0000003766 K. W. hour

.0012861 B. T. U.

1 H. P. 745.7 watts

.7457 K. W.

33,000 ft. lbs. per min. 42.44 B. T. U. per min.

2.62 lbs. water evap. per hour from and at 212

degs. F.

1 Kilowatt 1,000 watts

1.3410 horse power 44,253 ft. lbs. per min. 56.92 B. T. U. per min.

3.52 lbs. water evap. per hour from and at

212 degs. F.

1 Joule 1 watt second

.000000278 K. W. hour .0009486 B. T. U. .73756 ft. lb.

1 lb. of water evap. from and at 212 degs. F. .2841 K. W. hour .3811 H. P. hour 970.4 B. T. U.

1,023,000 joules 754,525 ft. lbs.

1 B. T. U. 1,054.2 watt seconds

777.54 ft. lbs.

.0002928 K. W. hour .0003927 H. P. hour

#### INDEX

Abbreviations, 1, 66, 277	Birmingham wire and sheet gauges, 284
Acme threads, 64	Block chain, 132
Addendum (gear teeth), 141, 145, 146	Boiler patch bolts, 34
American system of rope transmission,	stay bolts, 34
129	tubes, 167, 168
wire gauge, 284	Bolt, bolts, 25–35
Anchor chain, 222, 223	ends of, 28, 265
shackle, 214, 215	heads for T slots, 89
swivel. 222	measurement of, 25
Angle, angles:	strength of, 59
couplings, 254–257	U. S. threads for, 59
equal leg, structural, 278–279	Board measure, 296
laying off, 23	Box wrench, 239
punching of, 288	Brads, 78, 79
unequal leg, structural, 283	Brass, composition of, 263
valves, 183, 187	tubes, 176
Annealing chain, 221	Bridle slings, 218–220
steel, 226	Briggs pipe thread, 71, 72
Apothecaries' weight, 294	British Association thread, 62
Area, metric measures of, 296	fine threads, 61, 62
U. S. measures of, 295	thermal unit, 304
Avoirdupois weight, 294	Brown and Sharpe screw gauge, 43
	sheet and wire gauge, 284
Balata belts, 120	Bushings, finished ends of, 266
Bar steel, weight of, 285	Butt welded pipe, 162
Beam, beams:	Buttress threads, 64
connections, 292, 293	Buttstrap, riveting of, 276
gauges for punching, 286	
I, 280, 281	Canvas belts, 120
Bearings, 106-109	Cap scréws, 46, 47
Belt, belting:	Capillary oilers, 107
balata, 120	Capstan wheel, 235
canvas, 120	Carriage bolts, 33
drives, 124–127	Case hardening steel, 226
length of, 124	Casing nails, 78, 80
h. p. transmitted by, 120, 121, 124	Cast iron, properties of, 263
leather, 119, 121, 124	flanged fittings, 179–181
ply, 119	flanges, 172
pull, 116	gears, 144, 147, 149
rubber, 119	pulleys, 112–115
widths of, 119, 120	screw fittings, 177, 178
Bends, pipe, 170, 171	sheaves, 127–130
Bevel gears, 150-153	washers, 248

#### INDEX

Cast steel, 226, 263	Couplings, angle, 254-257
Castellated nuts, 29, 38	hose, 76
Castings, shrinkage of, 12	pipe, 166
weight of, 12	shaft, 91, 94–98
Cement coated nails, 77	Crane chain, 222
Centimeters to inches, 299	hook, 213
Chain, chains:	Cranks, 230, 231
anchor, 222, 223	Crest of thread, 59
block, 132	Cross section hatchings, 3
crane, 222	valve, 183
drives, 105	Crossed belts, 124, 125
for transmitting power, 132–138	Crown of pulley, 110, 113-
hoisting, 221–226	Cubic measure, metric, 296
length of, 138	U. S., 296
roller, 133, 134	Cushioned check valve, 183
shackle, 214, 215	Cut nails, 77
silent link, 135–137	Cycloid, construction of, 19
slings, 224	
sprocket wheels, 135–137, 139, 140	Decimal equivalents of scre
swivels, 216	of an inch, 300
Channels, sizes of, 277, 278	Decimals of a foot, inches i
punching of, 286	Deck bolts, 30
Check nuts, 36	Dedendum (gear teeth), 14
valves, 182-187	Diametral pitch, 141
Chords, lengths of, 24	equivalent circular pitch
Chuck screws, squares for, 267	Double angle coupling, 257
Circle, divisions of, 24	belt pulleys, 112
Circular measure. 295	belts, 124
pitch (gears), 141, 145	extra strong pipe, 165
Clearance for cover plate riveting, 289	Drawings, notes on, 1
web riveting, 289	patent office, 9
gear teeth, 141	Drill, drills:
Clevis nuts, 209	for machine screws, 53
Clinch nails, 78, 80	shanks, 245, 246
rings, 249	tap, 60, 77
Clutches, jaw, 103, 104	Drilled holes, 286
split friction, 99-101	Drilling flanges, 172, 173
solid, 101, 102	Drive fit, 6
Coach screws, 51	screws, 48
Coarse threads, 68	Drop flange pulley, 112, 11
Cocks, 192	Drum scores for chain, 224
Cold drawn steel tubes, 168, 169	rope, 225
Collar screws, 53	Dry measure, 295
shaft, 105	
Companion flanges, 172-174	
Composition, 263	Electrical units, 304
Compression couplings, 95–97	Ellipse, construction of, 18
Copper expansion joints, 193	Ends of bolts, 28, 265
tubes, 176	English system rope transm
Cottered joints, 88	Epicycloid, construction of
Cotters, spring, 90	Equalizing thimble, 218

hings, 3 125 10, 113–115 etric, 296, 298 alve, 182 ion of, 19

its of screw gauge, 43 , inches in, 301 eeth), 141 41 lar pitch, 146 ling, 257 e, 165 n, 1 ws, 53 72, 173 , 112, 113 nain, 224, 225

on of, 18 e transmission, 130 uction of, 20 , **21**8

Expansion bends, 170, 171
joints, 193–199
Extra heavy flanged fittings, 181
flanges, 174, 175
screwed fittings, 177
Extra strong wrought iron pipe, 164
Eye bolts, 211
nuts, 41

Face spanner, 240 Fastenings, 25-90 Feet to centimeters, 299 Field rivets, 275 Fine threads, 61, 70 Finish, abbreviation of, 1 of wrenches, 238 Finished ends of bolts, 265 bushings, 266 collars, 266 gears, 266 shafts, 265 Fits, screw threads, 59, 71 shaft, 4, 5, 6, 7 Fittings, pipe: screw, 177, 178 flange, 179-181 Flange couplings, 94 Flanged fittings, 179-181 Flanges, pipe, 172-176 Flexible couplings, 98 Flooring brads, 79 Franklin Institute bolts and nuts, 27 Friction clutches, 99-103

Gate valves, 189-191 Gauge, gauges: for punching, 286-288 screw, 43 sheet metal, 284 wire, 284 Gear, gears: bevel, 150-153 finish of, 266 forms for ordering, 148-150 helical, 161 herringbone, 161 horse power of, 147 materials for, 149 mitre, 150-154 spur, 141-150

Gear, gears:
tooth construction, 142
worm, 156-159
Geometrical constructions, 12-23
Gib head keys, 85
Gibs and keys, 88
Globe valve, 183, 184
Grease cups, 107
Grommets, 217, 219
Grooves for chain, 224, 225
rope, 129, 130, 225

Half round keyways, 88 turn belts, 126 Hand wheels, 232-235 Half round keyways, 88 turn belts, 126 Hand wheels, 232-235 Handles, 227-231 Hanger screws, 47 Hangers, shaft, 91, 109 Hardening steel, 226 Hatchings for sections, 3 Heads, bolt, 26-29, 89 nail, 78 rivet, 269-274 screw, 42, 44, 46, 47 spike, 81-83 Heat unit, B. t. u., 304 Helical gears, 160 Helix angle of thread, 59 Herringbone gears, 161 Hexagon bolts, 26, 27 construction of, 14, 15 nuts, 26, 27, 36, 38 sleeve nuts, 203 Hoisting chains, 221, 222 Hook, hooks: bridle sling, 217, 218 crane, 213 hoist, 212, 226 Horse power: B. t. u. equivalent of, 304 of belts, 120, 121, 124 of chains, 132, 134, 136 of gears, 147 of shafting, 93 transmitted by steel pulleys, 122, 123 Hose couplings, 75 Hyperbola, construction of, 23 Hypocycloid, construction of, 21

I beams, sizes of, 280, 281 Malleable iron, 263 Manila rope, 129 gauges for punching, 286 Imperial wire gauge, 284 Materials: Inch, inches: for bolts, 25 in decimals of a foot, 301 for gears, 149 millimeter conversion table, 299. properties of, 263 300 strength of, 302 Involute: weights of, 303 construction of, 22 Measurement of bolts, screws and rivteeth, 142 ets. 25 Mechanical units, 304 Metric conversion tables, 297-300 Jaw clutch, 103, 104 measures and weights, 296, 297 Joint, length of thread for, 177 screw threads, 63 Millimeter-inch conversion table, 299, , Keys: 300 gib head, 85 Milling cutters, keys for, 88 half round, 88 Minimum rivet spacing, 289 rectangular, 84 Mitre gear, 150, 154 square, 83, 88 Moment of inertia, 277 tapered, 85, 86 Mule stands, 117, 118 Woodruff, 86, 87 Keyways, keyseats, 84, 85, 88, 110, Nails: 111 Kilowatt, 304 brads, 79 Knobs, 236 casing, 80 Knuckle joints, 258 cement coated, 77 Knurled sets, 237 clinch, 80 common, 79 heads and points, 78 Lag screws, 51 penny, 77 Lap joint, 276 roofing, 80 welded pipe, 162 National screw thread commission, 58, welded tubes, 167, 168 66, 74-76 Lead of screw, 58 Nipples, pipe, 75, 166, 167 Leather Belt. See Belt Nuts: Limit standards, 3 castellated, 29, 38 Linear measure, metric, 296, 297 eye, 41 U.S., 294, 295 hexagon, 26, 27, 36 Lines in drawings, 2 lock, 36 Liquid measure, metric, 297, 298 planer, 35 U.S., 295 slotted round, 42 Lock nuts, 36, 37 square, 26, 27 Loose pulley, 112 threads for, 59 Low pressure flanged fittings, 179, 180 wing, 39, 40 flanges, 172 screwed fittings, 178

Lubricating devices, 107

Octagon, construction of, 16
Odontograph for gear teeth, 142, 143,
144
Screws, 52, 53
Screws, drills for, 53

OG. Washers, 248
Oil cups, 107

Oilers, capillary, 107	Power transmission—Continued
Oiling rings, 107, 108	by gears, 141-161
Open belts, 124, 125	by rope, 127-131
wrench, 238	Press fit, 7
Ordering gears, 148-150	Pull, belt, 116
pipe, 162	chain, 132, 134, 136
pulleys, 110	Pulley, pulleys:
rivets, 273, 274	cast iron, 112-115, 128, 131
shapes, 283	keys, 83–88
tubes, 176	steel, 116, 122, 123
worm gears, 157	wood, 116
Outside flange pulley, 112	Punched holes, 286
	Punching, gauges for, 286-288
Parabola, construction of, 22	
Patent office drawings, 9	Quarter turn belts, 126
Patterns, weight of, 12	Quill drives, 91, 92
Penny nails, 77	1 ' '
Pillow blocks, 106, 108	Rack, construction of, 143
Pinion, 148-150	finish of, 266
Pins, split, 90	form for ordering, 150
taper, 264, 265	Radian, 295
Pipe bends, 170, 171	Radius of gyration, 277
couplings, 166	Railroad spikes, 82
double extra strong, 165	Rings, chain, 226
extra strong, 164	clinch, 249
fittings, 177-181	Rivet, rivets:
flanges, 172–176	heads, 269-274
ordering, 162	holes, 286
nipples, 75, 166, 167	joints, 276
standard, 163	measurement of, 25
threads, 71–76	points, 269
turnbuckles, 200, 202	proportions, 268-274
Pitch, circular (gears), 141, 145, 146	signs, 275
diameter (threads), 58	spacing, 288-291
diametral (gears), 141, 145, 146	tests, 271, 275
of chain, 221	Rods, circular, 54, 55
of rivets, 276	ends of, for yokes, 261
of threads, 58	square, 56, 57
Planer head bolts, 35	upset screw ends of, 54-57
nuts, 35	Roller chain, 133, 134
Plates, steel, weights of, 285	Roofing nails, 78, 80
Plug gauges, 9	Rope, drives, 127-131
Ply, belting, 121, 122	drums, 225
Points, nail, 78	Manila, 129
rivet, 269	sheaves, 127, 128
screw, 42	slings, 217-221
Polygon, construction of, 17	sockets, 205-208
lengths of sides, 24	thimbles, 204, 210
Power transmission, 91–161	Rough turning, 5
by belt, 124–127	Rubber belts, 119
by chain, 105, 132-140	Running fit, 4, 7, 8

•	
·Safety set screws, 49	Shrink fit, 7
Screw, screws:	Shrinkage of castings, 12
cap, 46	Shrouded gears, 141
coach, 51	Silent link chain, 135-137
collar, 53	Single belt, 119, 121
ends of bolts, 28, 265	pulley, 112
round bars, 54, 55	Sister hooks, 210
square bars, 56, 57	Sleeve nuts, 203
fittings (pipe), 177, 178	Sliding fit, 6
gauge, 43	Slings, chain, 224
hanger, 47	rope, 217–221
heads, 42, 44, 46, 47	Slotted nuts, 37, 42
lag, 51	Society of Automotive Engineers':
machine, 52, 58	bolts and nuts, 29
measurement of, 25	rod ends, 261
points, 42	threads, 29, 65
set, 49, 85, 110-112	yoke ends, 259, 260
thread, National Commission, 58, 64,	Socket, rope, 205-208
7 <del>4</del> –76	set screws, 49
threads, 58–71	wrench, 240, 241
thumb, 50	Solid friction clutch, 101–103
wood, 43-45, 48	Spanner wrench, 239, 240
Seamless brass tubes, 176	Specific gravities of materials, 303
copper tubes, 176	Spikes, railroad, 81, 82
steel tubes, 168, 169	round, 82, 83
Section modulus, 277	square, 81, 82
Set screws, dimensions of, 49	Spiral gears, 161
position of, 85, 110–112	jaw clutch, 104
Shackle bridle sling, 219	Split friction clutches, 99-101
for chain and anchor, 214, 215	pins, 90
swivel, 216, 217	Spring, springs:
Shaft, shafts, shafting:	compression, 250
bearings for, 106–109	cotters, 90
clutches, 91, 99–104	ends, 250
collars, 105	extension, 250
couplings, 94–98	formulæ, 251
dimensions of, 91	keys, 90
finished ends of, 265	table, 252, 253
hangers, 91, 109	Sprocket teeth, 134, 139
horse power, 93	wheels, 139, 140
key seats in, 83, 84	Spur gears, 141–150
materials of, 91	circular pitch of, 141, 145
Shearing stresses, 276, 302	construction of, 142-144
Sheaves, grooves in, 129, 130	diametral pitch of, 141, 146
wire rope, 127, 128	forms for ordering, 148-150
Sheet metal gauges, 284	h. p. of, 147
Shifting belts, 113	tooth forms, 142, 144
Ship rivets, 271, 272	working loads, 147
Shipping weight, 294	Square ends for chuck screws, 267
Shop rivets, 275	headed bolts, 26, 27
Shot of chain, 222	keys, 88
•	

Sames mate 28 97	Tomaile administration of the second of th
Square nuts, 26, 27	Tensile strength, see material in ques- tion
rods, 56, 57 threads, 63	Thimbles, 204, 210
washers, 247	equalizing, 218
Stagger of rivets. 290, 291	Thread, threads:
Standard pressure flanged fittings, 179	Acme, 64
flanges, 172	angle, 59
screw fittings, 178	Briggs pipe, 71, 72
Star wheel, 234	British Association, 62
Stay bolts, 34	British fine, 61, 62
Steel bars, flat, 285	buttress, 64
round, 54, 55	fits of, 71
square, 56, 57	forms of, 59-70
bolts, strength of, 59	French (metric), 63
cast, 263	lead, 58
pipe, 162	length of pipe, 177
plates, 285	National, Commission, 58, 66, 74-76
pulleys, 116, 122, 123	pipe, 71–76
rivets, 268-275	pitch, 58
shafts, 91	Soc. Aut. Eng'rs, 65
strength of, 271, 275, 279, 302	square, 63
structural shapes, 277-283	U. S. Standard, 59, 60
treatment of, 226	V, 60
tubes, 168, 169	Whitworth, 61, 73, 74
Stop valve, 183	Throttle valves, 188
Stove bolts, 33	Thumb nuts, 39, 40
Strength of materials, 302, see also ma-	screws, 50
terial in question	Timber, 303
Structural details, 286-293	Time measure, 295
rivets, 268–271	Tinners rivets, 274
shapes, 277–283	Tool straps, 262, 263
Stub teeth, 144	Tooth forms, gear, 142
Stub's steel wire gauge, 284	strength of, 147
Stud bolts, 28, 32	thickness of, 145, 146
link chain, 222, 223	Track bolts, 31
Stuffing boxes, 242-244	Troy weight, 294
Swinging check valve, 185, 186	Truss head rivets, 272
Swivel, 222	T alota, 89
shackles, 216	Tubes, boiler, 167
·	brass, 176
Tempering steel, 226	copper, 176
Tap bolts, 28, 35	steel, 168, 169
drills, 59, 60, 77	Turnbuckles, 200–203
rivets, 34	
Tapered drill shanks, 245, 246	Universal joints, 254–257
keys, 85, 86	U. S. bolts, 26
pins, 264, 265	measures, 297
Tees, pipe fittings, 178–181	nuts, 26
shapes, punching of, 287	sheet metal gauge, 284
	threads, 59, 60
Templates for drilling flanges, 173	wire gauge, 284

Units, electrical, 304 heat, 304 mechanical, 304

Valve, valves: check, 182, 185-187 gate, 189, 190 stop, 183 throttle, 188 V threads, 60

Wagon box head rivets, 273
Washers, circular, 247, 248
O. G., 248
square, 247
Weight, weights (see material in question):
and measures, metric, 297
U. S., 294
of common substances, 303
Wheels, sprocket, 135-137, 139, 140
Whitworth threads, bolt, 61
pipe, 73
Widths of belts, 119-121
Wing nuts, 39, 40

Wire gauges, 284 nails, 77 rope sheaves, 127, 128, 131 slings, 217-221 sockets, 205-208 thimbles, 204, 210 Wood, woods: properties of, 303 pulleys, 116 screws, 43-45 Woodruff keys, 86, 87 Working loads of gears, 147 Worm gearing, 156-159 Wrenches, box, 239 open, 238 socket offset handle, 240 T handle, 241 spanner, 239 squares for, 267 Wringing fit, 4 Wrought iron, 263 pipe, 163-165

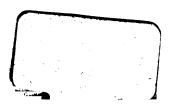
Yoke ends for rods, 259, 260

Zees, properties of, 282 punching of, 287

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